



**Project**

**Residential Development,  
Capdoo,  
Clane,  
Co. Kildare**

**Report Title**

**Site Specific Flood Risk Assessment**

**May 2019**

## Document Control

**Project Title:** Residential Development, Capdoo,  
Clane, Co. Kildare.

**Project Number:** 162074

**Report Ref:** 162074-rep-003

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**Approved By:**

**Date:** May 2019

**Distribution:** **An Bord Pleanala**

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Revision	Issue Date	Description	Prepared	Reviewed	Approved
Draft	Aug 2018	Draft	ED	BK	
-	Sep 2018	For ABP Pre-App Meeting	ED	BK	
<b>A</b>	<b>Apr 2019</b>	<b>For SHD Application</b>	<b>ED</b>	<b>BK</b>	

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## 1.0 INTRODUCTION

### 1.1 Background

DBFL Consulting Engineers have been instructed to prepare a Site-Specific Flood Risk Assessment (SSFRA) to support a planning application for a proposed residential development at Capdoo, Clane, Co. Kildare.

The proposed development (“the site”) comprises of 366 residential dwellings and a one-storey childcare facility on a 11.442 Ha site (approximately 0.7km north of Clane Town Centre).

The Net Developable Area is approximately 9.6778 Ha (omitting Capdoo Link Road, upgrade of Brooklands / Capdoo Link Junction and construction of the site’s surface water outfall).

The proposed site layout is shown on McCrossan O’Rourke Manning Architects Drawing Number 16016-PL02 (included in Appendix A).

This SSFRA should be read in conjunction with DBFL’s Infrastructure Design Report (162074-rep-002).

### 1.2 Objectives

The objectives of this report are to inform the planning authority in relation to flood risk associated with the site.

The report will assess the site in accordance the requirements of “The Planning System and Flood Risk Management, Guidelines for Planning Authorities” and its Technical Appendices (Office of Public Works, November 2009).

This flood risk assessment will outline the following;

- Information to allow an informed decision by the planning authority in relation to flood risk
- The site’s flood zone category
- Appropriate flood risk mitigation and management measures for any residual flood risk

### 1.3 Flood Risk Assessment Scope

This SSFRA relates only to the proposed development lands at Capdoo, Clane, Co. Kildare and its immediate surroundings.

This SSFRA uses information obtained from various sources in order to carry out an assessment of flood risk for the existing land and proposed development.

### 1.4 Approach

Section 2.0 of this SSFRA considers “The Planning System and Flood Risk Management, Guidelines for Planning Authorities” and its Technical Appendices as they relate to the site.

Flood risk identification is presented in Section 3.0, an initial flood risk assessment is carried out in Section 4.0, while a more detailed flood risk assessment is presented in Section 5.0.

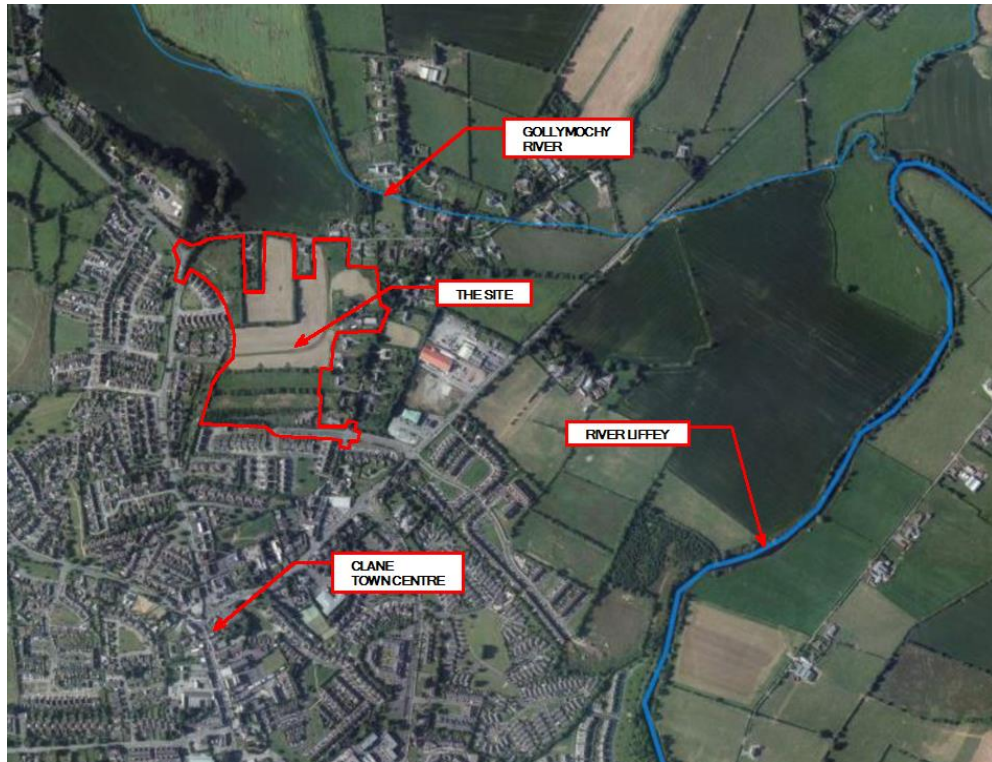
Conclusions and recommendations are outlined in Section 6.0.

### 1.5 Existing Site

The site (currently greenfield) is situated in the northern environs of Clane town (refer to Figure 1.1) and is currently in agricultural use. A farmhouse and stables are located adjacent to the eastern boundary.

Capdoo Park is located to the south of the site and Mainham Woods and College Road East are located to the west of the site. Rural roads are located to the north and east of the site (“Capdoo Common”). Several existing residential dwellings are located along these rural roads.

The proposed route of the Capdoo Link Road traverses the site (linking the Kilcock Road. to Celbridge Road).



**Figure 1.1 Extract from EPA Online Mapping Service (Site Boundary Indicative Only)**

The site generally falls from west to east at gradients ranging from 1/15 to 1/100. (refer to Figure 1.2 and Appendix B for Topographic Survey Plans prepared by Land Surveys).

A network of open drains is located to the east of the site which ultimately discharge to the Gollymochy Stream (refer to Figure 1.1).

Existing public surface water drains are located to the south and west of the site (refer to Figure 1.2 below). As the site naturally falls from west to east, it is proposed to construct a surface water outfall along the roads north east of the site and discharge to the Gollymochy Stream north (refer to DBFL Drawing 162074-3002). The majority of the site will discharge to this outfall with the link road and an isolated section north west of the site draining to the public surface water drains to the south and north-west.

Existing topographic survey information is shown in the background of the Proposed Road Layout Plans (refer to DBFL Drawing No's. 162074-2000, 162074-2001, 162074-2002 and 162074-2003).

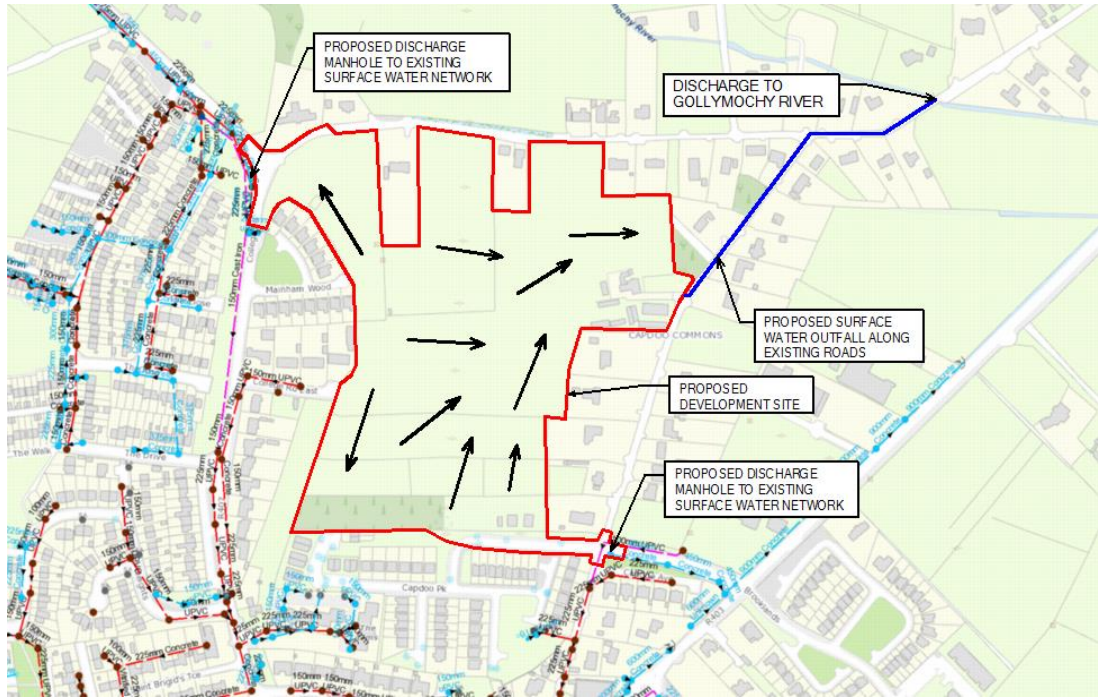


Figure 1.2 Extract from Irish Water Utility Plan.

## 1.6 Proposed Development

The proposed development comprises of 366 residential dwellings, a one-storey childcare facility and associated engineering infrastructure including provision of surface water drainage, foul drainage and water supply connections (refer to DBFL Drawings 162074-3001, 162074-3002, 162074-3003, 162074-3005, 162074-3006 and 162074-3007). It also includes the completion of the Capdoo Link Road and associated roundabout on the R407 (Kilcock Road) which will also facilitate primary access to the proposed development.

## 2.0 PLANNING SYSTEM FLOOD RISK MANAGEMENT GUIDELINES

### 2.1 General

“The Planning System and Flood Risk Management, Guidelines for Planning Authorities” and its Technical Appendices outline the requirements for a Site Specific Flood Risk Assessment.

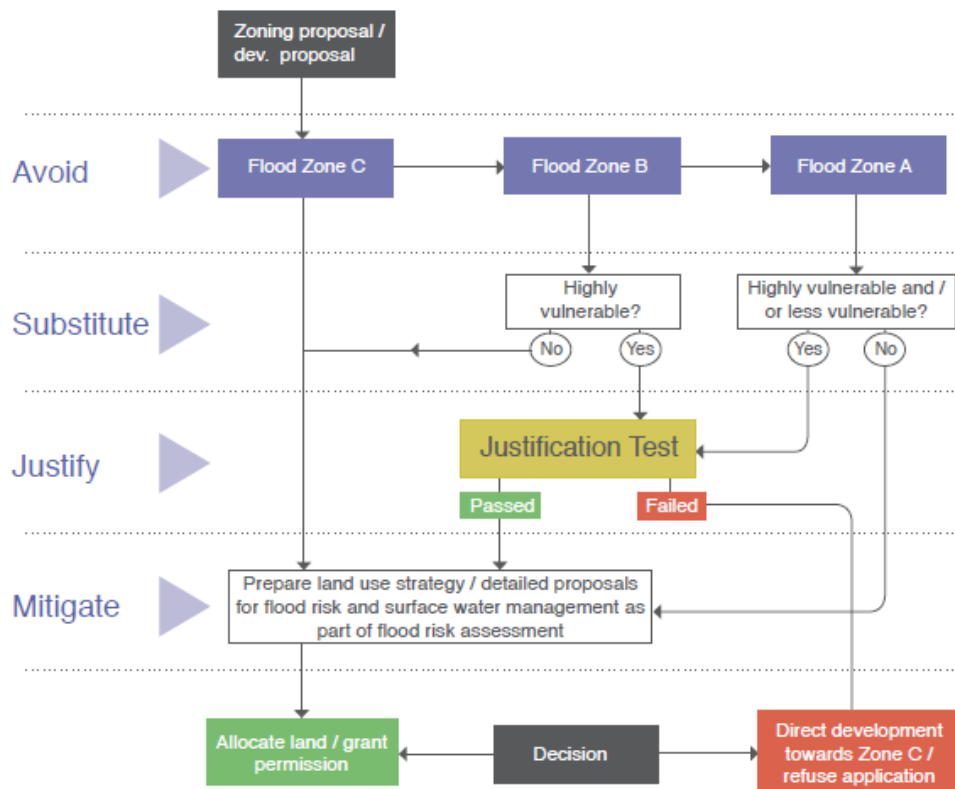
Table 3.1 of the guidelines classify “dwelling houses” as “highly vulnerable development”.

Table 3.2 of the guidelines indicates that a “highly vulnerable development” is classified as “appropriate” once located in Flood Zone C i.e. where probability of flooding from rivers is low (less than 0.1% AEP or 1 in 1,000 year).

If a “highly vulnerable development” is to be located in Flood Zone A or Flood Zone B a Justification Test is required.

### 2.2 Sequential Approach

This SSFRA will initially use existing flood risk information to determine the flood zone category of the site i.e. to determine whether the development is considered appropriate or whether a justification test is required (see Figure 2.1 below).



**Figure 2.1 – Extract from The Planning System and Flood Risk Management Guidelines (Fig. 3.2: Sequential Approach Mechanism in the Planning Process)**



## 2.3 Flood Risk Assessment Stages

The stages of a Flood Risk Assessment as defined by “The Planning System and Flood Risk Management, Guidelines for Planning Authorities” and its Technical Appendices are as follows:

- Stage 1 – Flood Risk Identification
- Stage 2 – Initial Flood Risk Assessment
- Stage 3 – Detailed Flood Risk Assessment

The following sections of this SSFRA follows this approach.

### 3.0 STAGE 1 – FLOOD RISK ASSESSMENT

#### 3.1 General

The flood risk identification stage uses existing information to identify whether there may be any flooding or surface water management issues related to the site that may require further investigation.

#### 3.2 Information Sources

Information sources consulted for the identification exercise are outlined in Table 3.1 below.

Information Source	Comments
Predictive and historic flood maps, and Benefiting Lands Maps, such as those at <a href="http://www.floodmaps.ie">www.floodmaps.ie</a> .	Information obtained (and reviewed) from <a href="http://www.floodmaps.ie">www.floodmaps.ie</a> (OPW website).
Expert advice from OPW who may be able to provide reports containing the results of detailed modelling and flood-mapping studies, including critical drainage areas, and information on historic flood events, including flooding from all sources.	Information obtained (and reviewed) from <a href="http://www.floodmaps.ie">www.floodmaps.ie</a> (OPW website) e.g. minutes from flood hazard mapping meeting with KCC Area Engineer.
Predictive flood maps produced by OPW	Floodinfo.ie providing access to Eastern CFRAM study Flood Maps –Fluvial Flood Extents and Fluvial Flood Depth Maps consulted.
Previous Strategic Flood Risk Assessments;	Eastern CFRAM Study consulted.
Topographical maps, in particular digital elevation models produced by aerial survey or ground survey techniques;	Site topographic survey undertaken (refer to Appendix B).
Information on flood defence condition and performance;	No flood defences identified in the immediate vicinity of the site.

Maps of the Geological Survey of Ireland (which would allow the potential for the implementation of source control and infiltration techniques and for groundwater and overland flood risk to be assessed). These maps, while not providing full coverage, can indicate areas that have flooded in the past (the source of the alluvium) and may be particularly useful at the early stages of the FRA process where no other information is available.	GSI maps consulted.
Walkover survey to assess potential sources of flooding, likely routes for flood waters and the site's key features, including flood defences, and their condition;	Walkover survey carried out.
National, regional & local spatial plans, such as the National Spatial Strategy, regional planning guidelines, development plans & local area plans provide key information on existing and potential future receptors.	Kildare County Council Development Plan and Clane Local Area Plan (LAP) consulted.
'Liable to flood' markings on the old '6 Inch' maps;	Historic OSI maps consulted.

**Table 3.1 - Information Sources Consulted**

### 3.2.1 OPW National Flood Hazard Mapping and Benefitting Lands Mapping

OPW's Summary Local Area Report is included in Appendix C (Flood Hazard Information). This report is sourced from the OPW website ([www.floodmaps.ie](http://www.floodmaps.ie)) and summarises all flood events within 2.5 km of the site. No flood events are noted in the immediate vicinity of the site.

### 3.2.2 Eastern CFRAM Study

Extracts from OPW's Eastern CFRAM Study ([www.floodinfo.ie](http://www.floodinfo.ie)) show Fluvial Flood Extent and Fluvial Flood Depth Plans and are included in Appendix C (Flood Hazard Information).

No fluvial flooding is indicated in the vicinity of the site.

### 3.2.3 Clane Local Area Plan (2017-2023)

Map ref. 9.1 from the Clane Local Area Plan 2017 to 2023 (see Appendix C Flood Hazard Information) which identifies the site being partially located in an area where “development proposals for lands outlined thus are to be the subject of site specific flood risk assessment in accordance with the flood risk management guidelines and appropriate to the type and scale of the development being proposed”.

### 3.2.4 Other Sources

Other information sources were consulted to determine if there was any additional flood risk to the site including:

- Topographical surveys of the area – the site is significantly elevated above the predicated 0.1% AEP fluvial flood level as shown in the Eastern CFRAM Study’s Flood Extent Maps.
- Soils and Groundwater Data from the GSI – no alluvium deposits or groundwater wells / springs are shown within the site on the GSI online mapping system.
- Groundwater information from IGSL – Ground water (seepage) was noted in trial pits and infiltration tests carried out in the north east of the site. The depth at which seepage was observed in these trial pits ranged from 0.9m to 2.2m below existing ground level. Refer to refer to Appendix D.
- Walkover survey carried out in November 2017 – no potential sources of flooding identified.
- Clane Local Area Plan (LAP) – the site is zoned for residential development.
- Irish Water Records – Existing surface water and foul drainage network are located to the south and west of the site.
- 6 inch OSI Map – no evidence of flooding or marsh areas shown within the site.

Review of the ‘other sources’ of information noted above do not indicate evidence of flood risk to the site.

### 3.3 Source Pathway Receptor Model

A Source-Pathway-Receptor model has been produced to summarize the possible sources of floodwater, the pathways by which flood water could reach receptors and the receptors that could be affected by potential flooding, see Table 3.2 below.

It outlines effects of various potential sources, the performance and response of pathways and the consequences to the receptors in the context of the proposed development.

These sources, pathways and receptors will be assessed further by the initial flood risk assessment stage.

Source	Pathway	Receptor	Likelihood	Consequence	Risk
Fluvial	Overbank from the Gollymochy Stream approximately 150m north-east of the site (refer to Figure 1.1)	People and Property (the proposed development).	Low	Medium	Low
Surface Water (Pluvial)	Blockage and / or surcharging of the proposed surface water drainage network	People and Property (the proposed development).	Possible	Medium	Medium
Human / Mechanical Error (Pluvial)	Failure of proposed SuDS measures (e.g. Hydrobrake failure)	People and Property (the proposed development).	Possible	Medium	Medium
Groundwater	Rising groundwater levels within the site	People and Property (the proposed development).	Remote	Medium	Low

**Table 3.2 - Source-Pathway-Receptor Analysis**

## 4.0 STAGE 2 – INITIAL FLOOD RISK ASSESSMENT

Flood risks identified during Stage 1 – Flood Risk Identification, are outlined in Table 3.2 (Source Pathway Receptor Analysis) and noted below. These risks are assessed further in this section of the SSFRA.

- Low risk of fluvial flooding
- Medium risk of pluvial flooding (surface water and human / mechanical error)
- Low risk of groundwater flooding

The information sources identified in Section 3.2 are considered adequate for the purpose of an Initial Flood Risk Assessment of the site and no further technical studies are proposed.

### 4.1 Initial Fluvial Flood Risk Assessment

The Eastern CFRAM flood extents mapping identifies the location of the predicated 1% AEP and 0.1% AEP fluvial flood events associated with watercourses in the Clane area (refer to Appendix C). No fluvial flooding is indicated in the vicinity of the site.

The closest modelled node to the site is located on the Gollymochy Stream (Node 09GOLL00135), approximately 150m north of the site.

The location of this node is shown on CFRAM Drawing E09CLA\_EXFCD\_F1\_11 (refer to Appendix C).

- |  |        |
|--|--------|
| • Node 09GOLL00135, 1% Fluvial AEP Event             | +66.22 |
| • Node 09GOLL00135, 0.1% Fluvial AEP Event           | +66.33 |
| • Lowest Proposed FFL (see DBFL Drawing 162074-2002) | +67.98 |
| • Freeboard from 1% AEP Flood Level                  | 1.76 m |

Note: Min. freeboard from 1% AEP required by GDSDS – 500mm.

## 4.2 Initial Pluvial Flood Risk Assessment

The Source-Pathway-Receptor model identified a medium risk of pluvial flooding relating to the proposed surface water drainage network and human / mechanical error. This risk can be mitigated by designing the surface water network in accordance with the Greater Dublin Strategic Drainage Study (GDSDS) including attenuation of the 1% AEP storm event and implementation of SuDS methodologies.

Proper operation and maintenance of the drainage system should also be implemented to reduce the risk of human or mechanical error causing pluvial flood risk from blockages, fuel / oil interceptor operation problems, Hydrobrake failure etc.

## 4.3 Initial Groundwater Flood Risk Assessment

During the site walkover survey, no marshy ground was observed. No groundwater wells or marsh areas are located within the site (based on review of information available on the GSI and OSI websites).

Therefore, the risk of groundwater flooding occurring at the site is considered negligible.

## 4.4 Flood Zone Category

On completion of Stage 2 – Initial Flood Risk Assessment, the site is considered to be located in Flood Zone C as defined by the requirements of “The Planning System and Flood Risk Management, Guidelines for Planning Authorities” and its Technical Appendices.

The proposed development (“dwelling houses”) is therefore considered appropriate.

## 5.0 STAGE 3 – DETAILED FLOOD RISK ASSESSMENT

### 5.1 General

As the Initial Flood Risk Assessment considers the site to be located in Flood Zone C and the proposed development is considered appropriate the Detailed Flood Risk Assessment Stage will only consider pluvial flood risk in relation to the following;

- Proposed Surface Water Management Measures and SuDS
- Flood Exceedance.
- Impact on Adjacent Areas.
- Climate Change.
- Access and Egress for Emergency Services during Flood Events.
- Residual Risks.
- Effectiveness of Flood Mitigation Measures.

### 5.2 Surface Water Management Measures and SuDS

The Gollymochy Stream is approximately 150m to the north of the site. The Gollymochy is expected to provide a suitable surface water discharge point for the proposed development, via a proposed surface water outfall constructed along rural roads to the north-east of the site (refer to DBFL Drawing 162074-3002). This will serve the majority of the site with the Capdoo Link Road and an isolated section north west of the site draining to the existing public surface water drainage network. The north west section and the upper link road will discharge to an existing surface water manhole north west of the site on College Road and the lower link road will discharge to an existing surface water manhole south east of the site adjacent to Capdoo Avenue.

Proposed surface water drains have been designed in accordance with the Greater Dublin Strategic Drainage Study (GDSDS). Surface water discharge rates from the proposed surface water drainage network will be controlled by a Hydrobrake type flow control device and associated underground attenuation tanks (Stormtech Chambers). Surface water discharge will also pass via a full retention fuel / oil separator (sized in accordance with permitted discharge from the site).

The proposed surface water drainage network will collect surface water runoff from the site via a piped network prior to discharging off site via the attenuation tank, flow control device and separator arrangement as noted above.



Surface water runoff from the site's road network and link road will be directed to the proposed pipe networks via conventional road gullies while surface water runoff from driveways will be captured by permeable paving.

Surface water runoff from roofs will be routed to the proposed surface water pipe network via the porous aggregates beneath permeable paved driveways (providing an additional element of attenuation).

### 5.2.1 SuDS Methodologies

The following methodologies are being implemented as part of a SuDS treatment train approach:

- Permeable paving in driveway areas
- Surface water runoff from roofs will be routed to the proposed surface water pipe network via the stone reservoirs beneath permeable paved driveways. Note, this detail does not rely on infiltration, the stone reservoir is intended to provide an additional element of attenuation storage
- Attenuation of the 100-year return period storms within Stormtech Attenuation Chambers, note our calculated attenuation volume does not rely on infiltration.
- "Smart Manholes" (with internal weir) to ensure attenuation systems and Hydrobrakes continue to operate up to and including the 1.0% AEP storm event.
- Installation of a Hydrobrake (limiting surface water discharge from the site to 2.0 l/sec/ha)
- Surface water discharge will also pass via a Class 1 full retention fuel / oil separator (sized in accordance with permitted discharge from the site).

### 5.2.2 Surface Water Attenuation and Storage

Attenuation volumes have been calculated based on an allowable outflow / greenfield runoff rate of 2.0 l/sec/ha.

### 5.3 Flood Risk Exceedance

During storms greater than the 1% AEP pluvial event, the development's drainage network design will be exceeded and areas with low ground levels will begin to flood.

Generally, proposed road levels fall towards the west and north. Overland flow is therefore directed towards open space areas, rural roads located to the north and west of the site and the proposed Capdoo Link Road (refer to Figure 5.1).

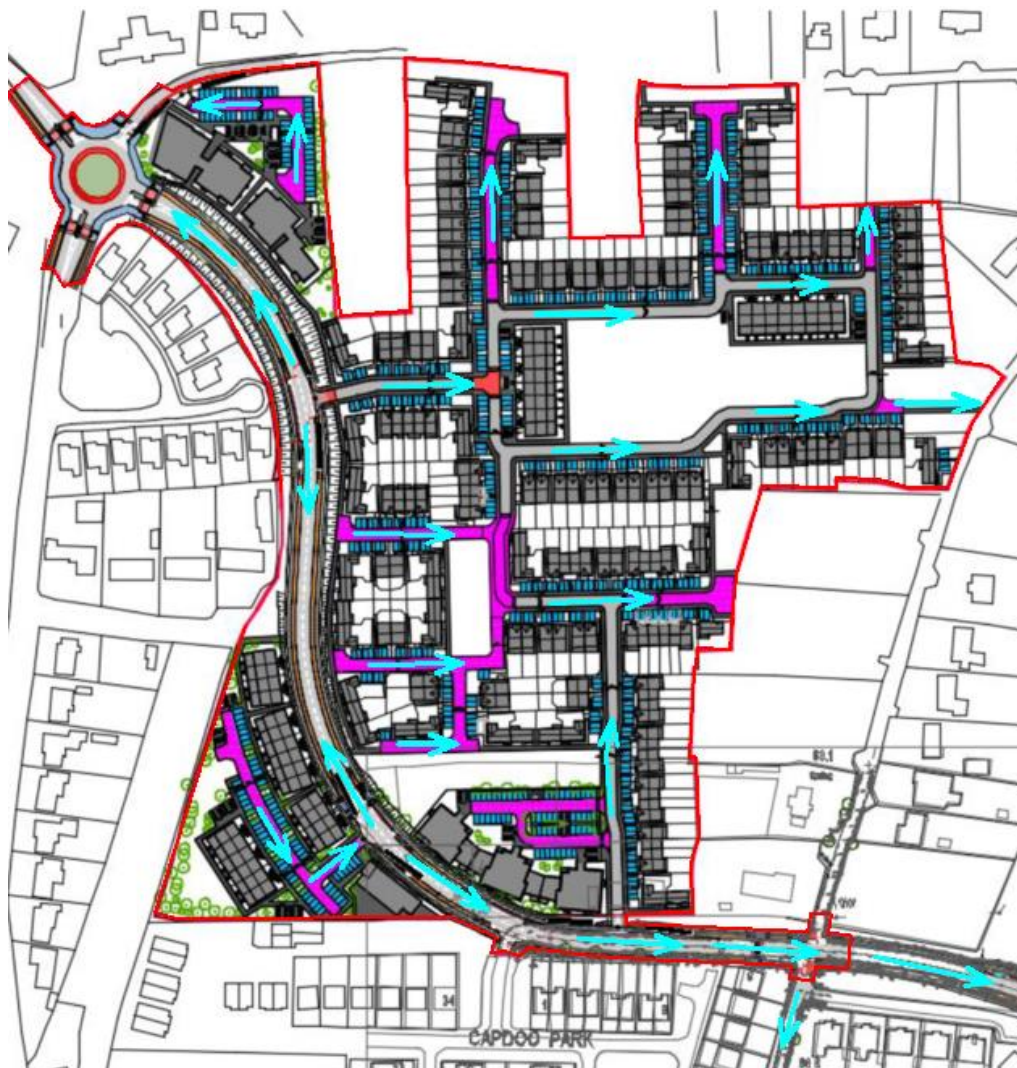


Figure 5.1 – Flood Exceedance (>1%AEP) Overland Flow Routes UPDATE

## 5.4 Impact on Adjacent Areas

Adjacent areas will not be impacted by the development up to the 1% AEP flood event.

Storms greater than the 1% AEP (exceeding the design capacity of the site's drainage system) may result in overland flow being directed towards open space areas, rural roads located to the north and west of the site and the proposed Capdoo Link Road.

## 5.5 Climate Change

The potential impact of climate change has been allowed for as follows;

- Pluvial flood risk - attenuation storage design allows for a 20% increase in rainfall intensities, as directed by Kildare County Council's Water Services Engineer.
- Pluvial flood risk - drainage system design allows for a 20% increase in flows, as recommended by the GSDS.

## 5.6 Access and Egress for Emergency Services During Flood Events

Access and egress to the site is provided primarily by way of the proposed Capdoo Link Road which will transverse the site. The proposed apartments located in the north west corner of the site can be accessed from a regional road running north of the proposed development.

The Capdoo Link Road and regional road north of the site are located in Flood Zone C as defined by the OPW guidelines therefore, it is expected that the site can be safely accessed during storm events up to 1% AEP event.

## 5.7 Residual Risks

Remaining residual flood risks, following the detailed assessment include the following;

1. Pluvial flooding from the private drainage system related to pipe blockage, flood exceedance or mechanical failure.
2. Pluvial flooding from the development's drainage system for storms in excess of the 1% AEP storm event.

## 5.8 Mitigation Measures

Proposed mitigation measures to address residual flood risks are summarized below;

M1. Proposed drainage system to be maintained on a regular basis to reduce the risk of a blockage.

M2. In the event of storms exceeding the 1% AEP design capacity of the attenuation system, possible overland flow routing towards open space areas should not to be blocked. At these locations, the site's boundaries should be permeable to facilitate flood routing onto adjacent public roads.

### 5.2.1 Effectiveness of Mitigation Measures

It is considered that the flood risk mitigation measures if implemented are sufficient to provide a suitable level of protection to the proposed development. A regularly maintained drainage system will ensure that it remains effective and in good working order should a large pluvial storm occur.

Should extreme pluvial flooding occur that is in excess of the development's attenuation capacity (i.e. greater than 1%AEP), then overland flow routes directed towards open space areas are provided in order to protect the proposed development.

## 6.0 CONCLUSIONS

The Site-Specific Flood Risk Assessment for proposed development at Capdoo, Clane was undertaken in accordance with the requirements of “The Planning System and Flood Risk Management, Guidelines for Planning Authorities” and its Technical Appendices.

Following the Flood Risk Assessment, it has been determined that is located in Flood Zone C as defined by the Guidelines.

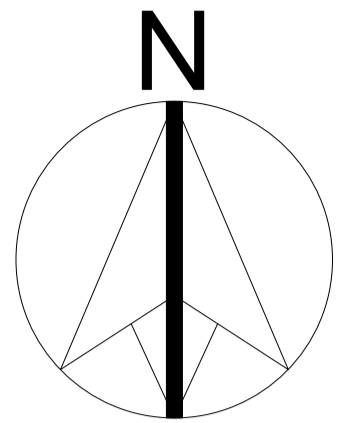
It is concluded that the;

- Proposed residential development is appropriate for the site’s flood zone category.
- The sequential approach outlined in Planning System and Flood Risk Management Guidelines has been adhered to and that the ‘Avoid’ principal has been achieved.

In conclusion, the proposed development is considered to have the required level of flood protection up to and including the 1% AEP flood event.

Overland flow paths have been identified for pluvial flooding exceeding the capacity of the surface water drainage network.

## APPENDIX A – PROPOSED SITE LAYOUT



EXTENT OF SHEET 16016 PL03

EXTENT OF SHEET 16016 PL04

### GENERAL NOTES

SITE BOUNDARY OUTLINED IN RED

THIS DRAWING TO BE READ IN CONJUNCTION WITH ARCHITECT'S DRAWINGS CONSULTANT ENGINEER'S DRAWINGS AND SPECIFICATIONS LANDSCAPE ARCHITECT'S DRAWINGS AND SPECIFICATIONS

FOR ROAD AND SITE LEVELS REFER TO DBFL CONSULTING ENGINEERS DRAWINGS

### Schedule of Accomodation:-

Dwelling Type	Total	(and %)
2 bedroom house	20	(5.46%)
3 bedroom house	75	(20.49%)
4 bedroom house	77	(21.03%)
5 bedroom house	12	(3.28%)

Total houses **184** (50.27%)

1 bed own door apartment	12	(3.28%)
1 bed apartment	16	(4.37%)
2 bed apartment	82	(22.4%)
2 bed own door apartment under duplex	36	(9.84%)
3 bed own door duplex	36	(9.84%)

Total Apartments/ Duplexes **182** (49.73%)

TOTAL NO. OF DWELLINGS	<b>366</b>
APPLICATION SITE AREA (RED LINE BOUNDARY)-	11.442HA
SITE AREA IN APPLICANT'S OWNERSHIP	10.798HA
NET DEVELOPMENT AREA (OMITTING Spine Road)	9.6778HA
GROSS DENSITY (366/ 10.798)	33.89 /HA
NET DENSITY (366/ 9.6778)	37.82 /HA

### Public Open Space

Total Public Open Space	1.6125HA
As a % of Development Area	16.668%

### Data Source / Reference:

PRIME2

### File Format:

Autodesk AutoCAD (DWG\_R2013)

### File Name:

v\_50016012\_1.dwg

### Clip Extent / Area of Interest (AOI):

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LRX,LRX= 688133.6823,728073.566  
ULX,ULY= 687303.6823,728688.566  
URX,URY= 688133.6823,728688.566

### Projection / Spatial Reference:

Projection= IRENET95\_Irish\_Transverse\_Mercator

### Centre Point Coordinates:

X,Y= 687718.6823,728381.066

### Data Extraction Date:

Date= 17-Jul-2018

### Version / Release:

Version= 1.0

### License / Copyright:

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### NOTES:

DO NOT SCALE FROM DRAWINGS. WORK TO FIGURED DIMENSIONS ONLY. ARCHITECT TO BE NOTIFIED OF ALL DISCREPANCIES.

REVISIONS		
DATE	DESCRIPTION	No.

ROSSAN O'ROURKE MANNING ARCHITECTS

PROJECT TITLE  
**Capdoo, Clane**

DRAWING TITLE  
**Residential Development Site Layout**

DATE  
July 2018

SCALE  
1:1000

SUB NO.  
16016

DRAWING NO.  
PL02

DATE  
July 2018

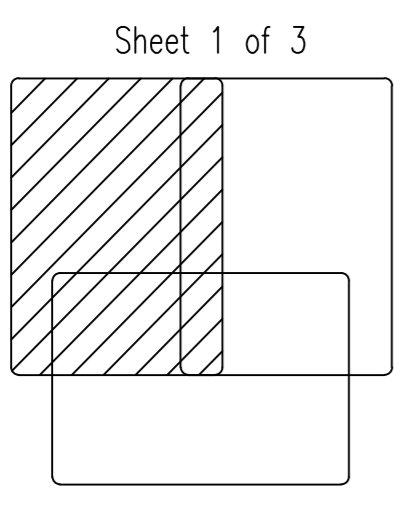
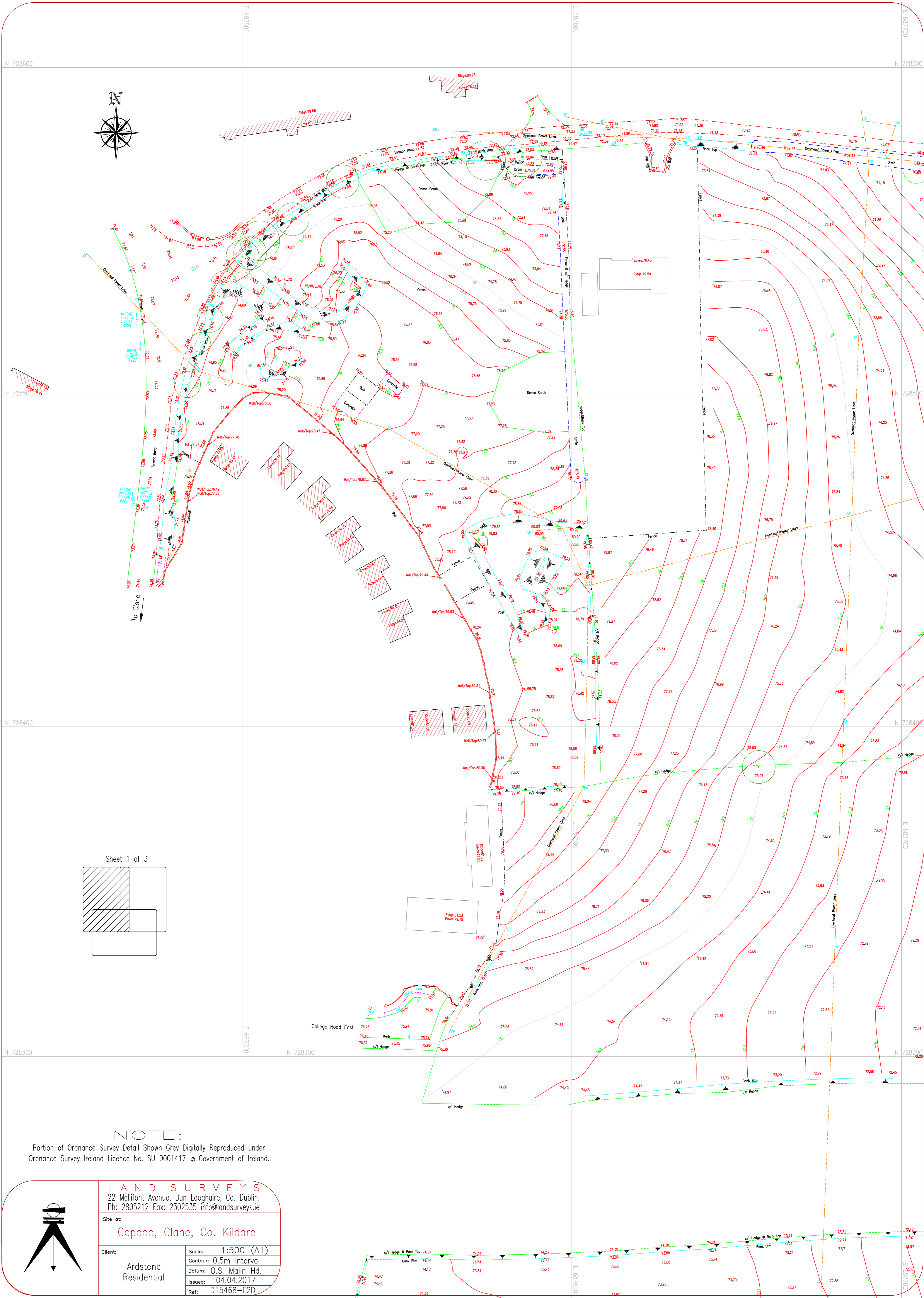
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PL02

## APPENDIX B – TOPOGRAPHIC SURVEY PLANS





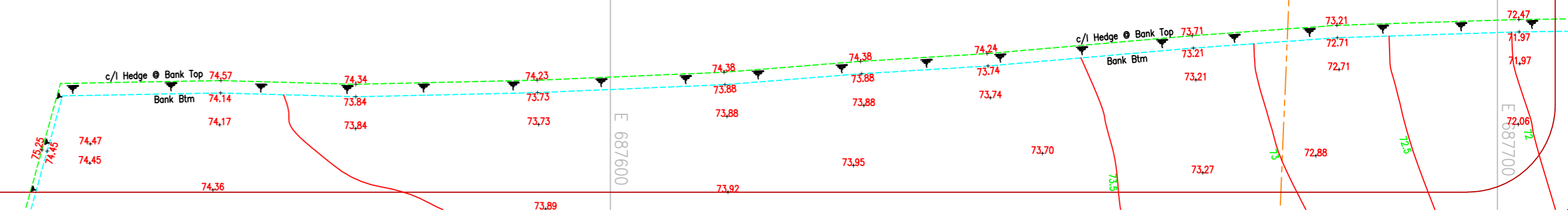
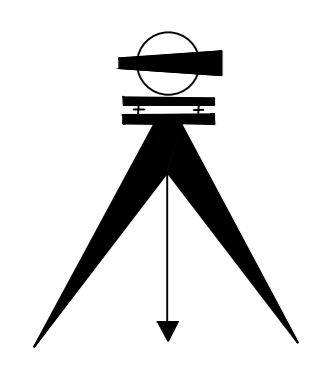
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 22 Mellifont Avenue, Dun Laoghaire, Co. Dublin.  
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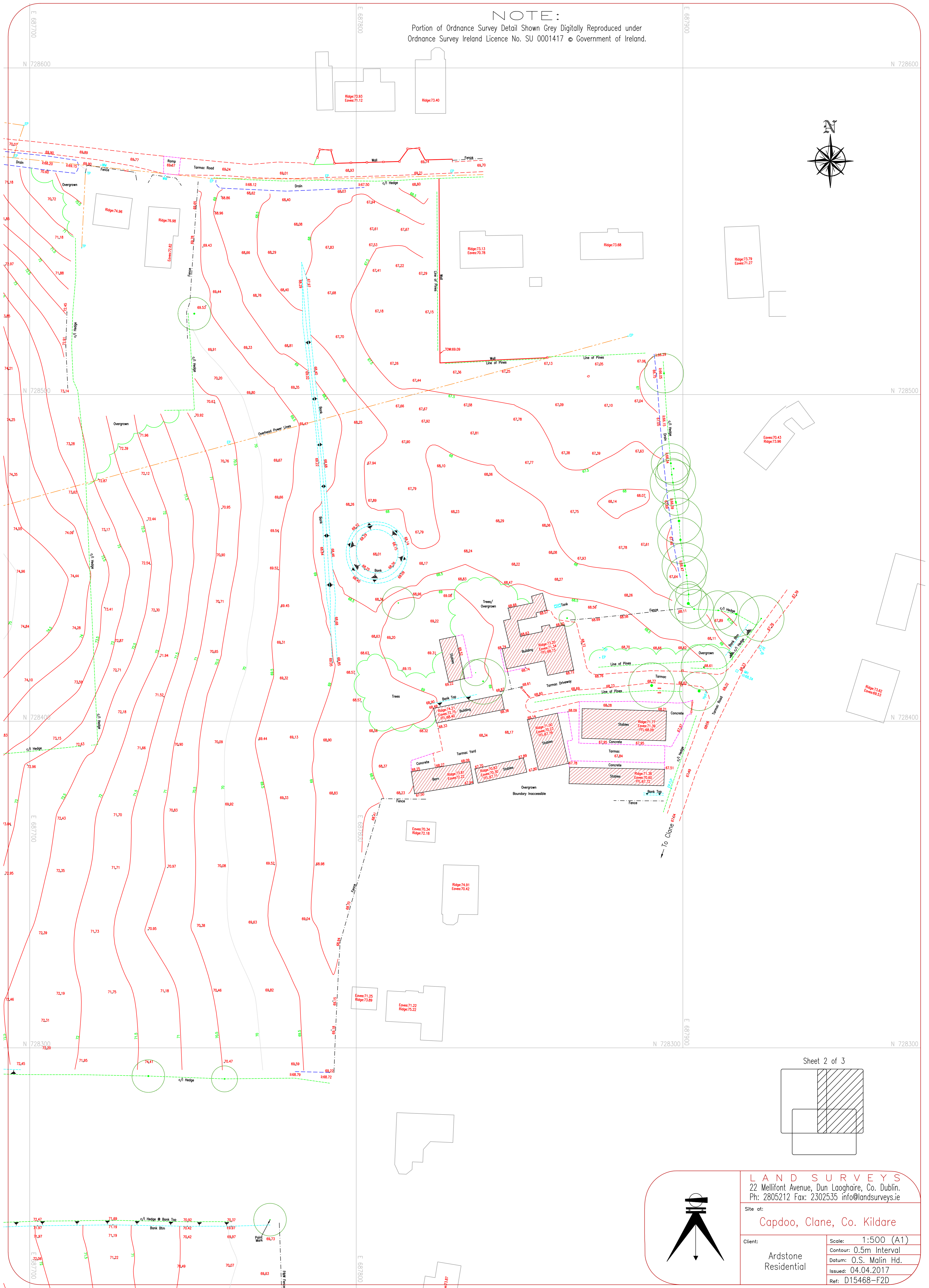
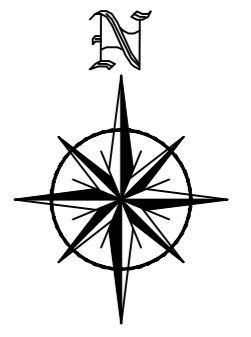
Site at:  
**Capdoo, Clane, Co. Kildare**

Client:  
**Ardstone Residential**

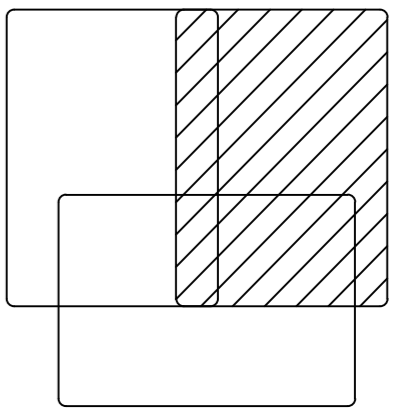
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 Contour: 0.5m Interval  
 Datum: O.S. Malin Hd.  
 Issued: 04.04.2017  
 Ref: D15468-F2D



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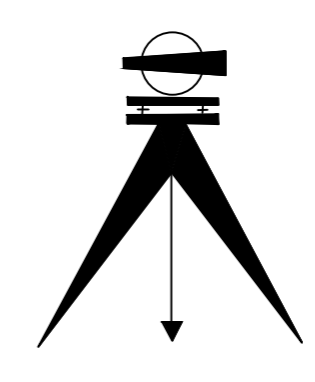
Sheet 2 of 3

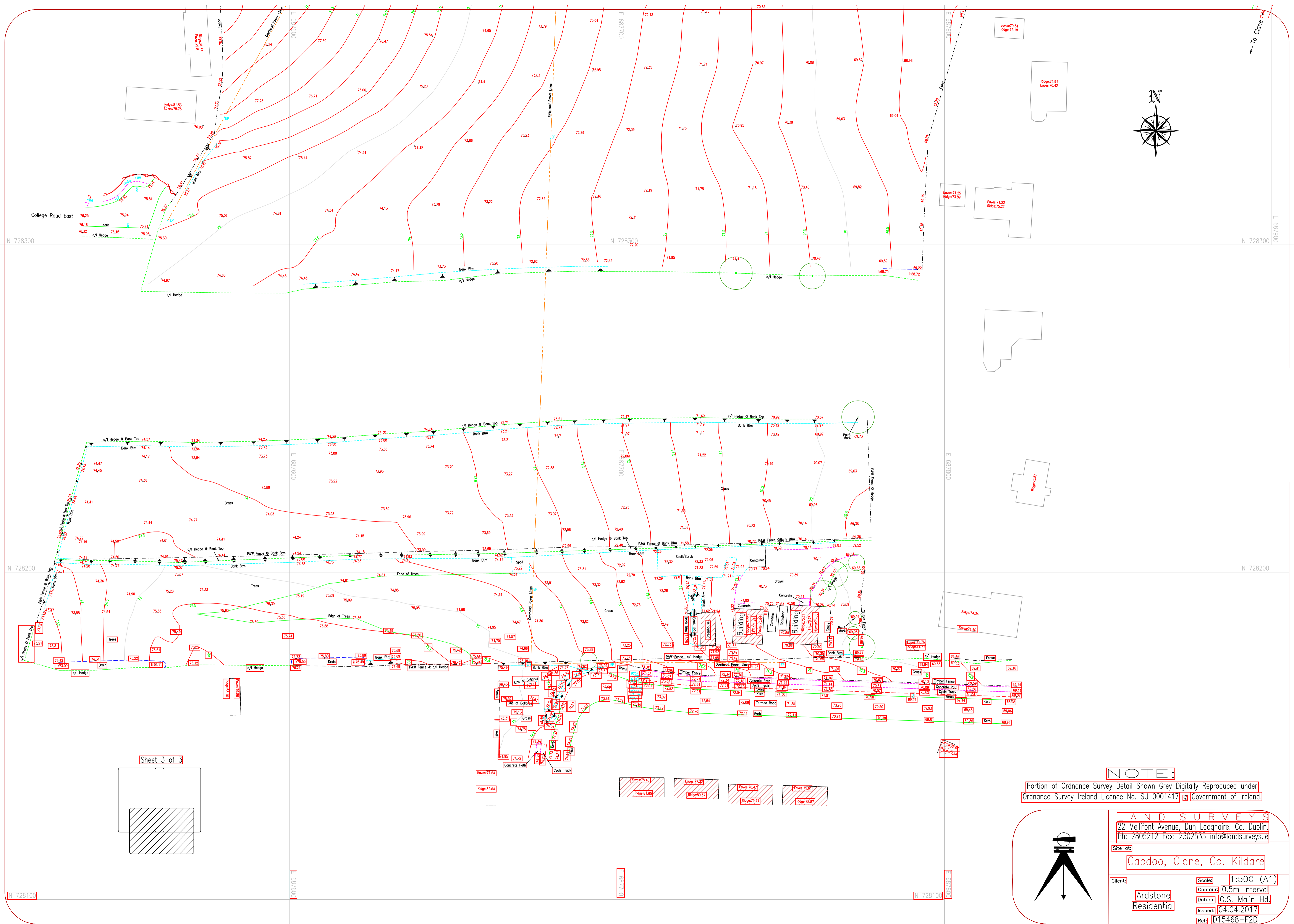


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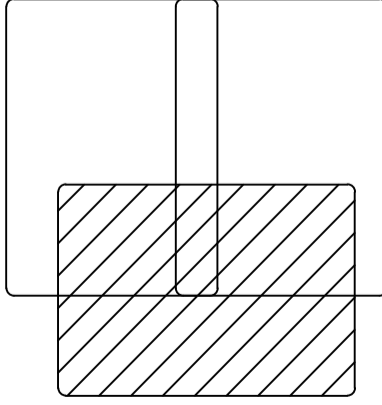
Site at:  
**Capdoo, Clane, Co. Kildare**

Client:	Ardstone Residential
Scale:	1:500 (A1)
Contour:	0.5m Interval
Datum:	O.S. Malin Hd.
Issued:	04.04.2017
Ref:	D15468-F2D

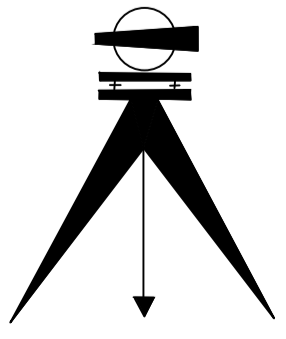




Sheet 3 of 3



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Site at:  
**Capdoo, Clane, Co. Kildare**

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**Ardstone Residential**

Scale: 1:500 (A1)  
 Contour: 0.5m Interval  
 Datum: O.S. Malin Hd.  
 Issued: 04.04.2017  
 Ref: D15468-F2D

## APPENDIX C – FLOOD HAZARD INFORMATION

## Summary Local Area Report

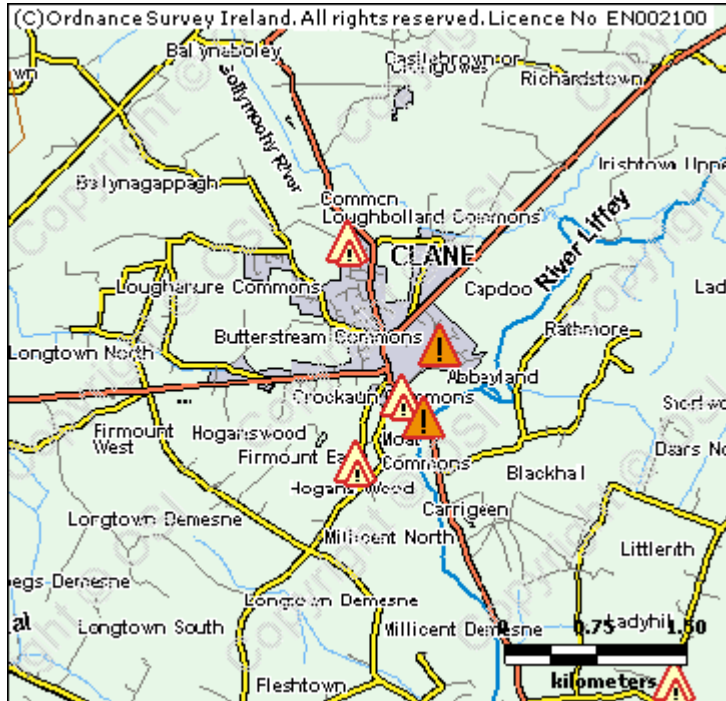
This Flood Report summarises all flood events within 2.5 kilometres of the map centre.

The map centre is in:

County: Kildare

NGR: N 875 276

This Flood Report has been downloaded from the Web site [www.floodmaps.ie](http://www.floodmaps.ie). The users should take account of the restrictions and limitations relating to the content and use of this Web site that are explained in the Disclaimer box when entering the site. It is a condition of use of the Web site that you accept the User Declaration and the Disclaimer.



Map Scale 1:62,129

Map Legend	
	Flood Points
	Multiple / Recurring Flood Points
	Areas Flooded
	Hydrometric Stations
	Rivers
	Lakes
	River Catchment Areas
	Land Commission *
	Drainage Districts *
	Benefiting Lands *

\* Important: These maps do not indicate flood hazard or flood extent. Their purpose and scope is explained in the Glossary.

## 5 Results

	1. Liffey Clane Dec 1954 County: Kildare Additional Information: Reports (2) Press Archive (1) More Mapped Information	Start Date: 08/Dec/1954 Flood Quality Code:2
	2. Morrell Clane 30th Dec to 1st Jan 2010 County: Kildare Additional Information: Reports (1) More Mapped Information	Start Date: 30/Dec/2009 Flood Quality Code:3
	3. Loughbrollard, Clane Recurring County: Kildare Additional Information: Reports (1) More Mapped Information	Start Date: Flood Quality Code:4
	4. Millicent Rd, Clane Recurring County: Kildare Additional Information: Reports (1) More Mapped Information	Start Date: Flood Quality Code:4
	5. Commons, Clane Recurring County: Kildare	Start Date: Flood Quality Code:4



## MINUTES OF MEETING

**Reference:** P4D403A – F310 – 017 – 004-001 Page 1 of 3

**Project No.:** P4D403A

**Project Title:** OPW Flood Hazard Mapping – Phase 1

**Purpose of Meeting:** Kildare County Council – Oral Report – Area Engineer – Clane

**Participating:**

Area Engineer	Kildare County Council
Supervisor	Kildare County Council
Search Manager	ESBI

**Venue:** Clane

**Date of Meeting:** 22/03/05

**Copies to:**

**Compiled by:** Search Manager ESBI

**Status** Draft

**Approved for ESBI:**

**Approved for Kildare County Council**

**Date:**

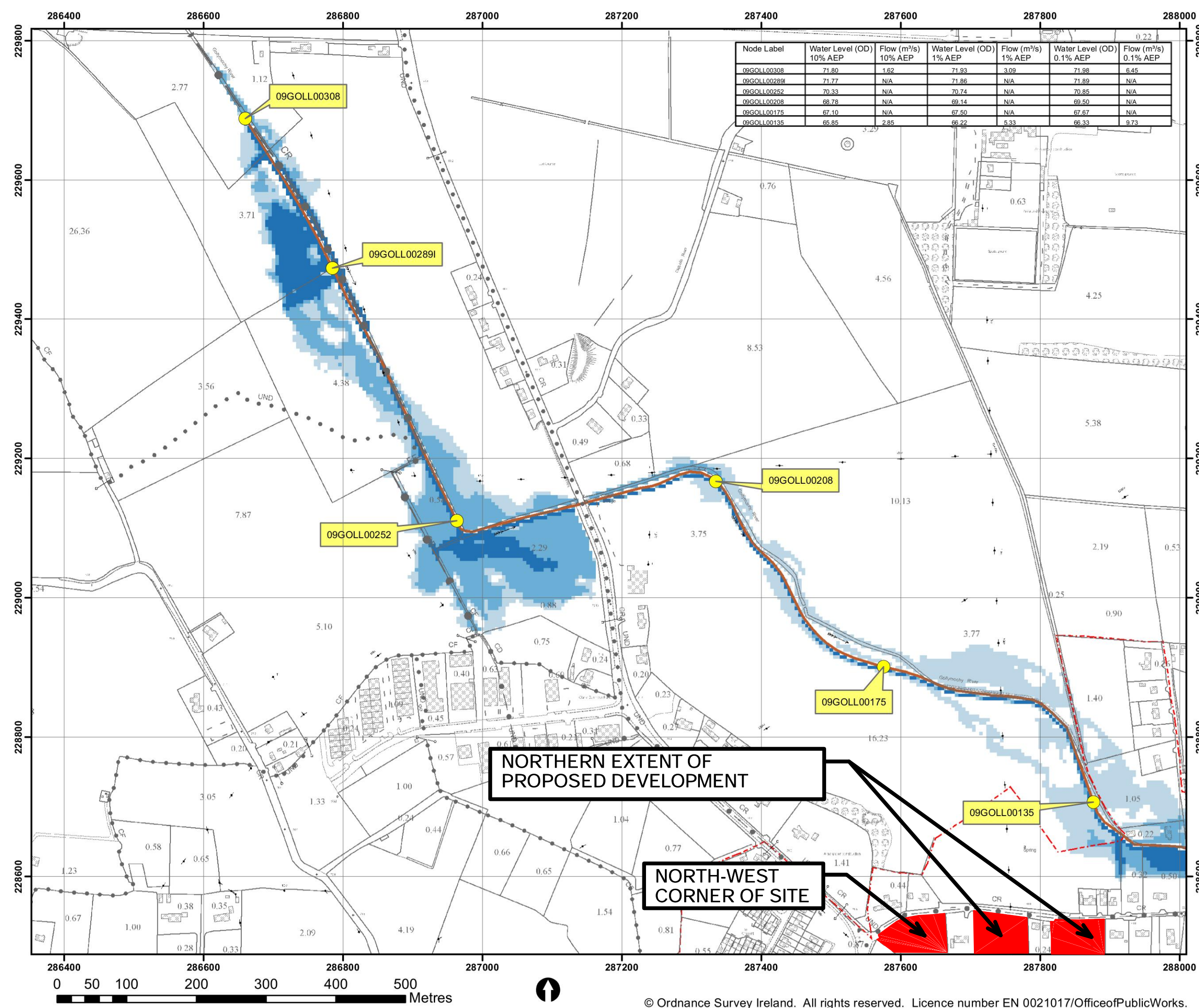
## Meeting with Area Engineer for Clane 22/03/05

The Area Engineer and his supervisor outlined 29 areas that are or were prone to flooding. These are: -

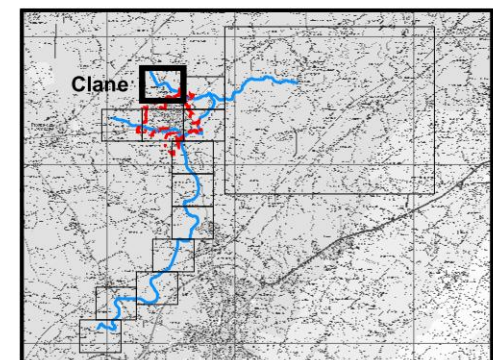
1. Newtown – River Blackwater overflows its banks after heavy rain. This occurs every year.  
Flood Id = 1272
2. Timoltan/Fanagh – Drain overflows after heavy rain every year. A property is affected. Road is liable to flooding.  
Flood Id = 1274
3. Clonshanbo – The Clonshanbo river overflows its banks after heavy rain every year. The main Clane – Kilcock road is liable to flooding and was flooded in January 2005. Road has been raised by the council.  
Flood Id = 1276
4. Staplestown at mill pond – Mill pond over flows after heavy rain a couple of times per year. County road is liable to flooding.  
Flood Id = 1277
5. Allenwood – Low lying area floods after heavy rain. Road is liable to flooding. No property is affected  
Flood Id = 1278
6. Prosperous – A property is flooded after heavy rain every year  
Flood Id = 1279
7. Killinagh – Area floods after heavy rain every year. The culvert of a stream under the Grand Canal can't take volume of water.  
Flood Id = 1280
8. Bluetown– Flooding occurs after heavy rain every year. This is due to inadequate drainage and drains being filled in by property owners  
Flood Id = 1281
9. Staplestown Bog– Road is liable to flooding after heavy rain every year.  
Flood Id = 1282
10. Killeenmore - Flood plain of Morell river and tributaries. A number of properties were flooded in November 2000 and November 2002. OPW have undertaken remedial work  
Flood Id = 1283
11. Ladyhill– River overflows its banks onto flood plain after heavy rain. Road is liable to flood.  
Flood Id = 1284
12. Commons, Clane- The Butterstream overflows its banks after heavy rain every year. A property is affected. Road is liable to flooding  
Flood Id = 1285
13. Ballycaghan – Low lying land floods every year. Road is liable to flooding  
Flood Id = 1287
14. School Street, Kilcock – Low lying land floods after heavy rain every year due to inadequate drainage  
Flood Id = 1288
15. Kilcock – Low lying land floods after heavy rain every year due to inadequate drainage  
Flood Id = 1289
16. Ryewater, Kilcock – Ryewater overflows its banks after heavy rain every year onto flood plain.  
Flood Id = 1290
17. Millicent Road, Clane – Low lying area floods after heavy rain every year due to inadequate and blocked drainage. Road is liable to flood . There has been significant development.



- Flood Id = 1291
18. Laragh– Stream overflows its banks after heavy rain every year. Road is liable to flood. This area flooded in 2005  
Flood Id = 1292
  19. Loughballard, Clane – Low lying area floods every year after heavy rain due to inadequate drainage  
Flood Id = 1293
  20. Clonfert – Property is flooded after heavy rain. Water flows off high land and stream overflows  
Flood id = 1294
  21. Carrick Hill – Low point in upland area floods after heavy rain. The council may have resolved the issue.  
Flood id = 1295
  22. Boyne Bridge, Edenderry – Flood plain of the River Boyne  
Flood Id = 1296
  23. Ballycowan – Flood plain of the River Boyne  
Flood Id = 1297
  24. Thomastown – Stream overflow its banks after significant rainfall. Last flooded November 2000  
Flood Id = 1298
  25. Calfstown – Low lying area floods after heavy rain. The garden of a Property has been flooded  
Flood Id = 1299
  26. Oldcourt Road – Water flows across road after heavy rain  
Flood Id = 1300
  27. Moyvally – Water flows off the main road into the side road after heavy rain every year  
Flood Id = 1301
  28. Carbury – Standing water in bog every winter  
Flood Id = 1302
  29. Knockanally/Dysart – Flood plain of tributaries of River Blackwater.  
Flood Id = 1303



Node Label	Water Level (OD) 10% AEP	Flow (m³/s) 10% AEP	Water Level (OD) 1% AEP	Flow (m³/s) 1% AEP	Water Level (OD) 0.1% AEP	Flow (m³/s) 0.1% AEP
09GOLL00308	71.80	1.62	71.93	3.09	71.98	6.45
09GOLL00289I	71.77	N/A	71.86	N/A	71.89	N/A
09GOLL00252	70.33	N/A	70.74	N/A	70.85	N/A
09GOLL00208	68.78	N/A	69.14	N/A	69.50	N/A
09GOLL00175	67.10	N/A	67.50	N/A	67.67	N/A
09GOLL00135	65.85	2.85	66.22	5.33	66.33	9.73



**IMPORTANT USER NOTE:**  
THE VIEWER OF THIS MAP SHOULD REFER TO THE DISCLAIMER, GUIDANCE NOTES AND CONDITIONS OF USE THAT ACCOMPANY THIS MAP.

- Legend**
- 10% Fluvial AEP Event
  - 1% Fluvial AEP Event
  - 0.1% Fluvial AEP Event
  - Modelled River Centreline
  - AFA Extents
  - Node Point
  - Node ID Node Label

**FINAL**

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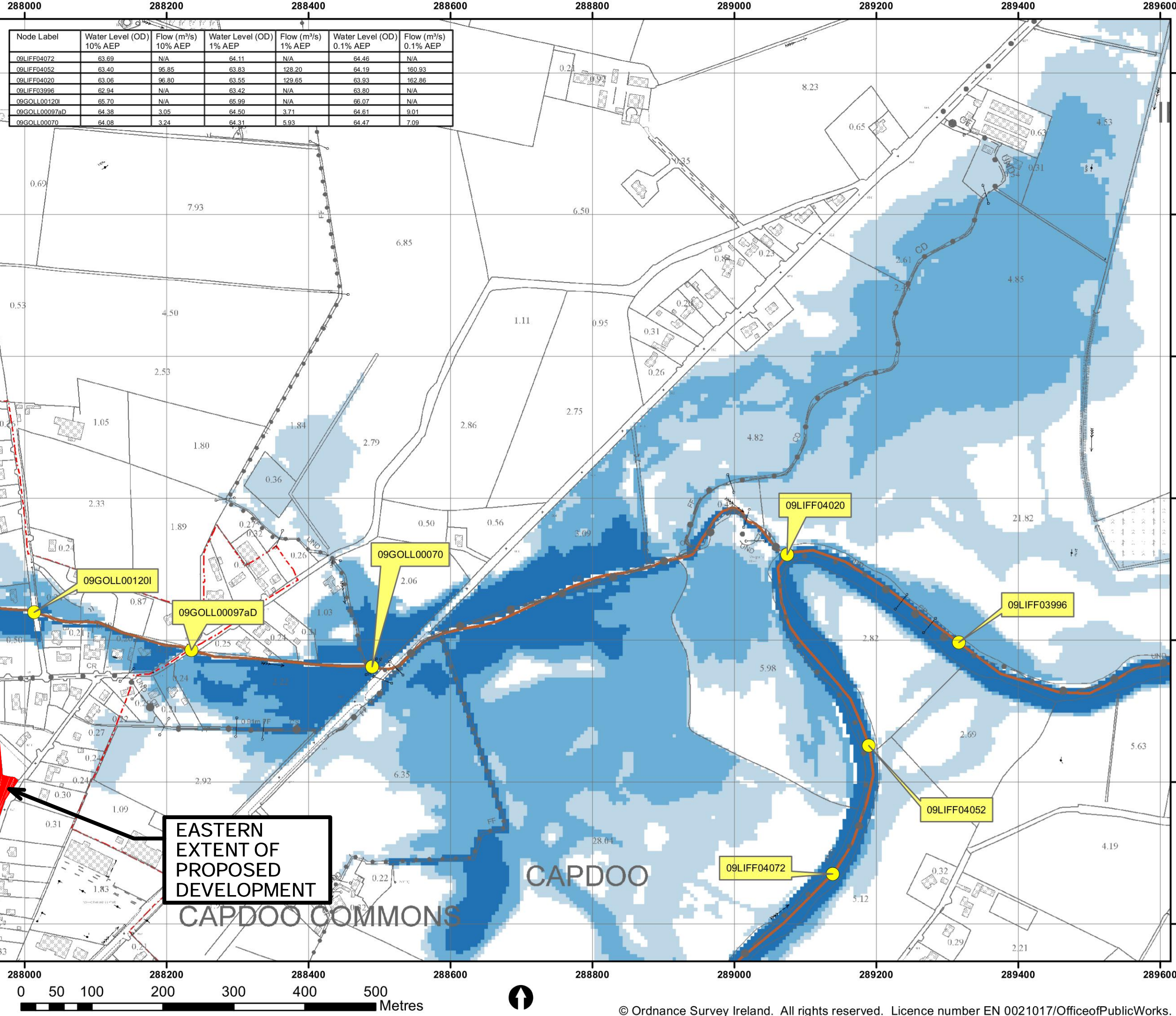


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Trim  
Co Meath

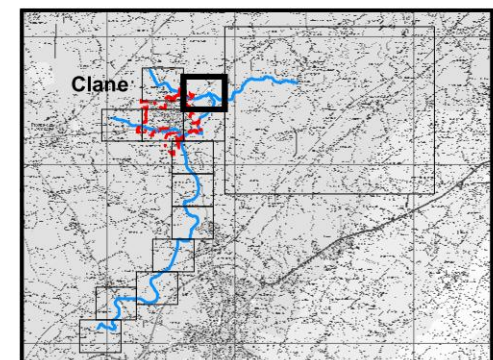
Elmwood House  
74 Boucher Road  
Belfast  
BT12 6RZ

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F +44(0) 28 90 668286  
W www.rpsgroup.com  
E ireland@rpsgroup.com

<b>Map:</b> Clane Fluvial Flood Extents	
<b>Map Type:</b> EXTENT	
<b>Source:</b> FLUVIAL	
<b>Map Area:</b> HPW	
<b>Scenario:</b> CURRENT	
<b>Drawn By:</b> C.C.	<b>Date:</b> 30 October 2017
<b>Checked By:</b> M.W.	<b>Date:</b> 30 October 2017
<b>Approved By:</b> S.P.	<b>Date:</b> 30 October 2017
<b>Drawing No.:</b> E09CLA_EXFCD_F1_11	
<b>Map Series:</b> Page 11 of 13	
<b>Drawing Scale:</b> 1:5,000 @A3	



Node Label	Water Level (OD) 10% AEP	Flow (m³/s) 10% AEP	Water Level (OD) 1% AEP	Flow (m³/s) 1% AEP	Water Level (OD) 0.1% AEP	Flow (m³/s) 0.1% AEP
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09LIFF04052	63.40	95.85	63.83	128.20	64.19	160.93
09LIFF04020	63.06	96.80	63.55	129.65	63.93	162.86
09LIFF03996	62.94	N/A	63.42	N/A	63.80	N/A
09GOLL00120I	65.70	N/A	65.99	N/A	66.07	N/A
09GOLL00097aD	64.38	3.05	64.50	3.71	64.61	9.01
09GOLL00070	64.08	3.24	64.31	5.93	64.47	7.09



**IMPORTANT USER NOTE:**  
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- Legend**
- 10% Fluvial AEP Event
  - 1% Fluvial AEP Event
  - 0.1% Fluvial AEP Event
  - Modelled River Centreline
  - AFA Extents
  - Node Point
  - Node ID
  - Node Label

**FINAL**

REV: 01	NOTE: Aquaduct was clipped from Page 4 of all maps	DATE: 30/10/17
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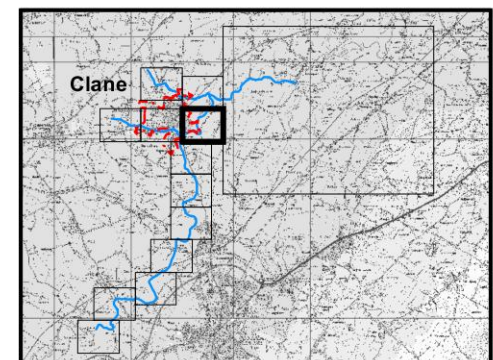
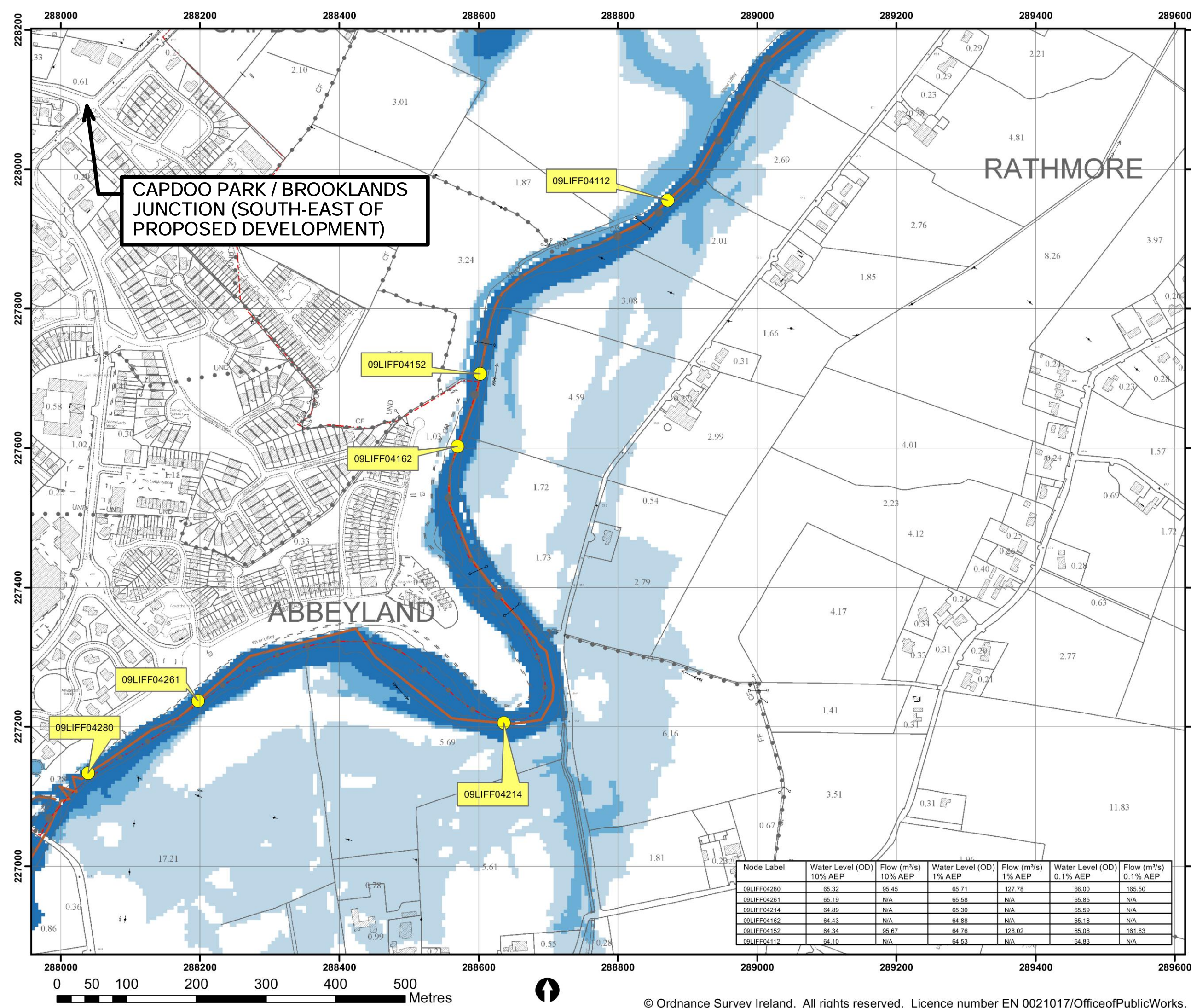


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<b>Map:</b>	
Clane Fluvial Flood Extents	
Map Type: EXTENT	
Source: FLUVIAL	
Map Area: HPW	
Scenario: CURRENT	
Drawn By: C.C.	Date: 30 October 2017
Checked By: M.W.	Date: 30 October 2017
Approved By: S.P.	Date: 30 October 2017
Drawing No.:	
E09CLA_EXFCD_F1_12	
Map Series: Page 12 of 13	
Drawing Scale: 1:5,000 @A3	



**IMPORTANT USER NOTE:**  
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- Legend**
- 10% Fluvial AEP Event
  - 1% Fluvial AEP Event
  - 0.1% Fluvial AEP Event
  - Modelled River Centreline
  - AFA Extents
  - Node Point
  - Node ID
  - Node Label

FINAL

REV: 01	NOTE: Aquaduct was clipped from Page 4 of all maps	DATE: 30/10/17
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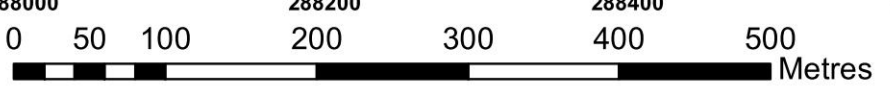
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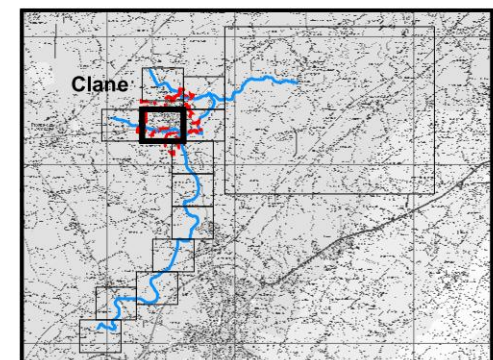
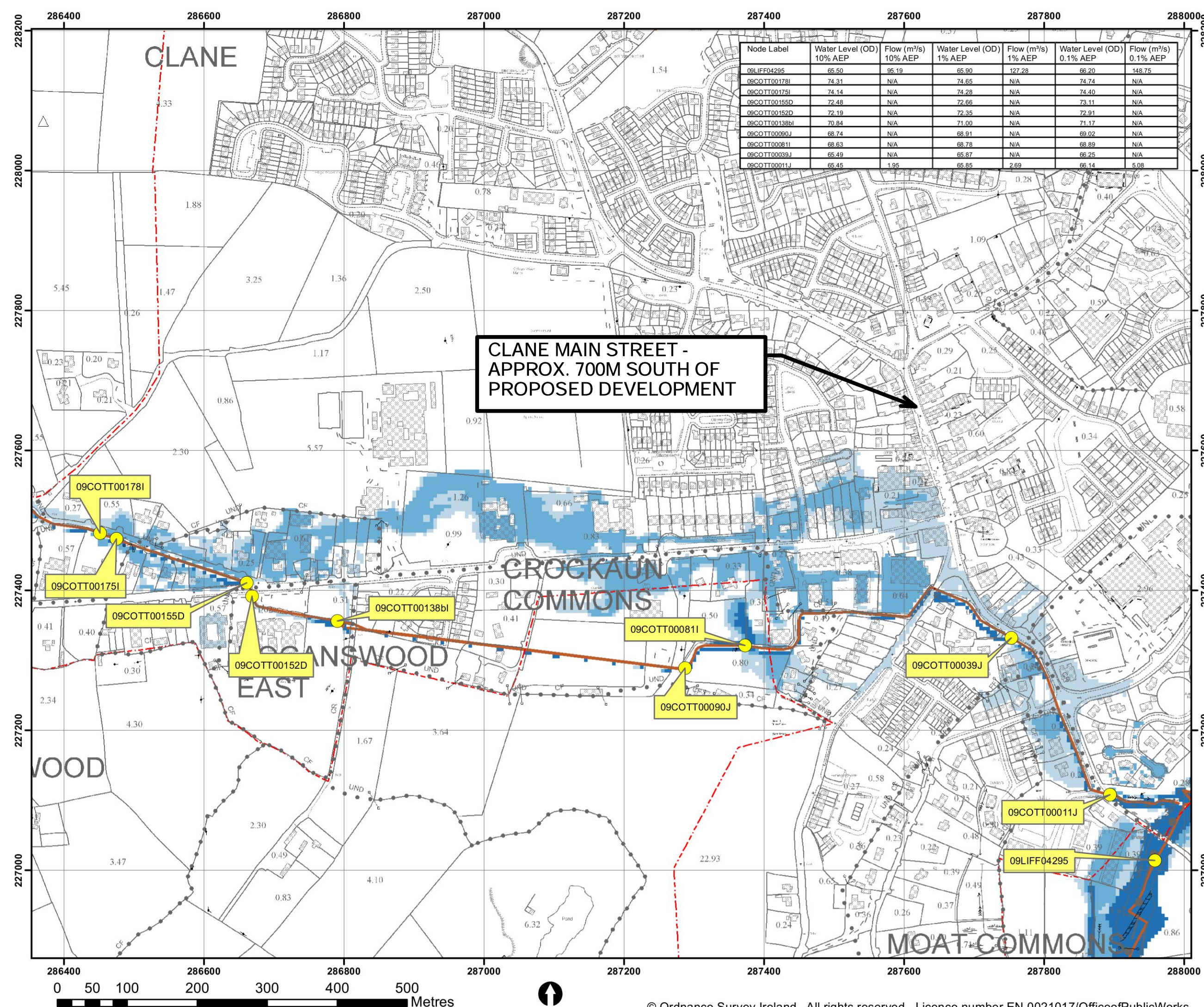
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<b>Map:</b> Clane Fluvial Flood Extents	
<b>Map Type:</b> EXTENT	
<b>Source:</b> FLUVIAL	
<b>Map Area:</b> HPW	
<b>Scenario:</b> CURRENT	
<b>Drawn By:</b> C.C.	<b>Date:</b> 30 October 2017
<b>Checked By:</b> M.W.	<b>Date:</b> 30 October 2017
<b>Approved By:</b> S.P.	<b>Date:</b> 30 October 2017
<b>Drawing No.:</b> E09CLA_EXFCD_F1_10	
<b>Map Series:</b> Page 10 of 13	
<b>Drawing Scale:</b> 1:5,000 @A3	

Node Label	Water Level (OD) 10% AEP	Flow (m <sup>3</sup> /s) 10% AEP	Water Level (OD) 1% AEP	Flow (m <sup>3</sup> /s) 1% AEP	Water Level (OD) 0.1% AEP	Flow (m <sup>3</sup> /s) 0.1% AEP
09LIFF04280	65.32	95.45	65.71	127.78	66.00	165.50
09LIFF04261	65.19	N/A	65.58	N/A	65.85	N/A
09LIFF04214	64.89	N/A	65.30	N/A	65.59	N/A
09LIFF04162	64.43	N/A	64.88	N/A	65.18	N/A
09LIFF04152	64.34	95.67	64.76	128.02	65.06	161.63
09LIFF04112	64.10	N/A	64.53	N/A	64.83	N/A





**IMPORTANT USER NOTE:**  
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**Legend**

- 10% Fluvial AEP Event
- 1% Fluvial AEP Event
- 0.1% Fluvial AEP Event
- Modelled River Centreline
- AFA Extents
- Node Point
- Node ID Node Label

**FINAL**

REV: 01	NOTE: Aquaduct was clipped from Page 4 of all maps	DATE: 30/10/17
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**Map:**  
Clane Fluvial Flood Extents

Map Type:	EXTENT
Source:	FLUVIAL
Map Area:	HPW
Scenario:	CURRENT
Drawn By:	C.C. Date: 30 October 2017
Checked By:	M.W. Date: 30 October 2017
Approved By:	S.P. Date: 30 October 2017
Drawing No.:	E09CLA_EXFCD_F1_09
Map Series:	Page 9 of 13
Drawing Scale:	1:5,000 @A3

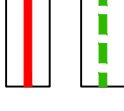




Kildare County Council  
Planning Department  
Áras Chill Dara,  
Devoy Park, Naas,  
Co Kildare.

### Clane Local Area Plan 2017 - 2023

#### Legend

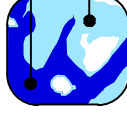


#### Local Area Plan Boundary

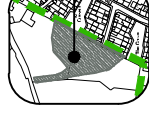
Development proposals for lands outlined thus are to be the subject of site-specific Flood Risk Assessment in accordance with the Flood Risk Management Guidelines and appropriate to the type and scale of the development being proposed.

Such Development Proposals shall also:

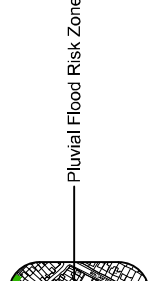
- Indicate and quantify loss of floodplain storage arising from the development proposal;
- Provide compensatory storage located within or adjacent to the proposed development;
- Indicate measures to ensure that water-vulnerable elements of the Development would not be flooded during the 1000year flood;
- Ensure that existing flow paths for flood waters will not be compromised.



Flood Risk Zone A (1.0% AEP)



Flood Risk Zone B (0.1% AEP)



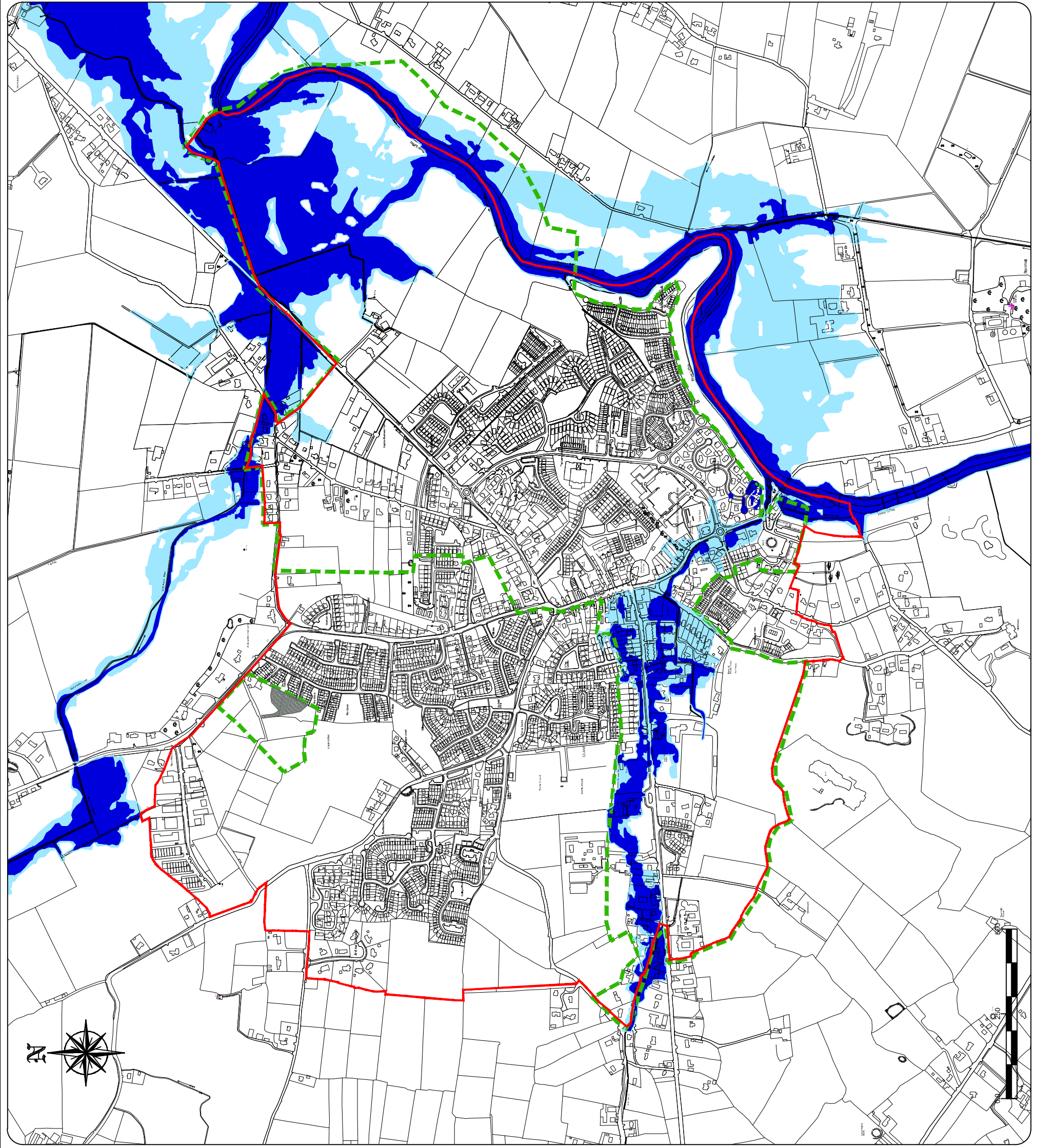
Pluvial Flood Risk Zone

Source:



### Strategic Flood Risk Assessment Recommendations

Scale:	N.T.S.	Map Ref:	9.1
Date:	June 2017 (Adopted LAP)	Drawing No.:	200/16/1000
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This drawing is to be read in conjunction with the written statement			



## APPENDIX D – IGSL SITE INVESTIGATION REPORT (EXTRACTS)

**PROPOSED HOUSING  
DEVELOPMENT  
CAPDOO CLANE  
FOR ARDSTONE**

---

**DBFL  
CONSULTING ENGS**

**CONTENTS**

<b>I</b>	<b>INTRODUCTION</b>
<b>II</b>	<b>FIELDWORK</b>
<b>III</b>	<b>TESTING</b>
<b>IV</b>	<b>DISCUSSION SUMMARY</b>

**APPENDICES**

<b>I</b>	<b>BOREHOLE RECORDS</b>
<b>II</b>	<b>TRIAL PIT RECORDS</b>
<b>III</b>	<b>PLATE BEARING TESTS</b>
<b>IV</b>	<b>DYNAMIC PROBES</b>
<b>V</b>	<b>PERCOLATION BRE DIGEST 365</b>
<b>VI</b>	<b>LABORATORY TESTS</b>
<b>VII</b>	<b>SITE LOCATION PLAN</b>



## FOREWORD

The following Conditions and Notes on Site Investigation Procedures should be read in conjunction with this report.

### General.

Recommendations made, and opinions expressed in the report are based on the strata observed in the exploratory holes, together with the results of in-situ and laboratory tests. No responsibility can be held for conditions which have not been revealed by exploratory work, or which occur between exploratory hole locations. Whilst the report may suggest the likely configuration of strata, both between exploratory hole locations, or below the maximum depth of the investigation, this is only indicative, and liability cannot be accepted for its accuracy.

Unless specifically stated, no account has been taken of possible subsidence due to mineral extraction below or close to the site.

### Boring Procedures.

Unless otherwise stated, the 'Shell and Auger' technique of soft ground boring has been employed. All boring operations sampling and/or logging of soils and in-situ testing complies with the recommendations of the British Standard Code of Practice BS 5930 (1999), 'Site Investigation' and BS 1377:1990, 'Methods of test for soils for civil engineering purposes'.

Whilst the technique allows the maximum data to be obtained in soft ground, some disturbance and variation of soft and layered soils is unavoidable. Attention is drawn to this condition, whenever it is suspected. Where cobbles and boulders are recorded, no conclusion should be drawn concerning the size, presence, lithological nature, or numbers per unit volume of ground.

Where peat has been encountered during siteworks, samples have been logged in accordance with the Von Post Classification (ref. Von Post, L. 1992. Sveriges Gologiska Undersoknings torvinventering och nogra av dess hittils vunna resultat (SGU peat inventory and some preliminary results) Svenska Mosskulturforeningens Tidskrift, Jonkoping, Swedden, 36, 1-37 & Hobbs N. B. Mire morphology and the properties of some British and foreign peats. QJEG, Vol. 19, 1986).

### **Routine Sampling.**

Undisturbed samples of soils, predominantly cohesive in nature are obtained unless otherwise stated by a 104mm diameter open-drive tube sampler. In granular soils, and where undisturbed sampling is inappropriate, disturbed samples are collected. Smaller disturbed samples are also recovered at intervals to allow a visual examination of the full strata section.

### **In-Situ Testing.**

Standard penetration tests, utilising either the standard split spoon sampler or solid cone and automatic trip-hammer are conducted unless otherwise where required by instruction. Subsequent to a seating drive of 150mm, a summation for the number of blows for 300mm penetration is recorded on the boring records together with the blow count for each 75mm penetration. In cases where incomplete penetration is obtained, the numbers of blows for the recorded value of penetration are noted. In coarse granular soils, a cone end is fitted to the sampler and a similar procedure adopted.

### **Groundwater.**

The depth of entry of any influx of groundwater is recorded during the course of boring operations. However, the normal rate of boring does not usually permit the recording of an equilibrium level for any one water strike. Where possible drilling is suspended for a period of twenty minutes to monitor the subsequent rise in water level.

Groundwater conditions observed in the borings or pits are those appertaining to the period of investigation. It should be noted however, that groundwater levels are subject to diurnal, seasonal and climatic variations and can also be affected by drainage condition, tidal variation or other causes.

### **Retention of Samples.**

After satisfactory completion of all the scheduled laboratory tests on any sample, the remaining material is discarded. Unless a period of retention of samples is agreed, it is our normal practice to discard all soil samples one month after submission of our final report.

**REPORT ON A SITE INVESTIGATION  
FOR A HOUSING DEVELOPMENT  
AT CAPDOO  
CLANE  
COUNTY KILDARE  
FOR  
ARDSTONE RESIDENTIAL  
  
DBFL CONSULTING ENGINEERS**

**Report No 20159**

**JULY 2017**

**I Introduction**

A major residential development is planned for a site located at Capdoo in Clane, County Kildare.

A comprehensive investigation of sub soil conditions in the area of development has been ordered by DBFL Consulting Engineers on behalf of Ardstone Residential Fund.

The programme of the field investigation included the construction of boreholes, trial pits and dynamic probes to establish geotechnical criteria on which to base foundation and infra-structural design. Work was carried out in accordance with BS 5930, Code of Practice for Site Investigations (1999).

In addition plate bearing tests were scheduled to determine in situ CBR values while soakaway testing was performed in several locations in accordance with BRE Digest 365.

A programme of laboratory testing to confirm geotechnical and environmental soil parameters followed site operations.

This report includes all factual data pertaining to the project and comments on the findings relative to foundation and infrastructural design.

## **II Fieldwork**

The site is predominantly a green field one located at Capdoo in Clane. A site location map and a drawing indicating the exploratory positions are enclosed in Appendix VII. This has been provided by DBFL engineers.

The various exploratory positions have been determined by DBFL and set out by the site engineer. Locations have been referenced to national grid and O.D. levels have been established.

Each location was electronically scanned to ensure that underground services were not disrupted. At borehole locations a trial pit was opened by hand to a depth of 1.20 metres to confirm this.

The scope of the field investigation included the following elements:

- \* 3 nr. Conventional Boreholes
- \* 23 nr Machine Excavated Trial Pits
- \* 20 nr. Plate Bearing Tests (In Situ CBR)
- \* 50 nr H.D. Dynamic Probes
- \* 8 nr Percolation Tests to BRE Digest 365

Following the field operations samples were selected for laboratory analysis. This included standard geotechnical testing and detailed environmental analysis carried out by specialist laboratory.

### *a. Boreholes*

The exploratory holes were bored with conventional 200mm cable-tool methods using a Dando 2000 Rig. One re-bore (BH02A) was carried out after shallow refusal in BH02.

Detailed geotechnical records are contained in Appendix I to this report - the records give details of stratification, sampling, in-situ testing and groundwater. Note is also taken of any obstructions to normal boring requiring the use of the heavy chisel for advancement.

Some variation in stratification was indicated. At BH01 surface top soil overlies a thin stratum of brown sandy gravelly CLAY. From 1.10 to 8.80 metres, medium dense to dense silty sandy GRAVEL is penetrated, with refusal noted at 8.80 metres. Ground water was observed at 4.20 metres BGL.

Boreholes BH02 and BH02A encountered stiff to very stiff brown sandy gravelly CLAY below top soil to respective refusal depths of 3.90 and 3.20 metres.

In BH03, very stiff brown gravelly CLAY extends from 0.20 to 2.20 metres with dense underlying GRAVEL 2.20 to 3.30 metres. Boulders at 3.30 metres prevented further advancement. No ground water was encountered in BH02, BH02A and BH03.

Both boreholes BH2 and BH3 were dry during the investigation period.

### *b. Trial Pits*

Trial pits were scheduled at twenty five locations. Because of access restraints TP01 and TP02 were omitted. Trial Pitting was carried out using a light tracked excavator under geotechnical engineering supervision. Samples were recovered at intervals, ground water was noted where relevant and detailed trial pit records prepared. These records are contained in Appendix II to this report with supporting photographs.

Top soil varying in thickness from 300mm to 600mm overlies the site. In the majority of trial pit locations a thin stratum of firm gravelly SILT/CLAY is then noted. This continues to depths between 1.00 and 2.00 metres. Below this stratum and directly below the top soil in some locations a stratum of silty or clayey gravelly SAND or sandy GRAVEL is found. Trial Pits continued to completion in this stratum at depths between 2.50 and 3.00 metres.

Ground water was noted in Trial Pits TP07 to TP12, associated with collapse of side walls in some instances. Some minor wall collapse was also recorded in dry non-cohesive soils.

### *c. Plate Bearing Tests*

In situ CBR values were established by Plate Bearing Test at twenty one specified locations. Testing was carried out directly below the top-soil zone at a depth of approximately 0.50 metres. Test locations were referenced CBR05 to CBR25. Four locations CBR01 to CBR04 were not accessible.

A 450mm diameter steel plate is loaded incrementally and deflection is recorded. The plate is then off loaded and recovery measured (Load Cycle). The process is then repeated (Re-Load Cycle).

The equivalent CBR value is calculated for both cycles. Detailed individual results are presented in Appendix III and the data is summarised in the following table.

**TABLE A CBR SUMMARY DATA**

<b>Test No.</b>	<b>CBR at Load Cycle (%)</b>	<b>CBR at RE-Load (%)</b>
05	54.9	68.7
06	2.8	3.7
07	1.5	3.4
08	0.2	0.2
09	1.0	1.5
10	3.7	5.0
11	5.1	7.1
12	2.5	3.6
13	1.0	3.1
14	N/A	N/A
15	4.3	6.1
16	1.2	3.1
17	2.6	5.5
18	4.1	6.0
19	8.1	9.8
20	1.2	2.2
21	1.4	3.9
22	2.5	10.0
23	1.1	2.6
24	1.0	1.7
25	1.6	4.6

The high CBR values noted at locations CBR05 and CBR 19 may reflect coarse dry surface material. The results over the remainder of the site reflect average CBR values on load cycle of 2.3% with an average CBR value of 3.6 % on reload.

A design CBR value of 3% would be appropriate for this site.

*d. Dynamic Probes*

Probing was scheduled at fifty locations to establish a pattern of soil strength with depth. Access was restricted at DP01 and DP02 and these probes were omitted. Forty-eight probes were completed.

Probing was in accordance with the heavy-duty probe specification of BS 1377: Part 9: 1990. In these tests, the soil resistance is measured in terms of the number of drop-hammer blows required to drive the test probe through each 100 mm increment of penetration. Probing is terminated when the blow count exceeds 25/100mm to avoid damage to the apparatus. Where loose material is present a single blow count may drive the apparatus in excess of 100mm. In this instance blow counts of zero may be recorded.

Some variation in probe resistances and associated soil strength were observed. Soft zones (defined by  $N_{100}$  values  $< 1$ ) were noted in several locations. A dynamic probe resistance of  $N_{100} = 3$  (with no dramatic underlying deterioration) would be the normal minimum requirement for conventional two storey house foundations.

Probe results are summarised with the depth to  $N_{100} = 3$  indicated as well as soft unsuitable zones. Final probe refusal depths are also indicated, these depths are not indicative of rock horizon.

<b>Probe No.</b>	<b>Soft Zones</b>	<b>Depth to N<sub>100</sub> = 3</b>	<b>Final Depth</b>
DP03	0 – 0.30	0.30	1.00
DP04	0.80 – 1.30	1.70	3.20
DP05	0 – 0.20	0.30	1.40
DP06	0.80 – 1.90	2.20	2.60
DP07	0 – 1.80	2.00	2.40
DP08	0 – 1.60	1.70	2.70
DP09	0 – 0.20	0.60	3.10
DP10	0 – 0.30	0.70	3.60
DP11	0 – 0.10	0.30	1.70
DP12	0.80 – 1.40	1.60	2.50
DP13	0 – 0.80	0.90	5.00
DP14	0 – 1.10	1.20	1.50
DP15	0 – 0.20	0.50	2.00
DP16	0 – 0.30	0.60	2.50
DP17	0 – 1.80	1.90	5.00
DP18	0 – 1.60	1.70	2.90
DP19	0 – 0.50	0.60	3.60
DP20	1.80 – 2.40	0.70	3.60
DP21	0 – 0.20	0.40	1.50
DP22	0 – 0.20	0.40	3.50
DP23	0 – 1.80	2.00	4.80
DP24	0 – 1.50	1.70	5.00
DP25	0 – 0.20	0.40	2.60
DP26	0 – 0.20	0.40	2.00
DP27	0 – 0.20	0.50	5.00
DP28	0 – 1.00	1.20	1.60
DP29	0 – 0.50	1.00	4.00
DP30		0.70	3.50
DP31	0 – 0.30	0.70	4.80
DP32		1.20	2.60
DP33	0 – 0.60	0.80	2.60
DP34	0 – 0.20	0.40	5.00
DP35		0.40	1.20
DP36	0 – 0.80	1.00	5.00
DP37	0 – 0.50	1.20	3.70
DP38	0 – 1.40	1.50	2.60
DP39	0 – 1.30	1.40	5.00
DP40	0 – 0.40	1.00	5.00
DP41	0 – 0.30	0.50	5.00
DP42	0 – 0.70	1.00	2.80
DP43	0 – 0.80	1.00	2.00
DP44	0 – 0.20	0.80	1.40
DP45	0 – 1.00	1.20	3.40
DP46	0 – 0.20	0.60	2.40
DP47	0 – 0.40	0.70	1.20
DP48	0 – 0.40	1.00	2.00
DP49	0 – 0.50	0.60	3.00
DP50	0 – 1.50	1.70	4.90



e. BRE Digest 365 Soakaway

A total of eight percolation tests were scheduled.

Infiltration testing was performed in accordance with BRE Digest 365 'Soakaway Design'. To obtain a measure of the infiltration rate of the sub-soils, water is poured into the test pit, and records taken of the fall in water level against time. This operation is generally performed over two cycles of soakage and dispersion following initial soakage.

The infiltration rate is the volume of water dispersed per unit exposed area per unit of time, and is generally expressed as metres/minute or metres/second. In these calculations the exposed area is the sum of the base area and the average internal area of the pit sides over the test duration.

Records for each test are presented in Appendix V. The stratification and water table in each test pit is noted and a record of fall in water level with time is made.

Designs are based on the slowest infiltration rate, which is generally calculated from the final cycle. The infiltration rate (f) is calculated and the results for the individual tests indicate that the soils in the test areas are relatively impermeable with little or no infiltration recorded.

The results reflect the variation in ground conditions over the site area. In two locations a high water table was noted, precluding completion of the test. Impermeable clay matrix soils were also encountered and some percolation was achieved in the more granular soils.

The Infiltration Rate (f) for each location with brief comment is noted as follows:

Test No.	Infiltration Rate (f) (metres / min)	Comment
IT01	0.00000	Silt/Clay
IT02	0.00054	Silty SAND
IT03	0.00163	SAND
IT04	0.00094	Silty SAND
IT05	No Test Possible	Water Table @ 1.30m
IT06	No Test Possible	Water Table @ 0.90m
IT07	0.00238	Sandy GRAVEL
IT08	0.00014	Silty SAND

### **III Testing**

#### ***(a) In-Situ :***

Standard penetration tests were carried out at approximate 1.00 metre intervals in the geotechnical boreholes to measure relative in-situ soil strength. N values are noted in the right hand column of the boring records, representing the blow count required to drive the standard sampler 300mm into the soil, following initial seating blows. Where full test penetration was not achieved the blow count for a specific penetration is recorded, or refusal is indicated where appropriate

The results of the tests are summarised as follows:

<b>STRATUM</b>	<b>N VALUE RANGE</b>	<b>COMMENT</b>
Sandy GRAVEL	12 to 52	Medium Dense to Dense
Gravelly CLAY	23 to 32	Stiff

In several instances refusal of SPT apparatus was noted, probably on boulder obstructions and results are presented as blows for specific penetration and refusal.

#### ***(b) Geotechnical and Environmental Laboratory :***

All samples from the boreholes and trial pits have been returned to the IGSL laboratory for initial visual inspection, a schedule of testing was prepared and tests as appropriate carried out. The programme of testing included the following elements and all results are presented in Appendix VI.

- a. Moisture Content and Classification (Liquid and Plastic Limits)
- b. Particle size distribution (Sieve Analysis / Hydrometer)
- c. Sulphate and pH determination.
- d. RILTA Environmental Suite

Geotechnical testing was carried out by IGSL in it's INAB accredited facility. Chemical and environmental testing was carried out by Chemtest Limited in their UKAS laboratory.

### *Classification*

The liquid and plastic limits were established for several samples of the upper cohesive soils. Results reflect variation from clay matrix to silt matrix material, essentially material of similar origin. Moisture contents range from 9 to 18% and the material is of low plasticity and sensitivity to moisture content variation.

### *Grading*

Grading tests were carried out on the main soil strata using wet sieve and hydrometer analysis as appropriate.

The grading curves reflect the variation in soil type over the site area. Clean sandy GRAVEL, finer silty SAND, gravelly SILT and gravelly CLAY have all been identified.

### *Sulphate and pH.*

Three samples were selected for sulphate and pH analysis. Sulphate concentrations (SO<sub>4</sub> 2:1 extract) of from 0.010 to 0.017 g/l were established with an average pH of 8.3. No special precautions are necessary to protect foundation concrete from sulphate aggression. A sulphate design class of DS-1 (ACEC Classification for Concrete) is indicated for concentrations less than 0.5 g/l.

### *Environmental*

Two soil samples were submitted for detailed environmental analysis to RILTA (WAC) parameters.

The results indicate that the soils can be classified as INERT with little or no elevated contaminant levels recorded. Material excavated from this site can be readily disposed of to a regular licensed landfill facility and no problems are anticipated with personnel operating on the site.

## **IV Discussion**

The proposed residential development is for traditional housing on a site located at Capdoo in Clane, County Kildare.

The area is an undulating greenfield one with ground level varying from about 67.00 to 80.00 OD. Access to part of the site was restricted and a number of scheduled Trial Pits, CBR Tests and Probes were omitted following consultation with the client and engineer.

A comprehensive investigation of ground conditions has been carried out on the instructions of DBFL involving Borehole and Trial Pit investigation with supporting Dynamic Probes, Plate Bearing Tests and Percolation Tests.

It is assumed that the development will as far as possible follow existing contours, however some cut and fill operations may be required.

Ground water was noted at approximately 4.00 metres in one of the boreholes and in rare trial pits generally below 1.00 metres.

### **Foundations:**

Soil strength has been determined by SPT tests in the three boreholes and by Dynamic Probe resistance in the fifty locations examined. Visual assessment of soil strength in the trial pits has also been used in assessing allowable bearing parameters.

Standard penetration tests in boreholes at 1.00 metre BGL were in excess of  $N = 20$ . This would suggest an allowable bearing pressure of 150 kN/sq.m. based on the lowest SPT value.

A Dynamic Probe resistance of  $N_{100} = 3$  with an increasing underlying strength trend will permit an allowable bearing pressure of 100 kN/sq.m. Similarly a probe resistance of  $N_{100} = 5$  will equate to 150 kN/sq.m.

Based on the data obtained we would suggest the use of traditional reinforced strip or pad foundations, founded at approximately 1.00 metre BGL and using an allowable bearing pressure of 100 kPa. This scenario will be applicable over most of the site. In about ten probe locations soft or weak soils were noted to depths in excess of the normal 1.00 metre. The relevant probes are DPs 4,6,7,8,12,17,18,23, 24 and 50. Apart from Probe 50, these are generally located in the northern section of the site.

Careful visual assessment of excavated formation will be essential to accurately define the soft zones which should be removed and replace with lean mix concrete up to base of reinforced foundation.

It is quite likely that variation from granular to cohesive soils will occur over relatively short distances. Ideally individual structures (detached or semi-detached) should be founded on similar material to ensure that differential settlement is avoided.

Settlement of foundations under the indicated loads will be of the order of 10 to 15mm. In the mainly granular soils settlement should be relatively rapid. Settlement in the clay soils will be more long term.

Well-reinforced foundations will assist in bridging any local discontinuities in the formation soils.

### **Ground Floor Slabs**

The sub soils below the top-soil at a depth of about 0.50 metres should readily support lightly loaded ground floor slabs. All organic soils and all FILL material should be removed and imported hardcore infill should fully comply with current building regulations.

### **Excavation**

Ground water was not observed at proposed foundation depth and should not be of concern in shallow excavation. While trial pit excavations remained stable over the short term of the investigation, some instability may occur in longer term excavations.

Some ground water may however be encountered in deep service trench excavations.

*Statutory safety regulations prohibit personnel entering unsupported excavations greater than 1.20 metre deep, irrespective of apparent stability.*

### **Roads and Pavements**

CBR tests at shallow depth indicate an average CBR of about 3%. Excavated road or pavement formation should be inspected to ensure that all organic or unsuitable material is removed.

### **Percolation**

The variation in soil type over the site area has been outlined in the detailed test sheets with low percolation noted in clay based soils and test failure where high water table is present. Infiltration tests in the granular soils indicate that it should be suitable for dispersion of surface water.

## **Concrete**

Tests indicates low sulphate concentration (< 0.017 g/l) and pH of 8.3. The results indicate a design classification of DS-1 (ACEC Classification). No special precautions are deemed necessary to protect foundation concrete.

## **Environmental**

Tests carried out on samples from this site indicate that the soils can be classified as INERT with extremely low contamination levels.

Material excavated from this site can be disposed of to licensed landfill or utilised within the site for non-engineering purposes, landscaping etc.

## **SUMMARY**

Conventional shallow reinforced strip or pad foundations are recommended for this housing development with allowable bearing pressures as follows:

100 kPa for foundations placed at about 1.00 metre BGL using a dynamic probe resistance of  $N_{100} = 3$  as a baseline. In areas where soft deposits occur depth of excavation to a suitable formation will increase. In these areas lean mix concrete can be used as backfill up to underside of main foundation.

Variation in founding medium from cohesive material (gravelly CLAY or SILT) to non-cohesive (SAND / GRAVEL) to intermixed zones (gravelly CLAY / clayey GRAVEL) can be expected over the site area.

IGSL/JC  
July 2017

## **Appendix II    Trial Pit Records**



# TRIAL PIT RECORD

**REPORT NUMBER**

**20159**

<b>CONTRACT</b> Capdoo, Clane		<b>TRIAL PIT NO.</b> TP03	
<b>LOGGED BY</b> L. Daniels		<b>SHEET</b> Sheet 1 of 1	
<b>CLIENT</b> Ardstone		<b>DATE STARTED</b> 15/06/2017	
<b>ENGINEER</b> DBFL		<b>DATE COMPLETED</b> 15/06/2017	
<b>CO-ORDINATES</b> 687,618.36 E 728,452.58 N		<b>EXCAVATION METHOD</b> 3.5 Ton Excavator	
<b>GROUND LEVEL (m)</b> 79.46			

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly SILT/CLAY. Gravel is fine to medium subangular to subrounded.		0.30	79.16						
	Brown silty fine to coarse subangular to subrounded GRAVEL with a medium cobble content and a low boulder content. Cobbles are subangular to rounded.		0.60	78.86						
1.0						AA78690	B	0.80		
	Grey to black sandy fine to coarse subrounded GRAVEL.		1.70	77.76						
2.0						AA78691	B	1.80		
	Grey slightly gravelly fine to medium SAND. Gravel is fine to coarse subangular to subrounded.		2.40	77.06						
						AA78692	B	2.50		
3.0	End of Trial Pit at 3.00m		3.00	76.46						

**Groundwater Conditions**

**Stability**

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL.GDT 3/7/17





# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP04
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,669.68 E 728,454.80 N
	<b>DATE STARTED</b> 15/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 75.82
<b>ENGINEER</b> DBFL	<b>DATE COMPLETED</b> 15/06/2017
	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly SILT/CLAY. Gravel is fine to medium subangular to subrounded.		0.30	75.52		AA78693	B	0.50		
1.0	Brown silty fine to coarse subangular to subrounded GRAVEL with a medium cobble content and a low boulder content. Cobbles are subangular to rounded.		1.00	74.82		AA78694	B	1.20		
2.0	Stiff brown gravelly SILT/CLAY with a medium cobble content and a low boulder content. Gravel is fine to coarse subangular. Cobbles are subrounded. Boulders up to 400mm subrounded. End of Trial Pit at 2.00m		1.90	73.92		AA78695	B	1.90		
2.00			2.00	73.82						
3.0										

**Groundwater Conditions**

**Stability**

**General Remarks**



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP05
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,727.70 E 728,443.79 N
	<b>DATE STARTED</b> 15/06/2017
	<b>DATE COMPLETED</b> 15/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 73.07
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
0.60	Grey slightly silty fine to coarse SAND.		0.60	72.47		AA67769	B	0.60		
1.60	Grey silty gravelly fine to coarse SAND. Gravel is fine to coarse subangular to subrounded.		1.60	71.47		AA67770	B	1.60		
2.50	End of Trial Pit at 2.50m		2.50	70.57		AA67771	B	2.50		

**Groundwater Conditions**

**Stability**

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL.GDT 3/7/17



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP06	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,753.62 E 728,441.59 N	<b>DATE STARTED</b> 15/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 71.06	<b>DATE COMPLETED</b> 15/06/2017
<b>ENGINEER</b> DBFL		<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
0.50	Grey slightly silty fine to coarse SAND.		0.50	70.56		AA67766	B	0.60		
1.90	Grey gravelly cobbly fine to coarse SAND. Gravel is fine to coarse subrounded. Cobbles are subrounded.		1.90	69.16		AA67767	B	1.80		
2.50	End of Trial Pit at 2.50m		2.50	68.56		AA67768	B	2.50		

**Groundwater Conditions**

**Stability**

**General Remarks**



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP07
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,774.50 E 728,496.33 N
	<b>DATE STARTED</b> 15/06/2017
	<b>DATE COMPLETED</b> 15/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 69.55
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Brown to grey silty fine to coarse subangular to subrounded GRAVEL with a medium cobble content.		0.30	69.25		AA78667	B	0.50		
1.0	Grey slightly gravelly medium SAND. Gravel is fine subangular.		1.30	68.25		AA78668	B	1.40		
2.0	Black slightly gravelly fine to medium SAND. Gravel is fine subangular.		2.00	67.55		AA78669	B	2.50		
3.0	End of Trial Pit at 3.00m		3.00	66.55						

**Groundwater Conditions**  
Slow seepage at 2.0m

**Stability**

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL.GDT 3/7/17



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP08	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,770.37 E 728,541.91 N	<b>DATE STARTED</b> 15/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 68.38	<b>DATE COMPLETED</b> 15/06/2017
<b>ENGINEER</b> DBFL		<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Soft to firm light brown slightly gravelly SILT/CLAY. Gravel is fine to medium subrounded.		0.30	68.08		AA78664	B	0.50		
	Grey slightly gravelly fine to medium SAND. Gravel is fine to coarse subangular to subrounded.		0.80	67.58		AA78665	B	0.90		
1.0	Grey to black slightly gravelly medium to coarse SAND. Gravel is fine subangular.		1.40	66.98		AA78666	B	1.60		
2.0	End of it due to wall collapse. End of Trial Pit at 2.20m		2.20	66.18						
3.0										

**Groundwater Conditions**  
Slow seepage at 1.4m

**Stability**  
Wall collapse from 1.4m

**General Remarks**



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP09
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,813.53 E 728,508.36 N
	<b>DATE STARTED</b> 15/06/2017
	<b>DATE COMPLETED</b> 15/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 67.21
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Stiff dark brown very gravelly slightly sandy SILT/CLAY. Gravel is fine to coarse subangular to subrounded.		0.30	66.91						
						AA78662	B	0.50		
1.0	Dark grey clayey sandy fine to coarse subangular to subrounded GRAVEL.		1.20	66.01		AA78663	B	1.20		
	End of pit due to wall collapse. End of Trial Pit at 1.50m		1.50	65.71						
2.0										
3.0										

**Groundwater Conditions**  
Moderate seepage at 0.8m

**Stability**  
Wall collapse from 1.2m

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL\_GDT 3/7/17



# TRIAL PIT RECORD

**REPORT NUMBER**  
**20159**

<b>CONTRACT</b> Capdoo, Clane		<b>TRIAL PIT NO.</b> <b>TP10</b>	
<b>LOGGED BY</b> L. Daniels		<b>SHEET</b> Sheet 1 of 1	
<b>CLIENT</b> Ardstone		<b>DATE STARTED</b> 15/06/2017	
<b>ENGINEER</b> DBFL		<b>DATE COMPLETED</b> 15/06/2017	
<b>CO-ORDINATES</b> 687,818.29 E 728,452.90 N		<b>EXCAVATION METHOD</b> 3.5 Ton Excavator	
<b>GROUND LEVEL (m)</b> 67.74			

	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly sandy SILT/CLAY. Sand is fine to medium. Gravel is fine to medium subangular to subrounded.		0.30	67.44						
	Grey to light brown gravelly medium to coarse SAND. Gravel is fine to coarse subangular to subrounded of limestone.		0.60	67.14		AA78655	B	0.50		
						AA78656	B	0.70		
1.0	Firm grey to light brown sandy gravelly SILT with a low cobble content. Sand is fine to medium. Gravel is fine to coarse subangular to subrounded of limestone. Cobbles are subrounded of limestone.		1.00	66.74		AA78657	B	1.20		
	Stiff dark brown gravelly CLAY with a medium cobble content and a low boulder content. Gravel is medium to coarse subrounded. Cobbles are subrounded. Boulders up to 400mm subrounded.		1.50	66.24						
	Black fine subrounded to subangular sandy GRAVEL.		1.70	66.04		AA78658	B	1.60		
2.0	End of pit due to groundwater. End of Trial Pit at 2.30m		2.30	65.44						
3.0										

**Groundwater Conditions**  
Groundwater at 2.0m

**Stability**

**General Remarks**



# TRIAL PIT RECORD

**REPORT NUMBER**  
**20159**

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP11
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,869.45 E 728,445.76 N
	<b>DATE STARTED</b> 14/06/2017
	<b>DATE COMPLETED</b> 14/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 68.02
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Grey to light brown gravelly medium to coarse SAND. Gravel is fine to coarse subangular to subrounded of limestone.		0.40	67.62		AA78659	B	0.50		
	Stiff dark brown very gravelly slightly sandy SILT/CLAY. Gravel is fine to coarse subangular to subrounded.		0.70	67.32		AA78660	B	0.80		
1.0										
	Black gravelly coarse SAND. Gravel is fine to medium.		1.40	66.62		AA78661	B	1.50		
2.0	End of pit due to wall collapse. End of Trial Pit at 2.00m		2.00	66.02						
3.0										

**Groundwater Conditions**  
Moderate seepage at 1.4m

**Stability**  
Wall collapse from 1.4m

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL.GDT 3/7/17





# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP12
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,784.26 E 728,411.11 N
	<b>DATE STARTED</b> 14/06/2017
	<b>DATE COMPLETED</b> 14/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 69.03
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly sandy SILT/CLAY. Sand is fine to medium. Gravel is fine to medium subangular to subrounded.		0.40	68.63		AA78651	B	0.50		
1.0	Firm grey to light brown sandy gravelly SILT with a low cobble content. Sand is fine to medium. Gravel is fine to coarse subangular to subrounded of limestone. Cobbles are subrounded of limestone.		0.90	68.13		AA78652	B	1.00		
	Stiff dark brown gravelly CLAY with a medium cobble content and a low boulder content. Gravel is medium to coarse subrounded. Cobbles are subrounded. Boulders up to 400mm subrounded.		1.50	67.53		AA78653	B	1.60		
2.0	Dark brown to black fine to coarse subrounded to subangular GRAVEL with a medium cobble content and a low boulder content. Cobbles are subrounded. Boulders up to 400mm subrounded.		2.00	67.03		AA78654	B	2.00		
	End of pit due to groundwater. End of Trial Pit at 2.50m		2.50	66.53						
3.0										

**Groundwater Conditions**  
Groundwater at 2.2m

**Stability**

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL.GDT 3/7/17



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP13
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,675.92 E 728,416.81 N
	<b>DATE STARTED</b> 14/06/2017
	<b>DATE COMPLETED</b> 14/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 75.27
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly SILT/CLAY. Gravel is fine to medium subangular to subrounded.		0.30	74.97						
	Brown silty fine to coarse subangular to subrounded GRAVEL with a medium cobble content and a low boulder content. Cobbles are subangular to rounded.		0.60	74.67		AA78696	B	0.50		
1.0										
						AA78697	B	1.20		
2.0										
	Black sandy fine to coarse subounded to rounded GRAVEL.		2.50	72.77		AA78698	B	2.50		
3.0	End of Trial Pit at 2.50m		3.00	72.27						

**Groundwater Conditions**

**Stability**

**General Remarks**



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP14
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,623.19 E 728,411.99 N
	<b>DATE STARTED</b> 14/06/2017
	<b>DATE COMPLETED</b> 14/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 78.03
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly SILT/CLAY. Gravel is fine to medium subangular to subrounded.		0.40	77.63		AA78686	B	0.60		
1.0	Brown silty fine to coarse subangular to subrounded GRAVEL with a medium cobble content and a low boulder content. Cobbles are subangular to rounded.		0.90	77.13		AA78687	B	1.20		
2.0	Grey sandy fine to coarse subrounded GRAVEL.		2.30	75.73		AA78688	B	2.00		
						AA78689	B	2.50		
3.0	End of Trial Pit at 3.00m		3.00	75.03						

**Groundwater Conditions**

**Stability**

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL.GDT 3/7/17



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP15
<b>LOGGED BY</b> L. Daniels	<b>SHEET</b> Sheet 1 of 1
<b>CLIENT</b> Ardstone	<b>DATE STARTED</b> 14/06/2017
<b>ENGINEER</b> DBFL	<b>DATE COMPLETED</b> 14/06/2017
<b>CO-ORDINATES</b> 687,619.03 E 728,356.62 N	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator
<b>GROUND LEVEL (m)</b> 76.61	

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
0.40	Firm brown slightly gravelly SILT/CLAY. Gravel is fine to medium subangular to subrounded.		0.40	76.21		AA78679	B	0.60		
1.40	Black gravelly coarse SAND. Gravel is fine to medium.		1.40	75.21		AA78680	B	1.60		
2.80	End of pit due to wall collapse. End of Trial Pit at 2.80m		2.80	73.81		AA78681	B	2.80		

**Groundwater Conditions**

**Stability**  
Minor wall collapse from 1.4m

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL.GDT 3/7/17



# TRIAL PIT RECORD

**REPORT NUMBER**  
**20159**

<b>CONTRACT</b> Capdoo, Clane		<b>TRIAL PIT NO.</b> <b>TP16</b>	
<b>LOGGED BY</b> L. Daniels		<b>SHEET</b> Sheet 1 of 1	
<b>CLIENT</b> Ardstone		<b>DATE STARTED</b> 14/06/2017	
<b>ENGINEER</b> DBFL		<b>DATE COMPLETED</b> 14/06/2017	
<b>CO-ORDINATES</b> 687,667.37 E 728,360.19 N		<b>EXCAVATION METHOD</b> 3.5 Ton Excavator	
<b>GROUND LEVEL (m)</b> 74.06			

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly SILT/CLAY. Gravel is fine to medium subangular to subrounded.		0.40	73.66		AA78682	B	0.60		
	Brown silty fine to coarse subangular to rounded GRAVEL with a medium cobble content and a low boulder content. Cobbles are subrounded to rounded.		0.80	73.26		AA78683	B	1.20		
1.0										
2.0										
	End of pit due to boulder. End of Trial Pit at 2.70m		2.70	71.36		AA78684	B	2.50		
3.0										

**Groundwater Conditions**

**Stability**

**General Remarks**



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP17
<b>LOGGED BY</b> L. Daniels	<b>SHEET</b> Sheet 1 of 1
<b>CLIENT</b> Ardstone	<b>DATE STARTED</b> 14/06/2017
<b>ENGINEER</b> DBFL	<b>DATE COMPLETED</b> 14/06/2017
<b>CO-ORDINATES</b> 687,724.68 E 728,357.77 N	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator
<b>GROUND LEVEL (m)</b> 71.69	

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
0.40	Grey silty fine to coarse rounded to subangular GRAVEL with a medium cobble content. Cobbles are subrounded to rounded.		0.40	71.29		AA78672	B	0.60		
2.00	Grey slightly gravelly fine to coarse SAND. Gravel is fine to medium subrounded.		2.00	69.69		AA78673	B	2.00		
3.00	End of Trial Pit at 3.00m		3.00	68.69		AA78674	B	3.00		

**Groundwater Conditions**

**Stability**

**General Remarks**

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# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP18
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,776.84 E 728,364.82 N
	<b>DATE STARTED</b> 14/06/2017
	<b>DATE COMPLETED</b> 14/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 69.26
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly SILT/CLAY. Gravel is fine to medium subangular to subrounded.		0.40	68.86		AA78670	B	0.50		
1.0	Grey to brown silty fine to coarse subangular to angular GRAVEL with a medium cobble content and a low boulder content. Cobbles subangular to subrounded. Boulders up to 400mm subrounded.		0.90	68.36		AA78671	B	1.10		
2.0	End of pit due to boulder. End of Trial Pit at 2.00m		2.00	67.26						
3.0										

**Groundwater Conditions**

**Stability**

**General Remarks**

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# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP19
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,729.97 E 728,319.16 N
	<b>DATE STARTED</b> 16/06/2017
	<b>DATE COMPLETED</b> 16/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 71.49
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Dark grey to black fine to coarse SAND.		0.60	70.89		AA78675	B	0.80		
1.0										
	Black sandy fine to coarse subounded to rounded GRAVEL with a low cobble content. Cobbles are subounded.		1.50	69.99		AA78676	B	1.60		
2.0										
	End of pit due to wall collapse. End of Trial Pit at 2.60m		2.60	68.89						
3.0										

**Groundwater Conditions**

**Stability**  
Wall collapse from 1.5m

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL.GDT 3/7/17





# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP20
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,622.57 E 728,313.25 N
	<b>DATE STARTED</b> 16/06/2017
	<b>DATE COMPLETED</b> 16/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 74.42
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly SILT/CLAY. Gravel is fine to medium subangular to subrounded.		0.50	73.92						
			0.70			AA78677	B	0.70		
1.0	Brown silty fine to coarse subrounded to angular GRAVEL.		0.90	73.52						
			1.00			AA78678	B	1.00		
2.0	End of pit due to wall collapse. End of Trial Pit at 1.80m		1.80	72.62						

**Groundwater Conditions**

**Stability**  
Wall collapse from 0.9m

**General Remarks**



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane		<b>TRIAL PIT NO.</b> TP21	
<b>LOGGED BY</b> L. Daniels		<b>SHEET</b> Sheet 1 of 1	
<b>CLIENT</b> Ardstone		<b>DATE STARTED</b> 16/06/2017	
<b>ENGINEER</b> DBFL		<b>DATE COMPLETED</b> 16/06/2017	
<b>CO-ORDINATES</b> 687,542.98 E 728,212.30 N		<b>EXCAVATION METHOD</b> 3.5 Ton Excavator	
<b>GROUND LEVEL (m)</b> 74.33			

Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
			Sample Ref	Type	Depth		
0.0							
0.30	74.03		AA67758	B	0.50		
1.20	73.13		AA67759	B	1.30		
1.80	72.53		AA67760	B	2.00		
2.50	71.83		AA67761	B	2.50		

**Groundwater Conditions**

**Stability**  
Wall collapse from 1.8m

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL.GDT 3/7/17



# TRIAL PIT RECORD

**REPORT NUMBER**

20159

<b>CONTRACT</b> Capdoo, Clane		<b>TRIAL PIT NO.</b> TP22	
<b>LOGGED BY</b> L. Daniels		<b>SHEET</b> Sheet 1 of 1	
<b>CLIENT</b> Ardstone		<b>DATE STARTED</b> 16/06/2017	
<b>ENGINEER</b> DBFL		<b>DATE COMPLETED</b> 16/06/2017	
<b>CO-ORDINATES</b> 687,595.01 E 728,187.92 N		<b>EXCAVATION METHOD</b> 3.5 Ton Excavator	
<b>GROUND LEVEL (m)</b> 75.36			

Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
			Sample Ref	Type	Depth		
0.0							
0.30	75.06						
0.60	74.76						
1.0							
2.0	73.36		AA67762	B	0.80		
			AA67763	B	1.20		
2.50	72.86		AA67764	B	2.10		
			AA67765	B	2.60		
3.0	72.36						

**Groundwater Conditions**

**Stability**

**General Remarks**

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# TRIAL PIT RECORD

**REPORT NUMBER**  
**20159**

<b>CONTRACT</b> Capdoe, Clane	<b>CO-ORDINATES</b> 687,634.91 E 728,214.75 N	<b>TRIAL PIT NO.</b> <b>TP23</b>	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>GROUND LEVEL (m)</b> 73.91	<b>DATE STARTED</b> 16/06/2017	<b>DATE COMPLETED</b> 16/06/2017
<b>CLIENT</b> Ardstone <b>ENGINEER</b> DBFL		<b>EXCAVATION METHOD</b> 3.5 Ton Excavator	

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
0.30	Light brown slightly silty gravelly fine to medium SAND. Gravel is fine to medium subrounded.		0.30	73.61		AA67755	B	0.50		
1.20	Firm brown slightly gravelly sandy SILT.		1.20	72.71						
1.60	Dark grey to black very sandy fine to medium subrounded GRAVEL. Sand is medium to coarse.		1.60	72.31		AA67756	B	1.60		
2.80						AA67757	B	2.80		
3.00	End of Trial Pit at 3.00m		3.00	70.91						

**Groundwater Conditions**

**Stability**

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL\_GDT 3/7/17



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane	<b>TRIAL PIT NO.</b> TP24
	<b>SHEET</b> Sheet 1 of 1
<b>LOGGED BY</b> L. Daniels	<b>CO-ORDINATES</b> 687,695.94 E 728,217.70 N
	<b>DATE STARTED</b> 16/06/2017
	<b>DATE COMPLETED</b> 16/06/2017
<b>CLIENT</b> Ardstone	<b>GROUND LEVEL (m)</b> 72.38
<b>ENGINEER</b> DBFL	<b>EXCAVATION METHOD</b> 3.5 Ton Excavator

	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly SILT/CLAY. Gravel is fine to medium subangular to subrounded.		0.30	72.08						
	Brown silty fine to coarse subangular to subrounded GRAVEL with a medium cobble content and a low boulder content. Cobbles are subangular to rounded.		0.60	71.78						
1.0						AA67752	B	0.80		
	Black slightly gravelly coarse SAND. Gravel is fine subangular.		1.70	70.68		AA67753	B	1.70		
2.0										
	End of pit due to wall collapse. End of Trial Pit at 2.60m		2.60	69.78		AA67754	B	2.60		
3.0										

**Groundwater Conditions**

**Stability**  
Minor wall collapse from 1.7m

**General Remarks**

IGSL TP LOG 20159.GPJ IGSL.GDT 3/7/17



# TRIAL PIT RECORD

REPORT NUMBER

20159

<b>CONTRACT</b> Capdoo, Clane		<b>TRIAL PIT NO.</b> TP25	
<b>LOGGED BY</b> L. Daniels		<b>SHEET</b> Sheet 1 of 1	
<b>CLIENT</b> Ardstone		<b>DATE STARTED</b> 16/06/2017	
<b>ENGINEER</b> DBFL		<b>DATE COMPLETED</b> 16/06/2017	
<b>CO-ORDINATES</b> 687,732.04 E 728,216.34 N		<b>EXCAVATION METHOD</b> 3.5 Ton Excavator	
<b>GROUND LEVEL (m)</b> 70.94			

Depth (m)	Geotechnical Description	Legend	Depth (m)	Elevation	Water Strike	Samples			Vane Test (KPa)	Hand Penetrometer (KPa)
						Sample Ref	Type	Depth		
0.0	TOPSOIL.									
	Firm brown slightly gravelly SILT/CLAY. Gravel is fine to medium subangular to subrounded.		0.40	70.54		AA78699	B	0.60		
	Brown silty fine to coarse subangular to subrounded GRAVEL with a medium cobble content and a low boulder content. Cobbles are subangular to rounded.		0.80	70.14						
1.0	Brown sandy fine to coarse subrounded GRAVEL.		1.20	69.74		AA78700	B	1.20		
	Black slightly gravelly fine to medium SAND. Gravel is fine subangular.		1.60	69.34		AA67751	B	1.80		
2.0										
3.0	End of Trial Pit at 3.00m		3.00	67.94						

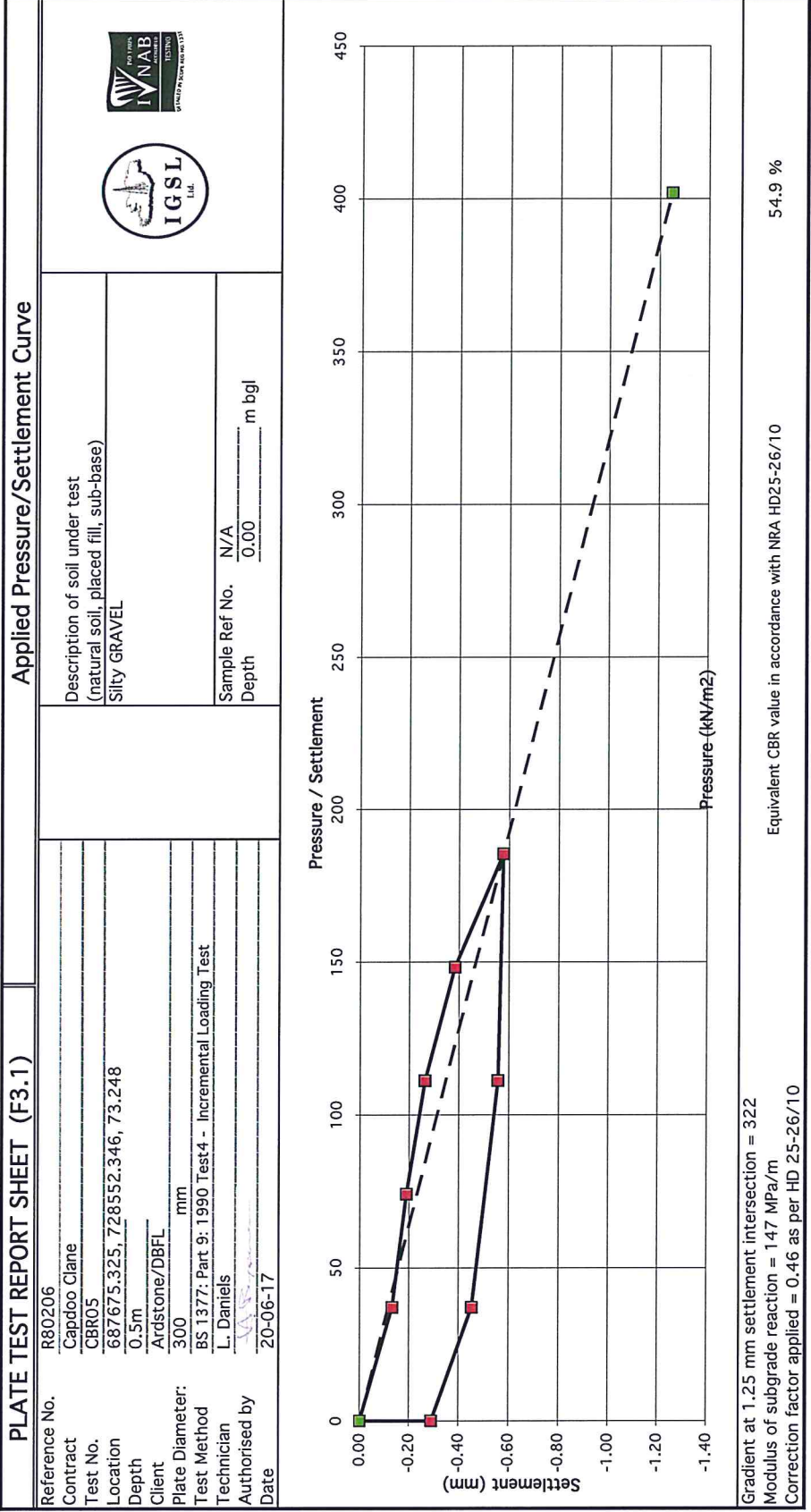
**Groundwater Conditions**

**Stability**

**General Remarks**



IGSL TP LOG 20159.GPJ IGSL\_GDT 3/7/17

## **Appendix III Plate Bearing Tests**

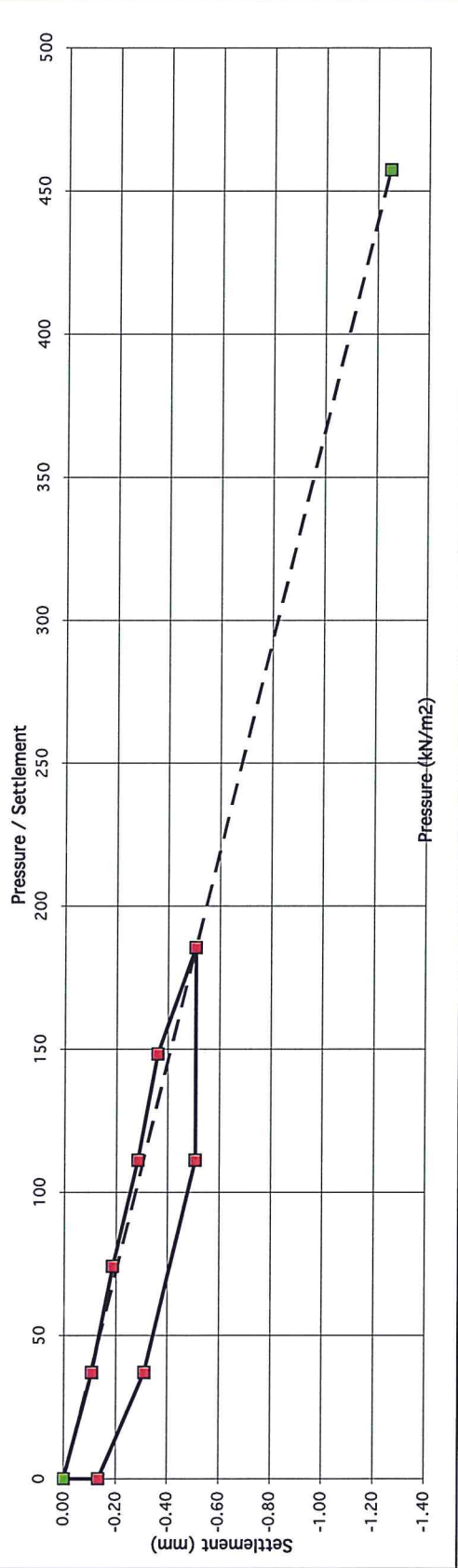




**PLATE TEST REPORT SHEET (F3.1)**



Reference No. R80206 Contract Capdoo Crane Test No. CB05 reload Location 687675.325, 728552.346, 73.248 Depth 0.5m Client Ardstone/DBFL Plate Diameter: 300 mm Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test Technician L. Daniels Authorised by AA Date 20-06-17	Description of soil under test (natural soil, placed fill, sub-base) Silty GRAVEL  Sample Ref No. N/A Depth 0.00 m bgl	 
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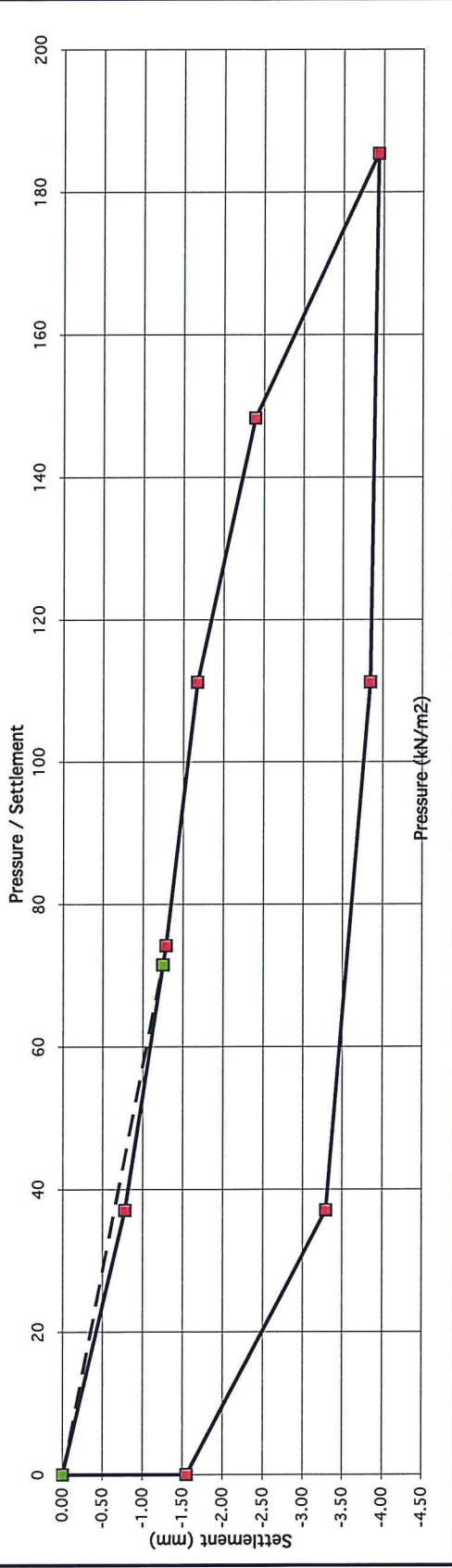
**Applied Pressure/Settlement Curve**



Gradient at 1.25 mm settlement intersection = 366  
 Modulus of subgrade reaction = 167 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10  
 Equivalent CBR value in accordance with NRA HD25-26/10 = 68.7 %

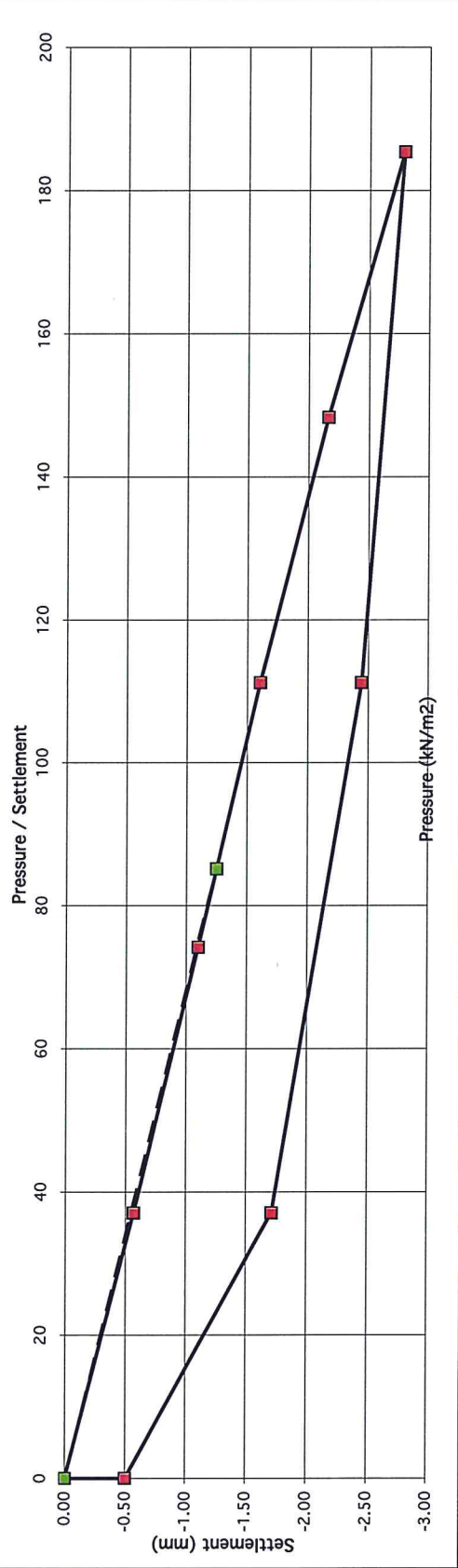
**PLATE TEST REPORT SHEET (F3.1)**

Reference No. R80207 Contract Capdoo Clane Test No. CBR06 Location 687672.781, 728492.900, 75.678 Depth 0.5m Client Ardistone/DBFL Plate Diameter: 300 mm Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test Technician L. Daniels Authorised by VAS Date 20-06-17	<p align="center"><b>Applied Pressure/Settlement Curve</b></p> Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT Sample Ref No. N/A Depth 0.00 m bgl	 
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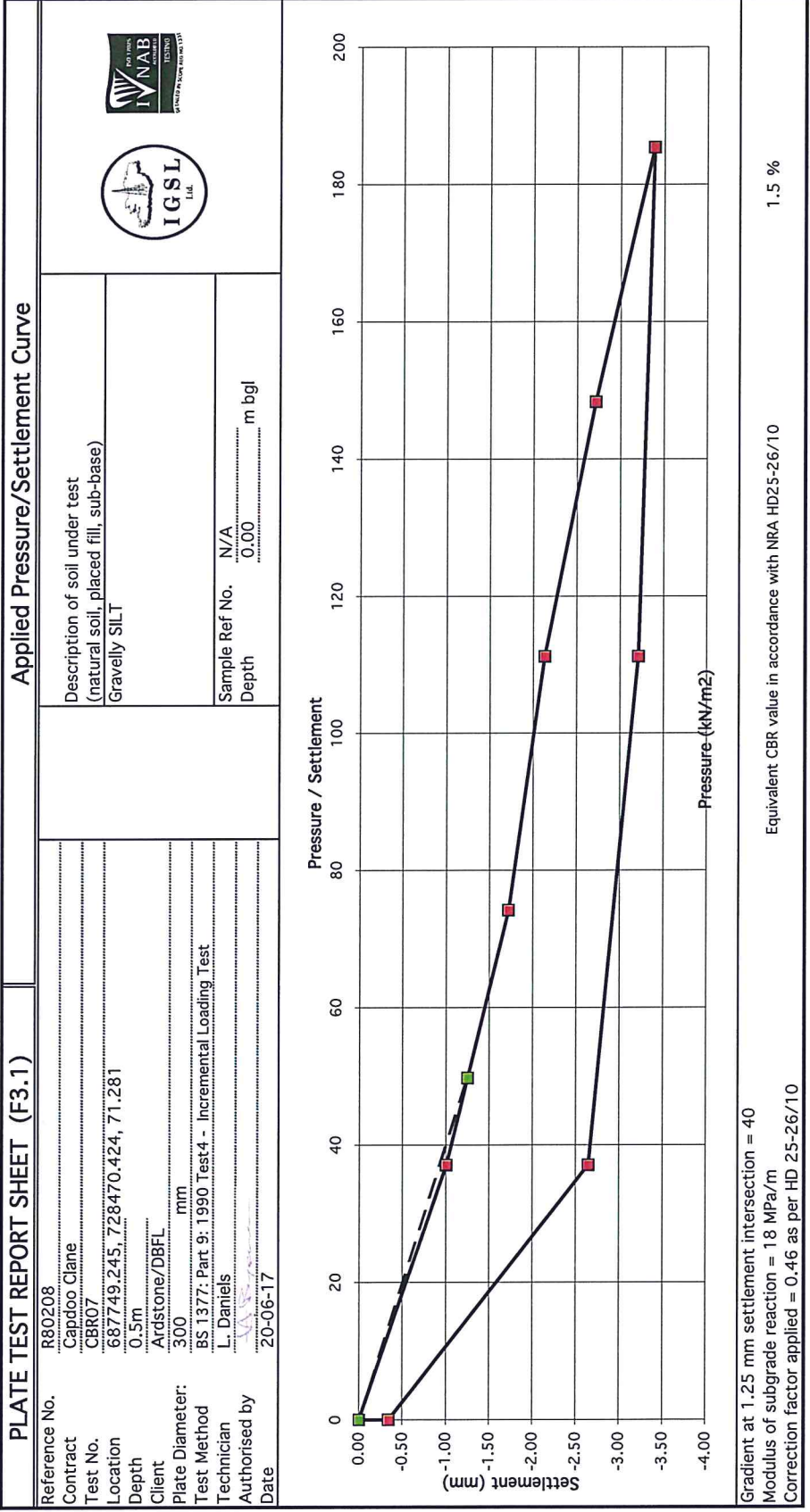
Gradient at 1.25 mm settlement intersection = 57  
 Modulus of subgrade reaction = 26 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10  
 Equivalent CBR value in accordance with NRA HD25-26/10 2.8 %

PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No.	R80207	Description of soil under test	
Contract	Capdoo Clane	(natural soil, placed fill, sub-base)	
Test No.	687672.781, 728492.900, 75.678	Gravelly SILT	
Location	See Map		
Depth	0.5m		
Client	Ardstone/DBFL		
Plate Diameter:	300 mm	Sample Ref No.	N/A
Test Method	BS 1377: Part 9: 1990 Test4 - Incremental Loading Test	Depth	0.00 m bgl
Technician	L. Daniels		
Authorised by	<i>(Signature)</i>		
Date	20-06-17		





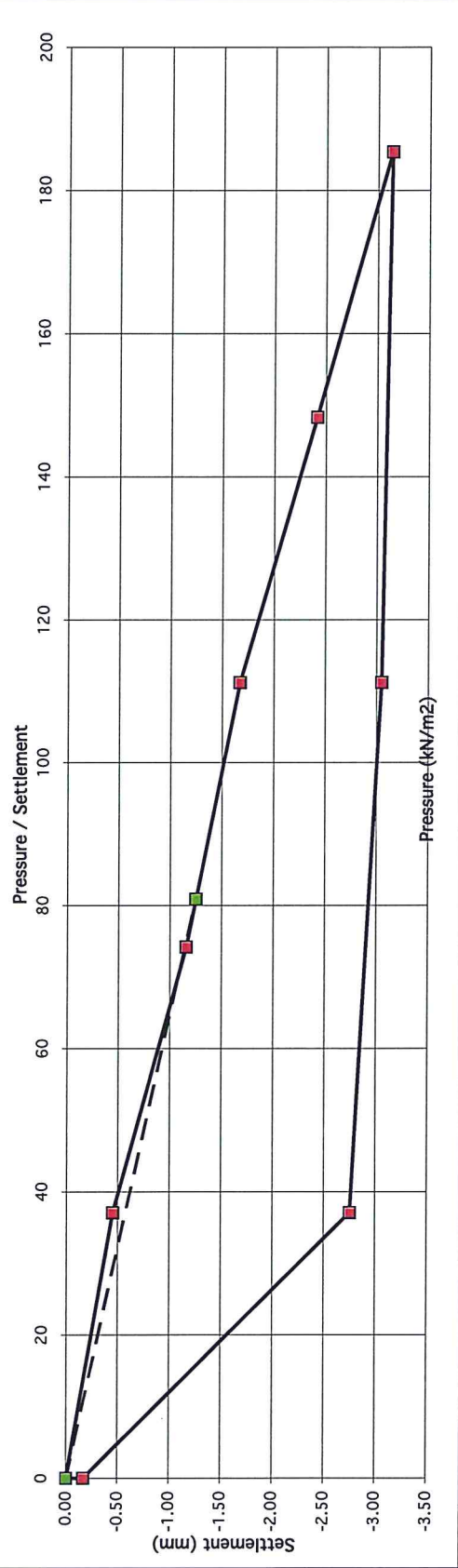
Gradient at 1.25 mm settlement intersection = 68  
 Modulus of subgrade reaction = 31 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

Equivalent CBR value in accordance with NRA HD25-26/10 3.7 %



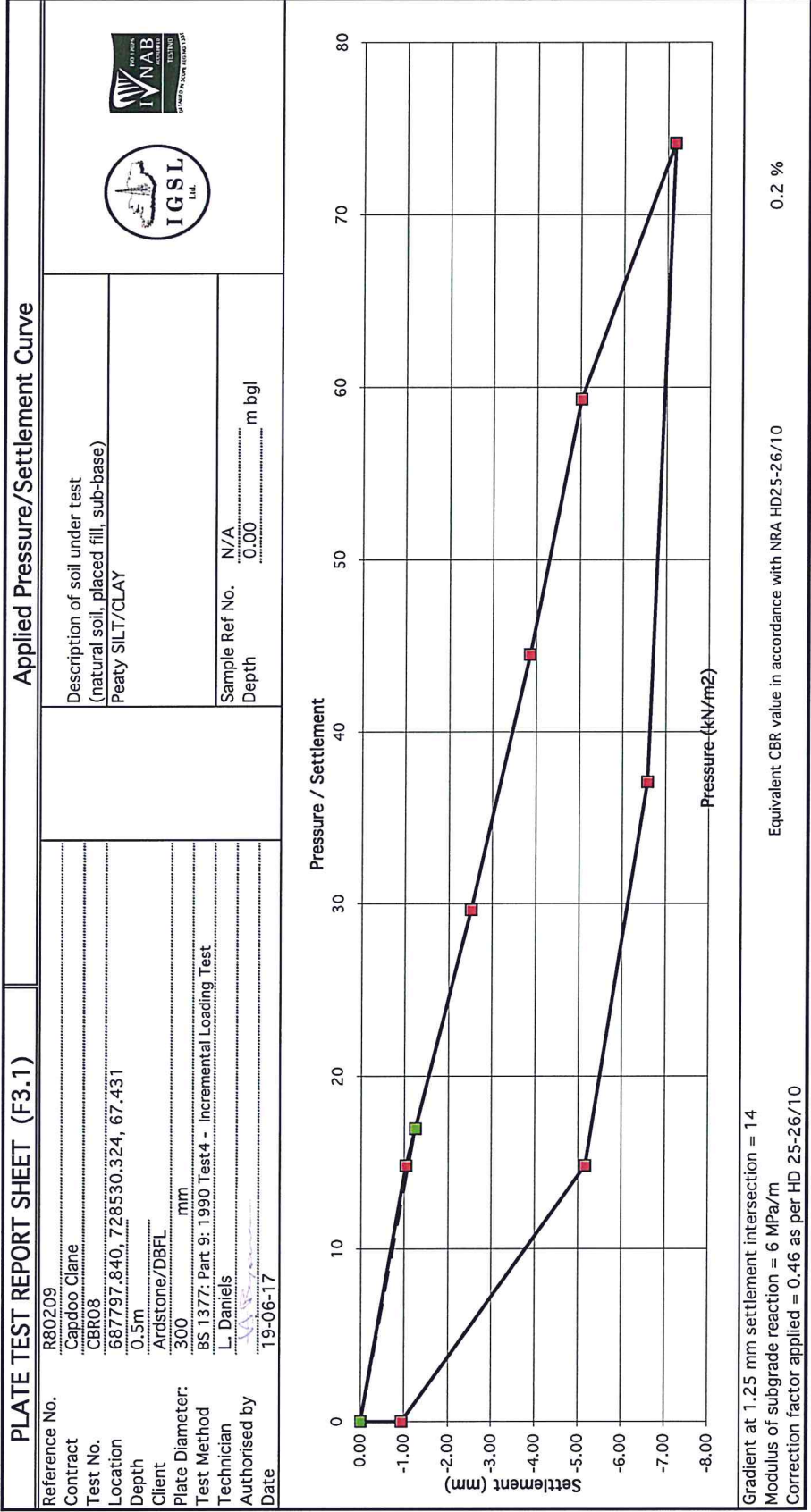
**PLATE TEST REPORT SHEET (F3.1)**

Reference No. 880208 Contract Capdoo Clane Test No. CBR07 reload Location 687749.245, 728470.424, 71.281 Depth 0.5m Client Ardstone/DBFL Plate Diameter: 300 mm Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test Technician L. Daniels Authorised by VAS Date 20-06-17	<p align="center"><b>Applied Pressure/Settlement Curve</b></p> Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	 
Sample Ref No. N/A Depth 0.00 m bgl		





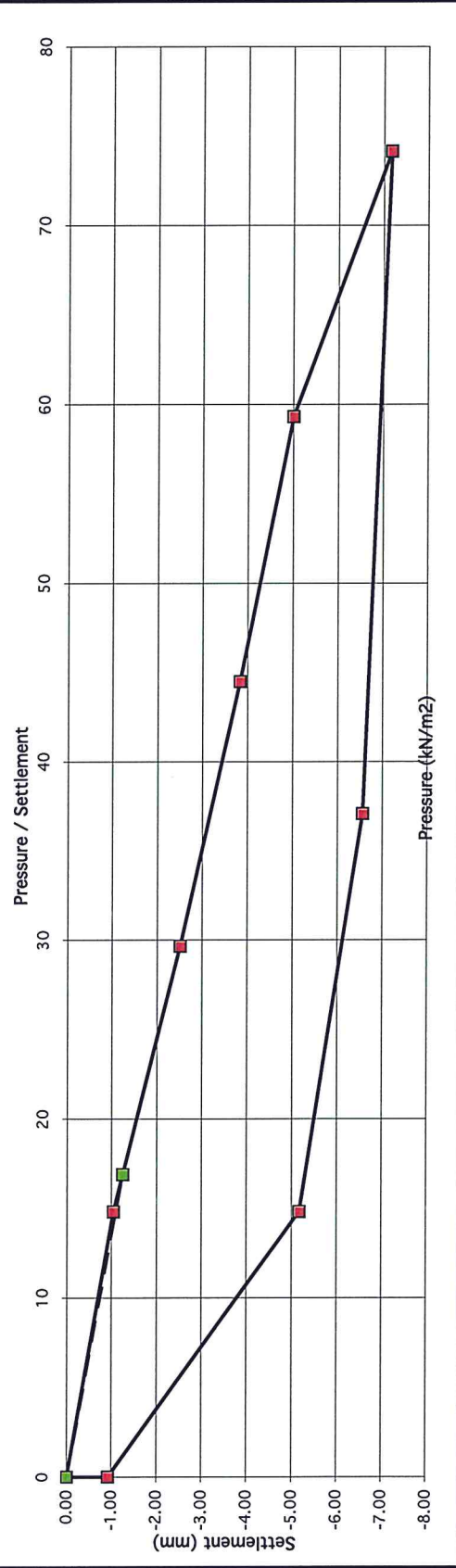
Gradient at 1.25 mm settlement intersection = 65  
 Modulus of subgrade reaction = 30 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

Equivalent CBR value in accordance with NRA HD25-26/10 **3.4 %**



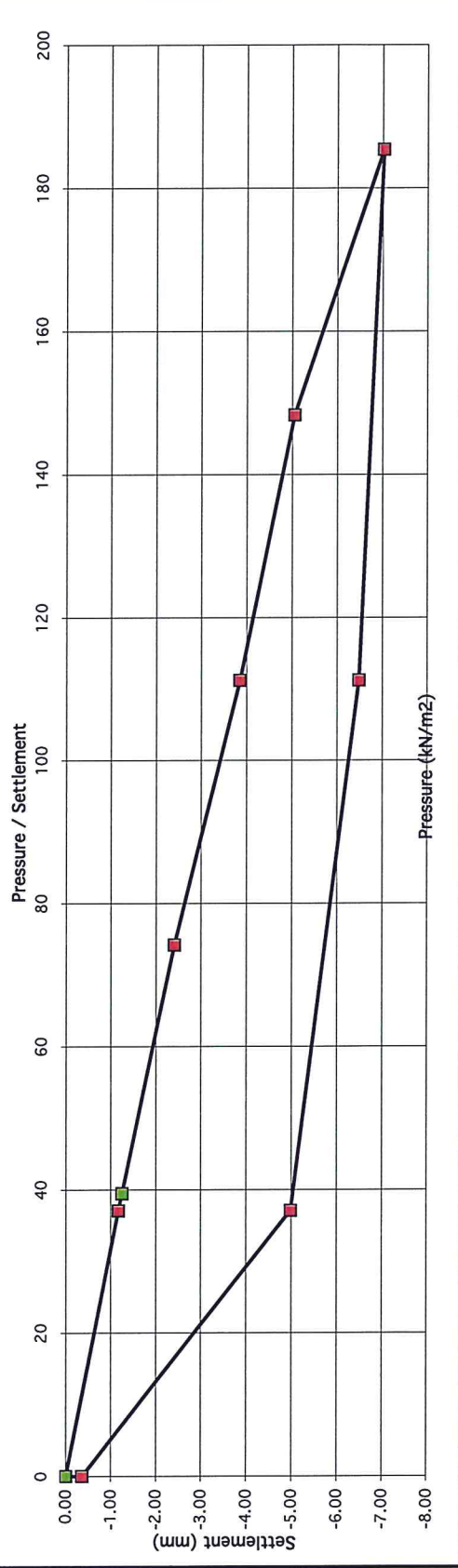
**PLATE TEST REPORT SHEET (F3.1)**

Reference No. R80209 Contract Capdoo Clane Test No. CBR08 reload Location 687797.840, 728530.324, 67.431 Depth 0.5m Client Ardstone/DBFL Plate Diameter: 300 mm Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test Technician L. Daniels Authorised by Date 19-06-17	Applied Pressure/Settlement Curve Description of soil under test (natural soil, placed fill, sub-base) Peaty SILT/CLAY Sample Ref No. N/A Depth 0.00 m bgl	 
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Gradient at 1.25 mm settlement intersection = 14  
 Modulus of subgrade reaction = 6 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10  
 Equivalent CBR value in accordance with NRA HD25-26/10 0.2 %

PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No.	R80210	Description of soil under test (natural soil, placed fill, sub-base)	
Contract	Capdoo Clane	Gravelly SILT	Sample Ref No. N/A
Test No.	CBR09		
Location	687803.717, 728468.047, 67.833	Depth	0.00 m bgl
Depth	0.5m		
Client	Ardstone/DBFL		
Plate Diameter:	300 mm		
Test Method	BS 1377: Part 9: 1990 Test4 - Incremental Loading Test		
Technician	L. Daniels		
Authorised by	<i>L. Daniels</i>		
Date	19-06-17		



Gradient at 1.25 mm settlement intersection = 32  
 Modulus of subgrade reaction = 14 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

Equivalent CBR value in accordance with NRA HD25-26/10 1.0 %







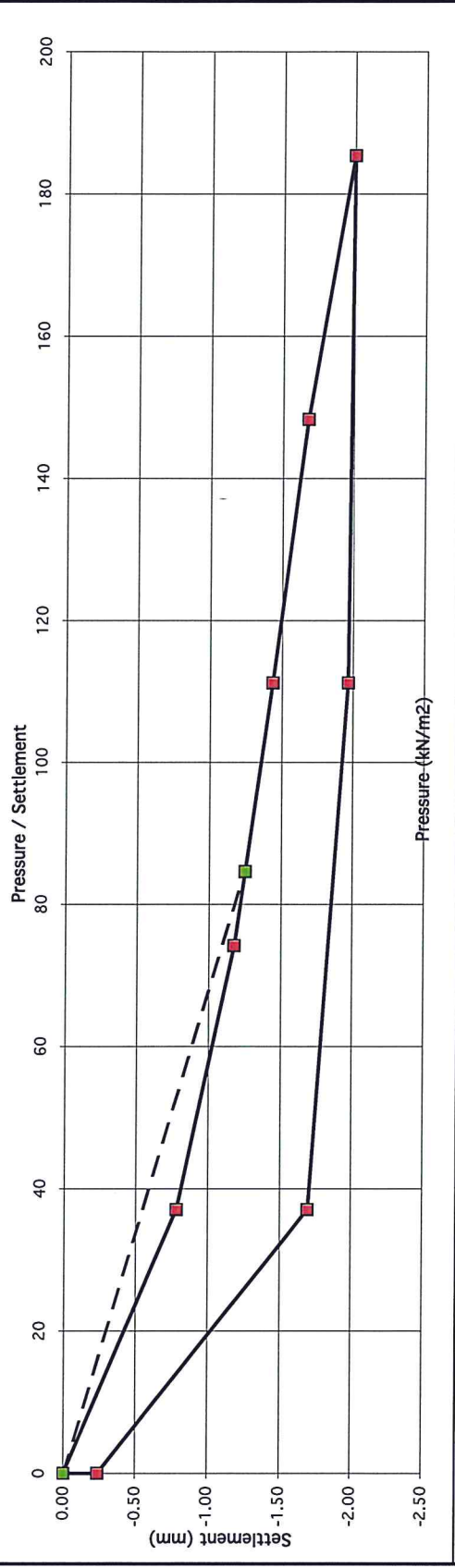
PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve																	
Reference No. R80208	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A																
Test No. CBR09_reload	Location 687803.717, 728468.047, 67.833			Depth 0.00 m bgl															
Depth 0.5m	Client Ardstone/DBFL	 																	
Plate Diameter: 300 mm	Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test																		
Technician L. Daniels	Authorised by																		
Date 19-06-17																			
<table border="1"> <caption>Applied Pressure/Settlement Curve Data</caption> <thead> <tr> <th>Pressure (kN/m<sup>2</sup>)</th> <th>Settlement (mm)</th> </tr> </thead> <tbody> <tr><td>0.00</td><td>0.00</td></tr> <tr><td>10.00</td><td>-1.00</td></tr> <tr><td>20.00</td><td>-2.00</td></tr> <tr><td>30.00</td><td>-3.00</td></tr> <tr><td>40.00</td><td>-4.00</td></tr> <tr><td>50.00</td><td>-5.00</td></tr> <tr><td>60.00</td><td>-6.00</td></tr> </tbody> </table>				Pressure (kN/m <sup>2</sup> )	Settlement (mm)	0.00	0.00	10.00	-1.00	20.00	-2.00	30.00	-3.00	40.00	-4.00	50.00	-5.00	60.00	-6.00
Pressure (kN/m <sup>2</sup> )	Settlement (mm)																		
0.00	0.00																		
10.00	-1.00																		
20.00	-2.00																		
30.00	-3.00																		
40.00	-4.00																		
50.00	-5.00																		
60.00	-6.00																		
Gradient at 1.25 mm settlement intersection = 40 Modulus of subgrade reaction = 18 MPa/m Correction factor applied = 0.46 as per HD 25-26/10																			
Equivalent CBR value in accordance with NRA HD25-26/10 <span style="float: right;">1.5 %</span>																			

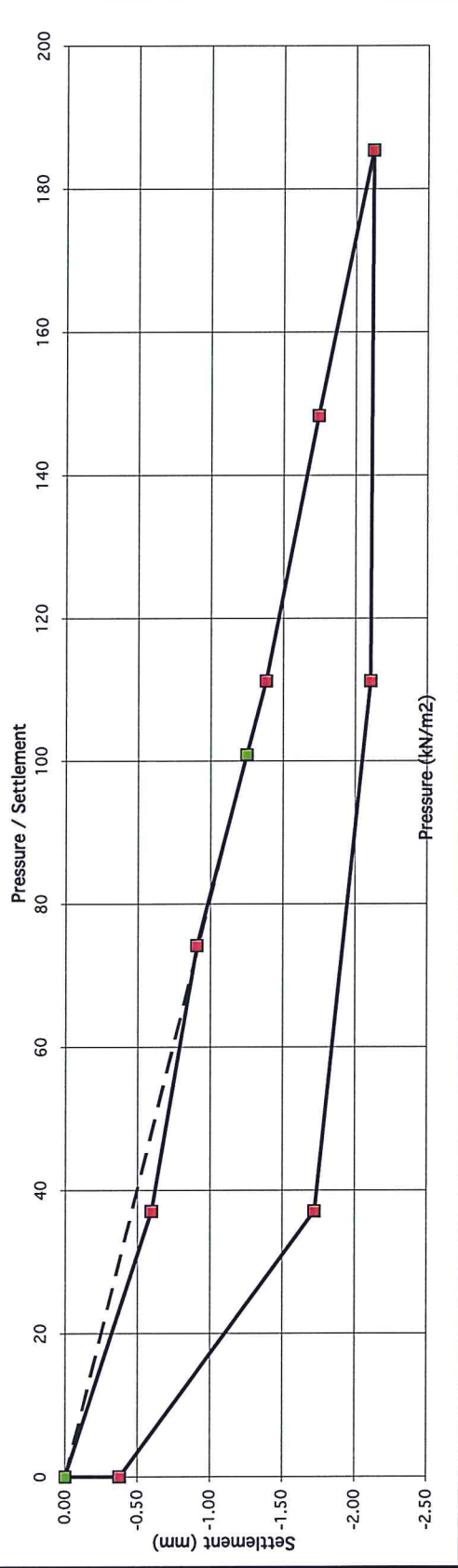
PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No. R80211	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	 
Test No. CBR10	Location 687877.151, 728463.847, 67.959	Sample Ref No. N/A	Depth 0.00 m bgl
Depth 0.5m	Client Ardstone/DBFL		
Plate Diameter: 300 mm	Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test		
Technician L. Daniels	Authorised by L. Daniels		
Date 19-06-17			





Gradient at 1.25 mm settlement intersection = 68  
 Modulus of subgrade reaction = 31 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

Equivalent CBR value in accordance with NRA HD25-26/10 3.7 %


PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No.	R80211	Description of soil under test (natural soil, placed fill, sub-base)	
Contract	Capdoo Clane	Gravelly SILT	Sample Ref No. N/A
Test No.	CBR10 reload		
Location	687877.151, 728463.847, 67.959	Depth	0.00 m bgl
Depth	0.5m		
Client	Ardstone/DBFL		
Plate Diameter:	300 mm		
Test Method	BS 1377: Part 9: 1990 Test4 - Incremental Loading Test		
Technician	L. Daniels		
Authorised by	<i>L. Daniels</i>		
Date	19-06-17		



Gradient at 1.25 mm settlement intersection = 81  
 Modulus of subgrade reaction = 37 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10  
 Equivalent CBR value in accordance with NRA HD25-26/10 5.0 %

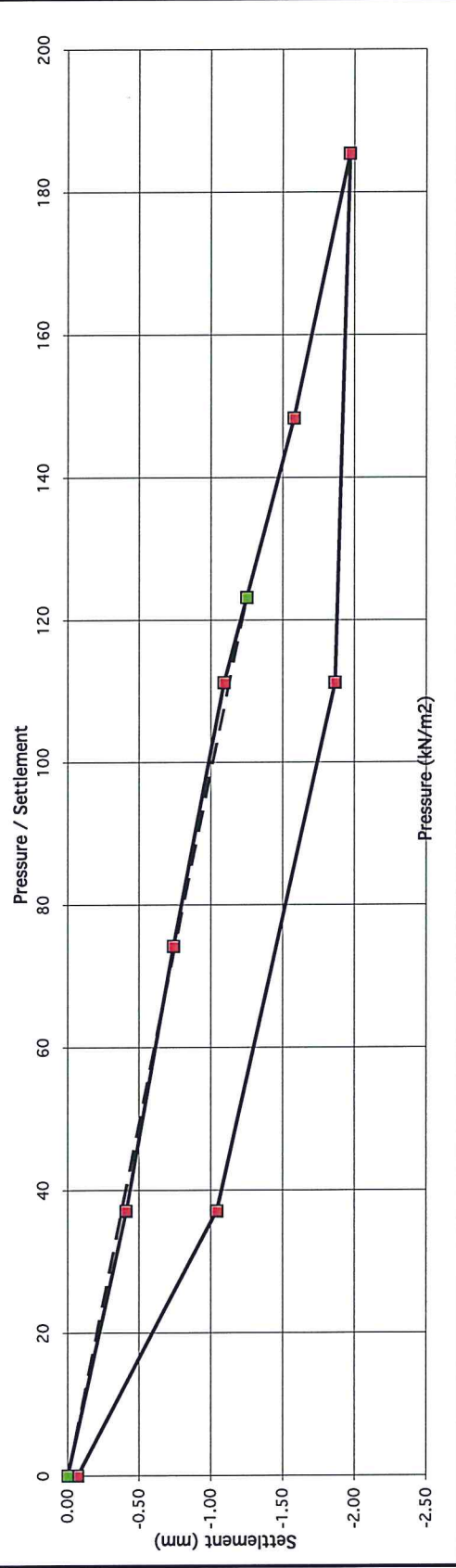
PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve															
Reference No. R80212	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	 	Sample Ref No. N/A Depth 0.00 m bgl														
Contract Capdoo Clane																	
Test No. CBR11																	
Location 687789.531, 728406.658, 68.844																	
Depth 0.5m																	
Client Ardstone/DBFL																	
Plate Diameter: 300 mm																	
Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test																	
Technician L. Daniels																	
Authorised by L. Daniels																	
Date 19-06-17																	
<table border="1"> <caption>Data points from the Applied Pressure/Settlement Curve</caption> <thead> <tr> <th>Pressure (kN/m<sup>2</sup>)</th> <th>Settlement (mm)</th> </tr> </thead> <tbody> <tr><td>0</td><td>0.00</td></tr> <tr><td>37</td><td>-0.50</td></tr> <tr><td>82</td><td>-1.00</td></tr> <tr><td>110</td><td>-1.25</td></tr> <tr><td>148</td><td>-1.50</td></tr> <tr><td>185</td><td>-2.00</td></tr> </tbody> </table>				Pressure (kN/m <sup>2</sup> )	Settlement (mm)	0	0.00	37	-0.50	82	-1.00	110	-1.25	148	-1.50	185	-2.00
Pressure (kN/m <sup>2</sup> )	Settlement (mm)																
0	0.00																
37	-0.50																
82	-1.00																
110	-1.25																
148	-1.50																
185	-2.00																
Gradient at 1.25 mm settlement intersection = 82 Modulus of subgrade reaction = 37 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 5.1 %															

**PLATE TEST REPORT SHEET (F3.1)**

Reference No. R80208 Contract Capdoo Clane Test No. CBRT1 reload Location 687789.531, 728406.658, 68.844 Depth 0.5m Client Ardstone/DBFL Plate Diameter: 300 mm Test Method BS.1377: Part 9: 1990 Test4 - Incremental Loading Test Technician L. Daniels Authorised by  Date 19-06-17	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A Depth 0.00 m bgl
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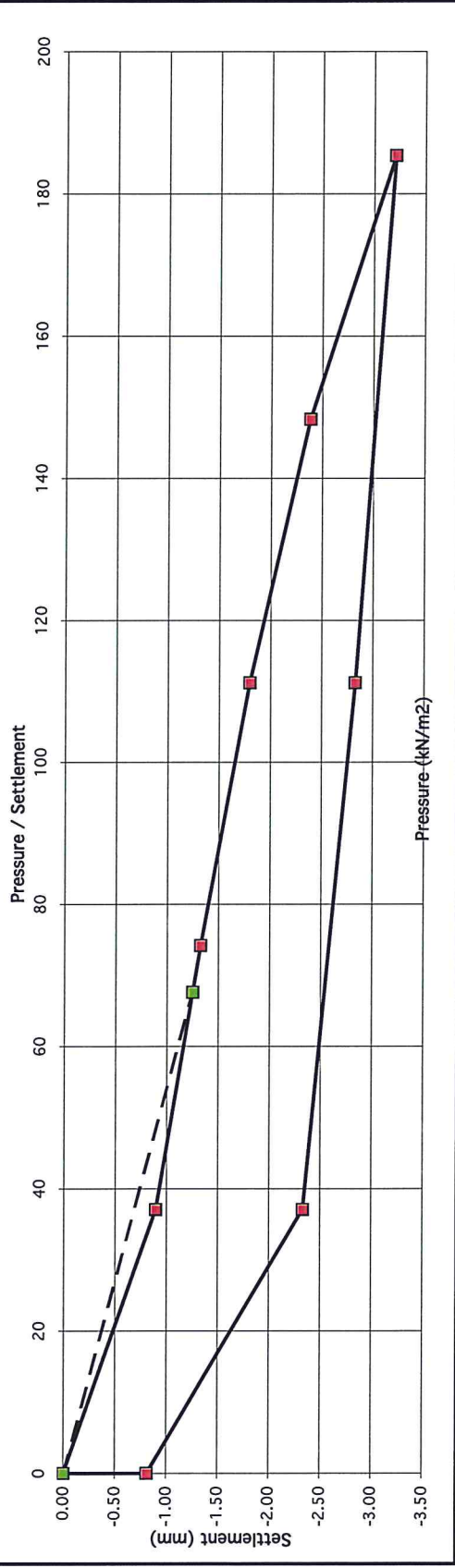
**Applied Pressure/Settlement Curve**



Gradient at 1.25 mm settlement intersection = 99  
 Modulus of subgrade reaction = 45 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10  
 Equivalent CBR value in accordance with NRA HD25-26/10 7.1 %

**PLATE TEST REPORT SHEET (F3.1)** **Applied Pressure/Settlement Curve**

Reference No. R80213 Contract Capdoo Clane Test No. CBR12 Location 687730.464, 728407.565, 72.162 Depth 0.5m Client Ardstone/DBFL Plate Diameter: 300 mm Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test Technician L. Daniels Authorised by <i>L. Daniels</i> Date 16-06-17	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A Depth 0.00 m bgl
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Gradient at 1.25 mm settlement intersection = 54  
 Modulus of subgrade reaction = 25 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

Equivalent CBR value in accordance with NRA HD25-26/10

2.5 %



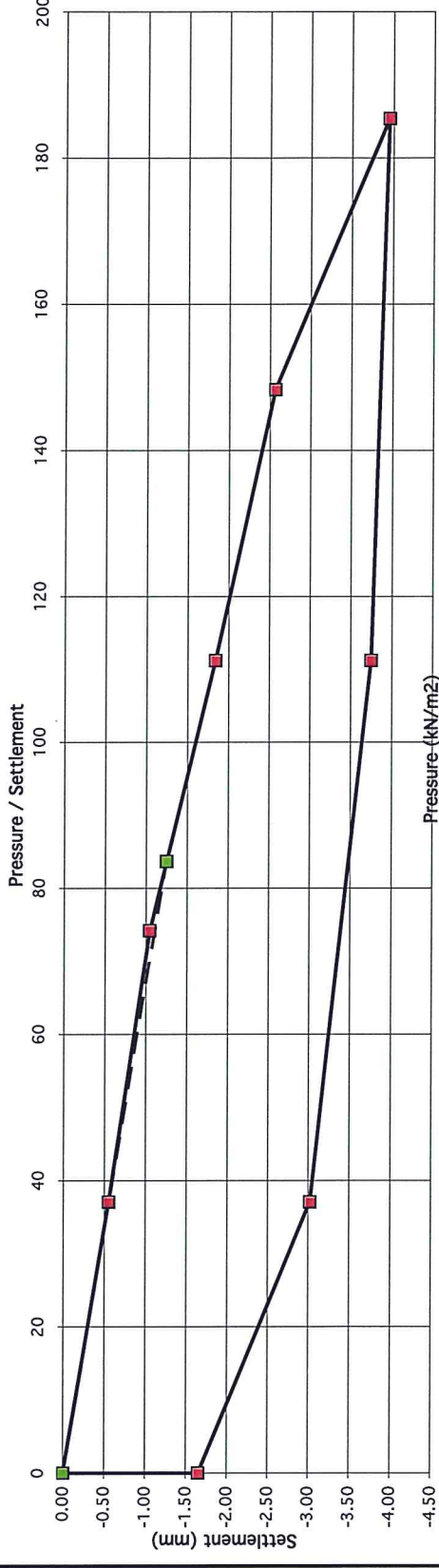
PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve																					
Reference No. R80213	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	 																				
Test No. CBR12 reload	Location 687730.464, 728407.565, 72.162																						
Location 687730.464, 728407.565, 72.162	Depth 0.5m	Sample Ref No. N/A	Depth 0.00 m bgl																				
Client Ardstone/DBFL	Plate Diameter: 300 mm																						
Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test	Technician L. Daniels																						
Authorised by L. Daniels	Date 16-06-17																						
 <p>The graph plots Settlement (mm) on the y-axis (0 to -4.50) against Pressure / Settlement (kN/m<sup>2</sup>) on the x-axis (0 to 200). The curve shows a non-linear relationship, starting at (0,0) and reaching approximately (185, -4.00). A tangent line is drawn at the 1.25 mm settlement point, intersecting the y-axis at -3.1 MPa/m.</p> <table border="1"> <caption>Approximate data points from the graph</caption> <thead> <tr> <th>Pressure / Settlement (kN/m<sup>2</sup>)</th> <th>Settlement (mm)</th> </tr> </thead> <tbody> <tr><td>0</td><td>0.00</td></tr> <tr><td>~10</td><td>-0.50</td></tr> <tr><td>~20</td><td>-1.00</td></tr> <tr><td>~30</td><td>-1.50</td></tr> <tr><td>~40</td><td>-2.00</td></tr> <tr><td>~50</td><td>-2.50</td></tr> <tr><td>~60</td><td>-3.00</td></tr> <tr><td>~110</td><td>-3.50</td></tr> <tr><td>~185</td><td>-4.00</td></tr> </tbody> </table>				Pressure / Settlement (kN/m <sup>2</sup> )	Settlement (mm)	0	0.00	~10	-0.50	~20	-1.00	~30	-1.50	~40	-2.00	~50	-2.50	~60	-3.00	~110	-3.50	~185	-4.00
Pressure / Settlement (kN/m <sup>2</sup> )	Settlement (mm)																						
0	0.00																						
~10	-0.50																						
~20	-1.00																						
~30	-1.50																						
~40	-2.00																						
~50	-2.50																						
~60	-3.00																						
~110	-3.50																						
~185	-4.00																						
Gradient at 1.25 mm settlement intersection = 67 Modulus of subgrade reaction = 31 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 3.6 %																					



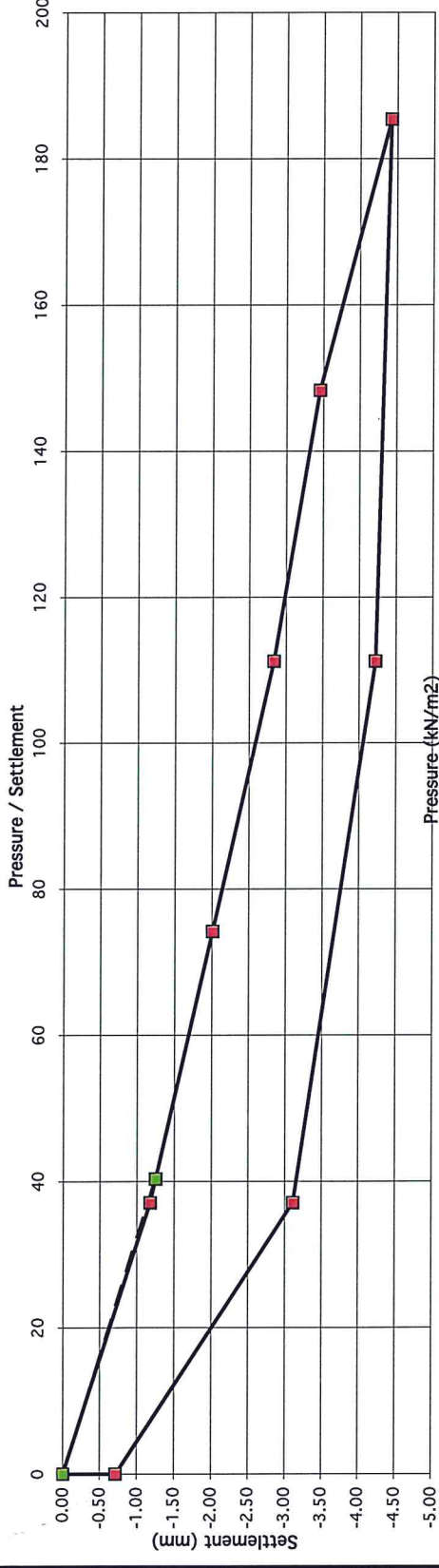


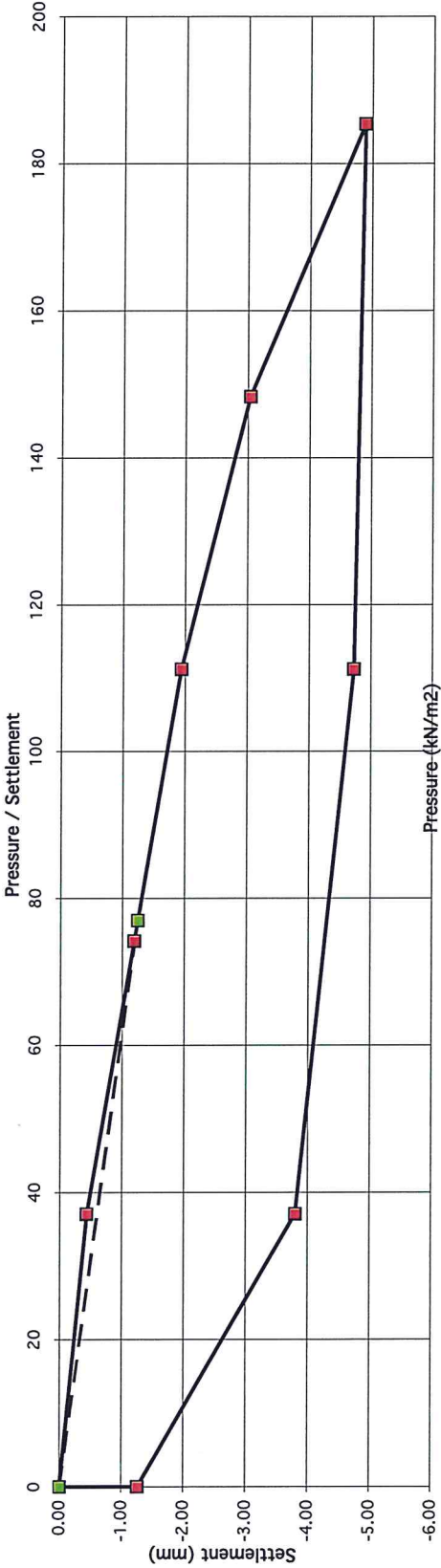
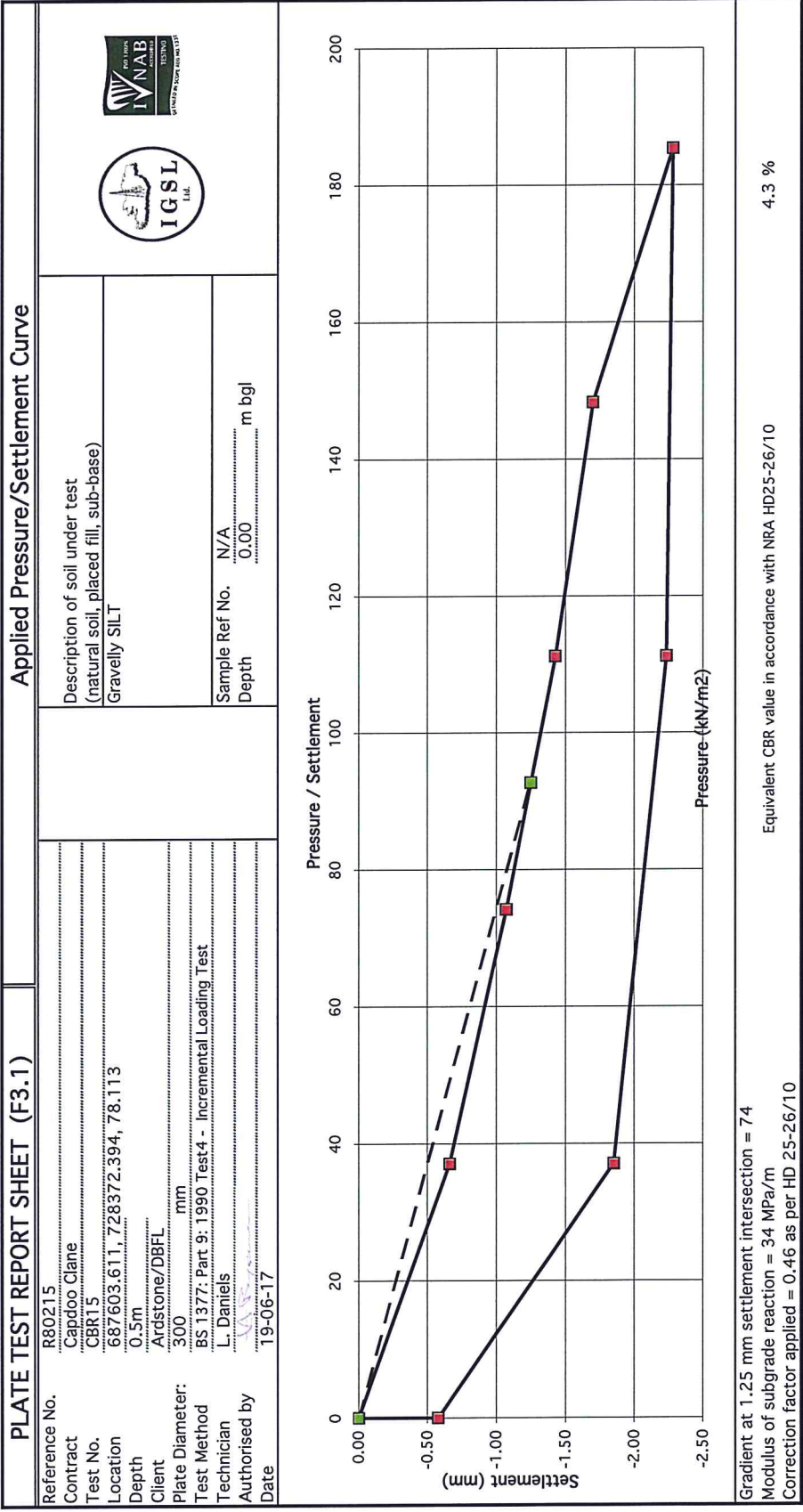
PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve																	
Reference No. R80214	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	 																
Test No. CBR13	Location 687654.908, 728465.015, 77.296																		
Depth 0.5m	Client Ardstone/DBFL	Sample Ref No. N/A	Depth 0.00 m bgl																
Plate Diameter: 300 mm	Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test																		
Technician L. Daniels	Authorised by L. Daniels																		
Date 16-06-17																			
 <p>The graph plots Settlement (mm) on the y-axis (0 to -5.00) against Pressure / Settlement (kN/m<sup>2</sup>) on the x-axis (0 to 200). The curve shows a non-linear relationship, starting at (0,0) and reaching approximately (185, -4.50). Key data points are marked with red squares.</p> <table border="1"> <caption>Key Data Points from Graph</caption> <thead> <tr> <th>Pressure / Settlement (kN/m<sup>2</sup>)</th> <th>Settlement (mm)</th> </tr> </thead> <tbody> <tr><td>0</td><td>0.00</td></tr> <tr><td>~10</td><td>-0.50</td></tr> <tr><td>~35</td><td>-1.00</td></tr> <tr><td>~75</td><td>-2.00</td></tr> <tr><td>~115</td><td>-3.00</td></tr> <tr><td>~150</td><td>-4.00</td></tr> <tr><td>~185</td><td>-4.50</td></tr> </tbody> </table>				Pressure / Settlement (kN/m <sup>2</sup> )	Settlement (mm)	0	0.00	~10	-0.50	~35	-1.00	~75	-2.00	~115	-3.00	~150	-4.00	~185	-4.50
Pressure / Settlement (kN/m <sup>2</sup> )	Settlement (mm)																		
0	0.00																		
~10	-0.50																		
~35	-1.00																		
~75	-2.00																		
~115	-3.00																		
~150	-4.00																		
~185	-4.50																		
Gradient at 1.25 mm settlement intersection = 32 Modulus of subgrade reaction = 15 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 1.0 %																	



PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve																					
Reference No. R80214	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	 																				
Test No. CBR13 reload	Location 687654.908, 728465.015, 77.296																						
Depth 0.5m	Client Ardstone/DBFL	Sample Ref No. N/A	Depth 0.00 m bgl																				
Plate Diameter: 300 mm	Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test																						
Technician L. Daniels	Authorised by L. Daniels																						
Date 16-06-17																							
 <table border="1"> <caption>Data points from Applied Pressure/Settlement Curve</caption> <thead> <tr> <th>Pressure (kN/m<sup>2</sup>)</th> <th>Settlement (mm)</th> </tr> </thead> <tbody> <tr><td>0.00</td><td>0.00</td></tr> <tr><td>3.50</td><td>-1.00</td></tr> <tr><td>7.50</td><td>-1.20</td></tr> <tr><td>11.00</td><td>-1.50</td></tr> <tr><td>15.00</td><td>-2.00</td></tr> <tr><td>20.00</td><td>-2.50</td></tr> <tr><td>25.00</td><td>-3.50</td></tr> <tr><td>30.00</td><td>-4.50</td></tr> <tr><td>40.00</td><td>-5.00</td></tr> </tbody> </table>				Pressure (kN/m <sup>2</sup> )	Settlement (mm)	0.00	0.00	3.50	-1.00	7.50	-1.20	11.00	-1.50	15.00	-2.00	20.00	-2.50	25.00	-3.50	30.00	-4.50	40.00	-5.00
Pressure (kN/m <sup>2</sup> )	Settlement (mm)																						
0.00	0.00																						
3.50	-1.00																						
7.50	-1.20																						
11.00	-1.50																						
15.00	-2.00																						
20.00	-2.50																						
25.00	-3.50																						
30.00	-4.50																						
40.00	-5.00																						
Gradient at 1.25 mm settlement intersection = 62 Modulus of subgrade reaction = 28 MPa/m Correction factor applied = 0.46 as per HD 25-26/10																							
Equivalent CBR value in accordance with NRA HD25-26/10 = 3.1 %																							



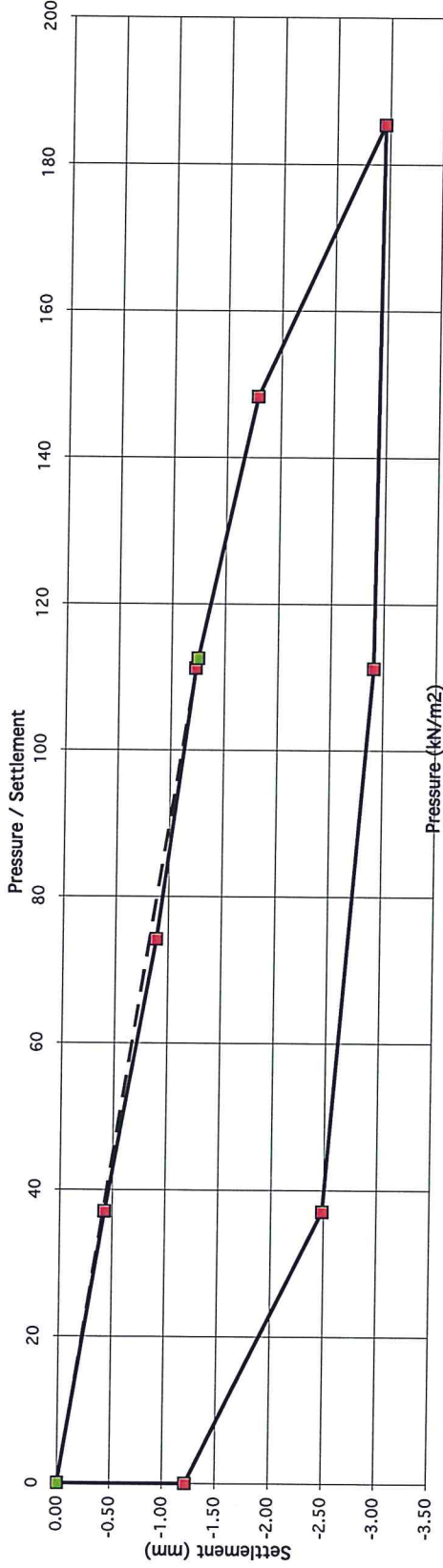
**PLATE TEST REPORT SHEET (F3.1)**

**Applied Pressure/Settlement Curve**

Reference No. R80215  
 Contract Capdoo Clane  
 Test No. CBR15 reload  
 Location 687603.611, 728372.394, 78.113  
 Depth 0.5m  
 Client Ardstone/DBFL  
 Plate Diameter: 300 mm  
 Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test  
 Technician L. Daniels  
 Authorised by [Signature]  
 Date 19-06-17

Description of soil under test  
 (natural soil, placed fill, sub-base)  
 Gravelly SILT



Sample Ref No. N/A  
 Depth 0.00 m bgl

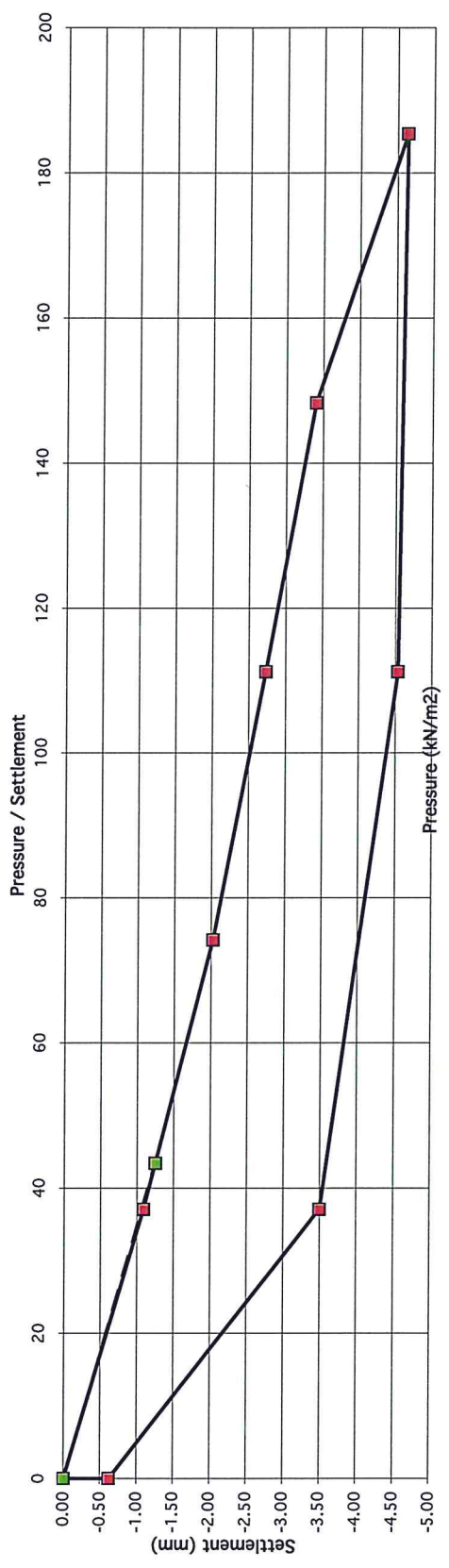


Gradient at 1.25 mm settlement: intersection = 90  
 Modulus of subgrade reaction = 41 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

Equivalent CBR value in accordance with NRA HD25-26/10

6.1 %

PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No. R80216	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A
Test No. CBR16	Location 687648.389, 728374.574, 75.477		
Location 0.5m	Client Ardstone/DBFL	 	
Depth 300 mm	Plate Diameter: 300 mm		
Client Ardstone/DBFL	Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test		
Technician L. Daniels	Authorised by <i>L. Daniels</i>		
Date 19-06-17			



Gradient at 1.25 mm settlement intersection = 35  
 Modulus of subgrade reaction = 16 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

Equivalent CBR value in accordance with NRA HD25-26/10 1.2 %



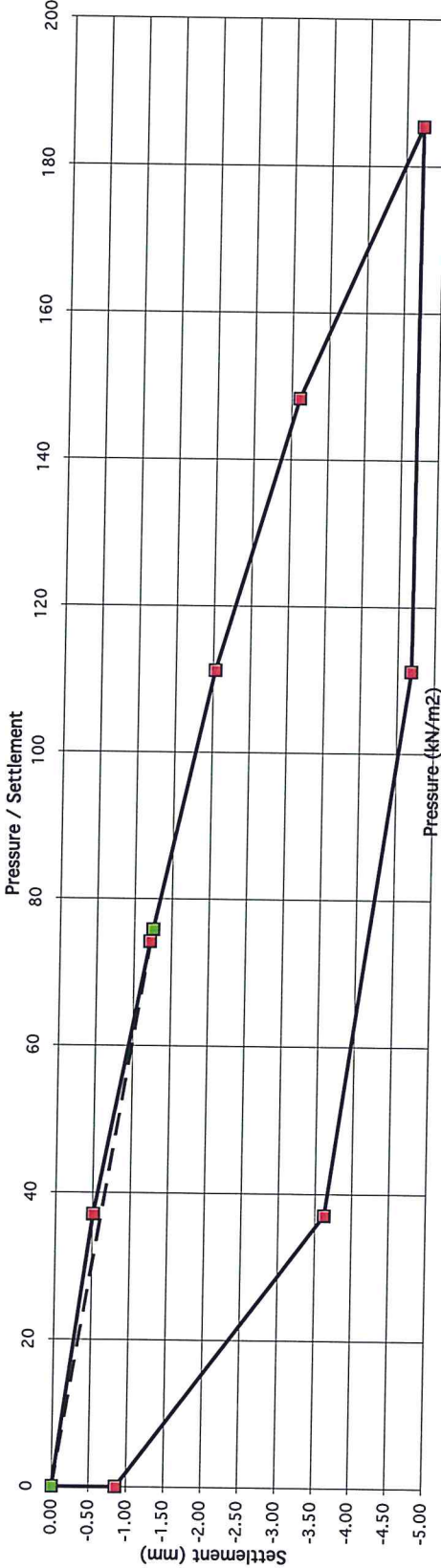
PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No. R80216	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A
Test No. CBR16 reload	Location 687648.389, 728374.574, 75.477		
Depth 0.5m	Client Ardstone/DBFL	 	
Plate Diameter: 300 mm	Test Method BS 1377: Part 9: 1990 Test 4		
Technician L. Daniels	Test Method Incremental Loading Test		
Authorised by AAE	Date 19-06-17		
			
Gradient at 1.25 mm settlement intersection = 61 Modulus of subgrade reaction = 28 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 3.1 %	



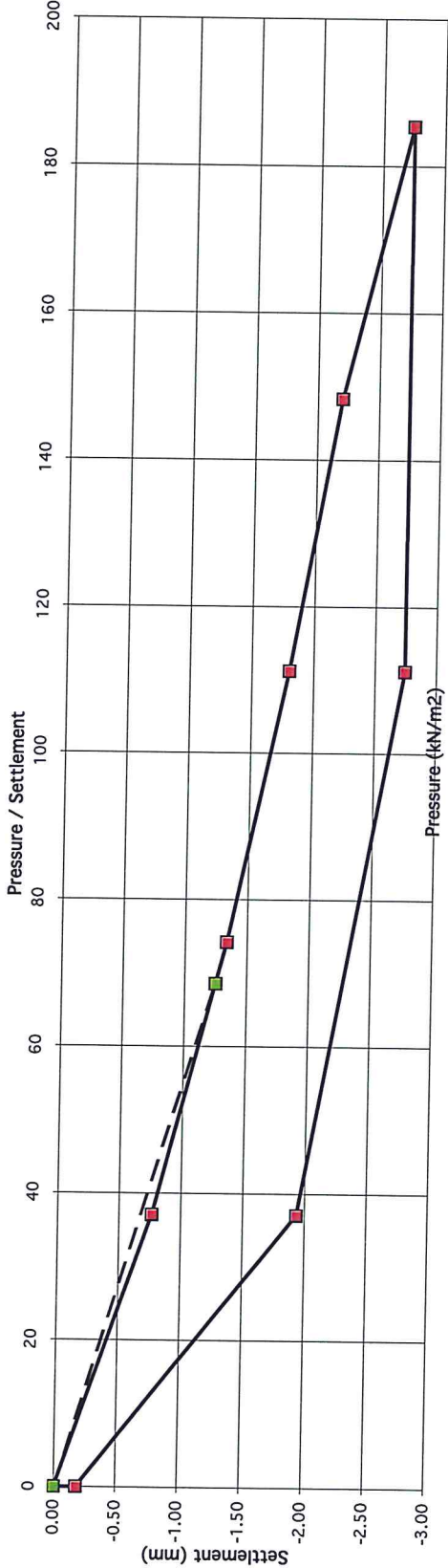
PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No. R80217	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	 
Test No. CBR17	Location 687599 217, 728320.626, 75.167	Sample Ref No. N/A Depth 0.00 m bgl	
Depth 0.5m	Client Ardstone/DBFL		
Plate Diameter: 300 mm	Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test	 <p style="text-align: center;">Pressure / Settlement</p> <p style="text-align: center;">Settlement (mm)</p> <p style="text-align: center;">Pressure (kN/m<sup>2</sup>)</p>	
Technician L. Daniels	Authorised by L. Daniels		
Date 19-06-17			
Gradient at 1.25 mm settlement intersection = 55 Modulus of subgrade reaction = 25 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 2.6 %	

PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No. R80217	Contract Capdoole Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A
Test No. CBR17 reload	Location 687599.217, 728320.626, 75.167		
Location 687599.217, 728320.626, 75.167	Depth 0.5m	IGSL Ltd. 100 Years 1917-2017	IGSL Ltd. 100 Years 1917-2017
Client Ardstone/DBFL	Plate Diameter: 300 mm		
Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test	Technician L Daniels	Applied Pressure / Settlement	
Authorised by <i>[Signature]</i>	Date 19-06-17		
Gradient at 1.25 mm settlement intersection = 85 Modulus of subgrade reaction = 39 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 5.5 %	



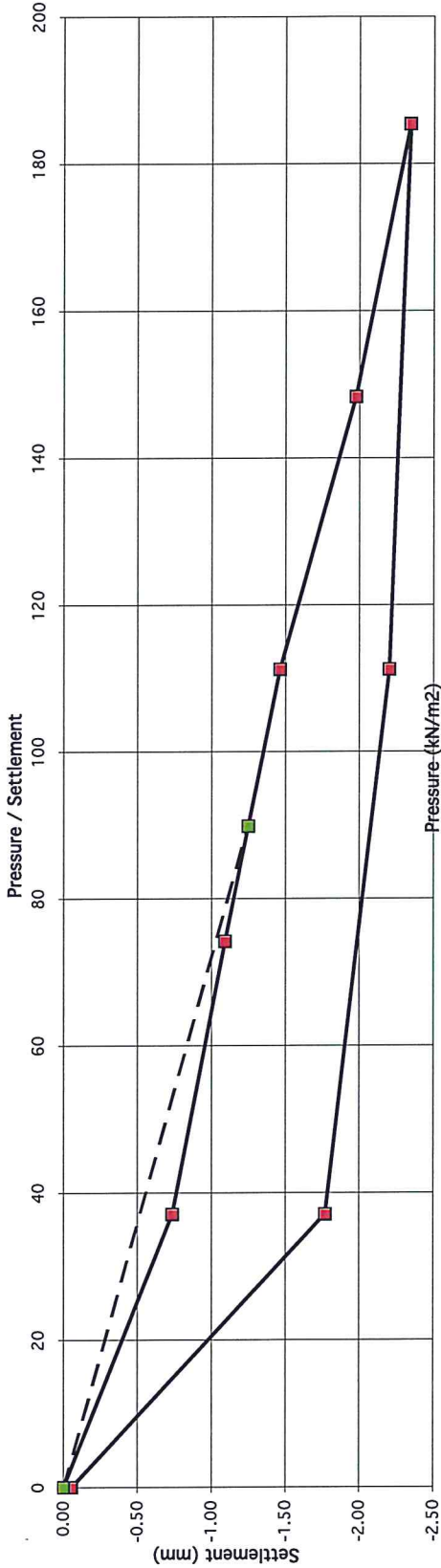
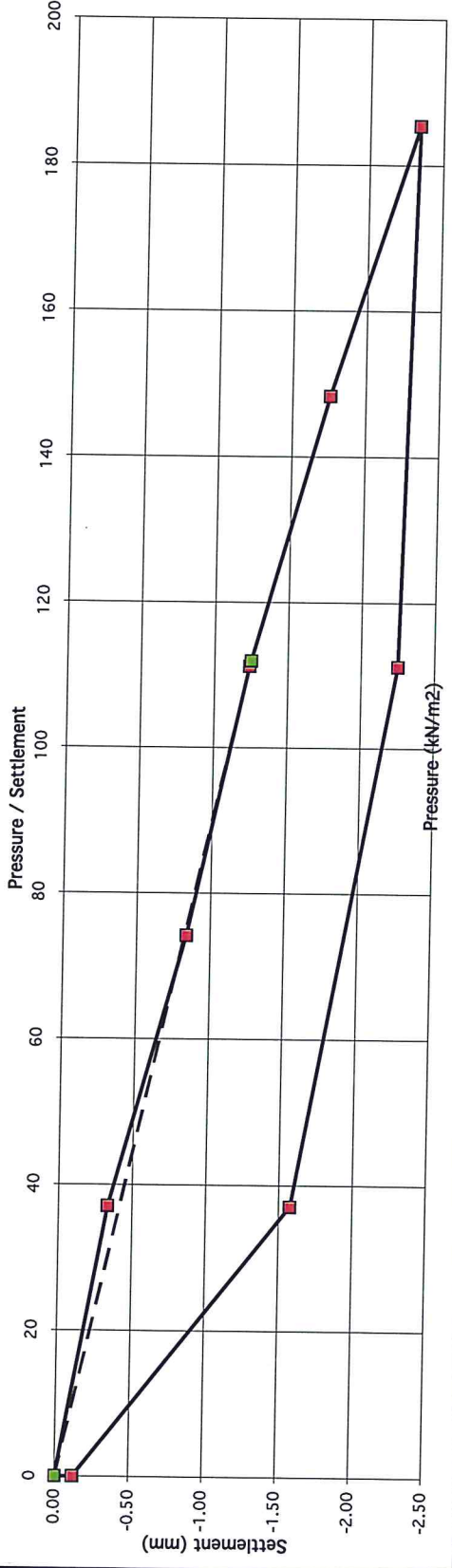
PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No. Contract Test No. Location Depth Client Plate Diameter: Test Method Technician Authorised by Date	R80218 Capdoo Clane CBR18 687662.505, 728326.399, 73.323 0.5m Ardstone/DBFL 300 mm BS 1377: Part 9: 1990 Test4 - Incremental Loading Test L. Daniels IGSL 19-06-17	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A Depth 0.00 m bgl
 			
			
Gradient at 1.25 mm settlement intersection = 72 Modulus of subgrade reaction = 33 MPa/m Correction factor applied = 0.46 as per HD 25-26/10			
Equivalent CBR value in accordance with NRA HD25-26/10 4.1 %			



PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No.	R80218	Description of soil under test (natural soil, placed fill, sub-base)	Sample Ref No.
Contract	Capdoo Cjane		
Test No.	CBR18 reload	Gravelly SILT	Depth
Location	687662.505, 728326.399, 73.323		
Depth	0.5m		m bgl
Client	Ardistone/DBFL		
Plate Diameter:	300 mm		
Test Method	BS 1377: Part 9: 1990 Test4 - Incremental Loading Test		
Technician	L. Daniels		
Authorised by			
Date	19-06-17		



Gradient at 1.25 mm settlement intersection = 90  
 Modulus of subgrade reaction = 41 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

Equivalent CBR value in accordance with NRA HD25-26/10 6.0 %




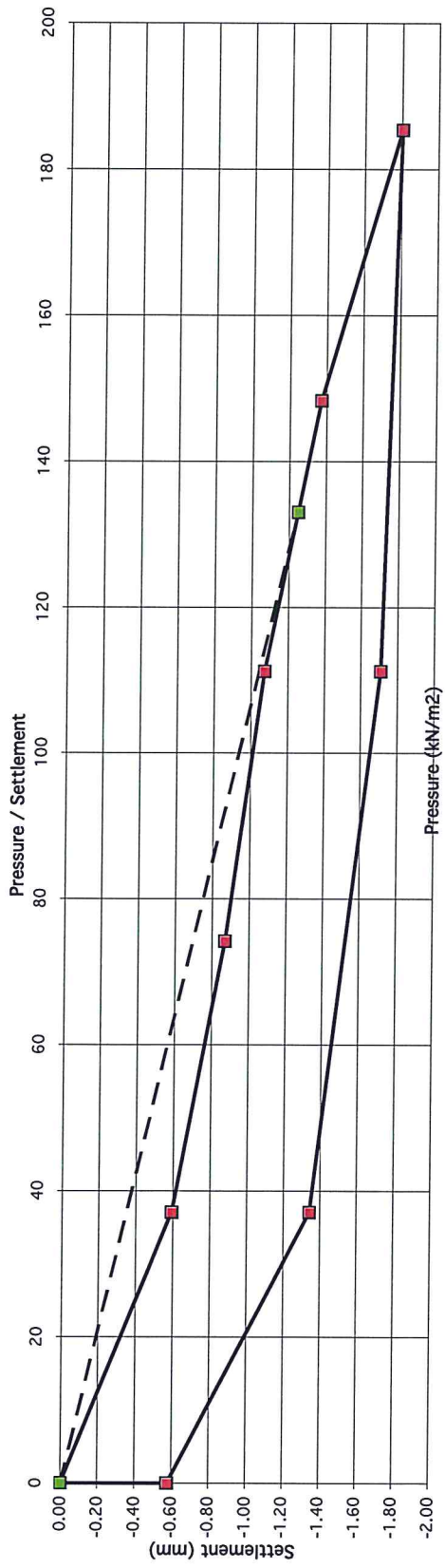


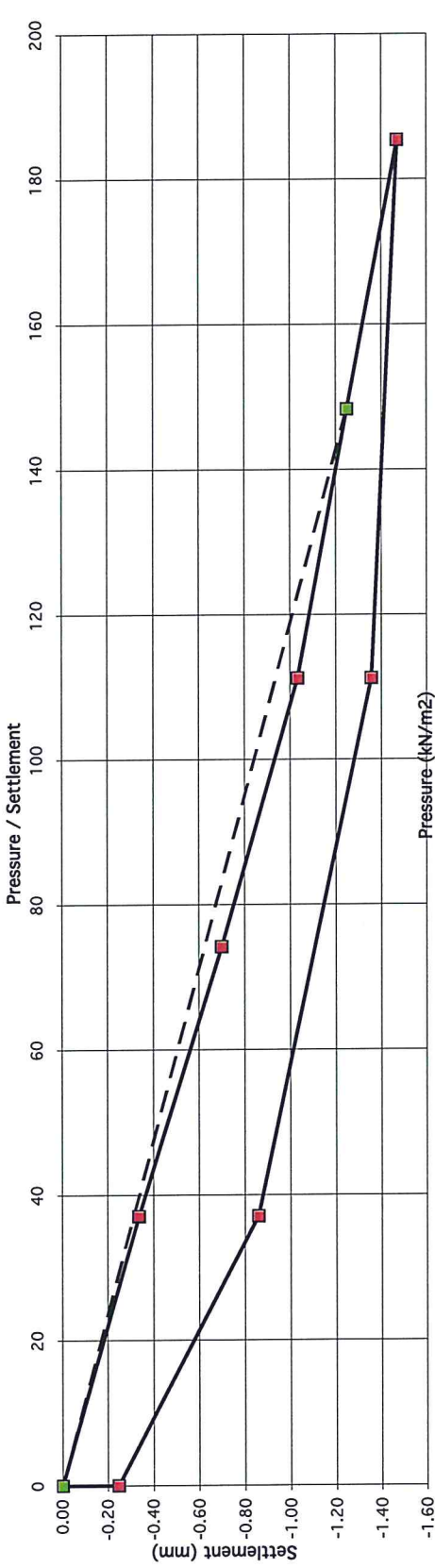
PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No.	R80219	Description of soil under test (natural soil, placed fill, sub-base)	Sample Ref No. N/A
Contract	Capdoo Clane		
Test No.	CBR19	Gravelly SILT	Depth 0.00 m bgl
Location	687726.137, 728330.736, 71.323		
Depth	0.5m		
Client	Ardstone/DBFL		
Plate Diameter:	300 mm		
Test Method	BS 1377: Part 9: 1990 Test4 - Incremental Loading Test		
Technician	L Daniels		
Authorised by			
Date	19-06-17		
 			
 <p>The graph plots Settlement (mm) on the y-axis (0 to -2.00) against Pressure / Settlement (kN/m²) on the x-axis (0 to 200). A dashed line represents the theoretical curve, and a solid line with square markers represents the experimental data. The data points are approximately: (0, 0), (37, -0.60), (74, -0.80), (111, -1.00), (148, -1.20), (185, -1.40), (222, -1.60), (259, -1.80).</p>			
Gradient at 1.25 mm settlement intersection = 106 Modulus of subgrade reaction = 49 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 8.1 %	

PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No. R80219	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	 	Sample Ref No. N/A Depth 0.00 m bgl
Contract Capdoo Glane			
Test No. CBR19 reload			
Location 687726, 137, 728330, 736, 71, 323			
Depth 0.5m			
Client Ardstone/DBFL			
Plate Diameter: 300 mm			
Test Method BS 1377: Part 9: 1990 Test 4 - Incremental Loading Test			
Technician L. Daniels			
Authorised by L. Daniels			
Date 19-06-17			
 <p>The graph plots Settlement (mm) on the y-axis (0 to -1.60) against Pressure (kN/m<sup>2</sup>) on the x-axis (0 to 200). A solid line shows the test data points, and a dashed line shows the theoretical curve. The data points are approximately: (0, 0), (10, -0.20), (30, -0.40), (70, -0.60), (100, -0.80), (110, -1.00), (140, -1.20), (180, -1.40).</p>			
Gradient at 1.25 mm settlement intersection = 119 Modulus of subgrade reaction = 54 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 9.8 %	

**PLATE TEST REPORT SHEET (F3.1)**

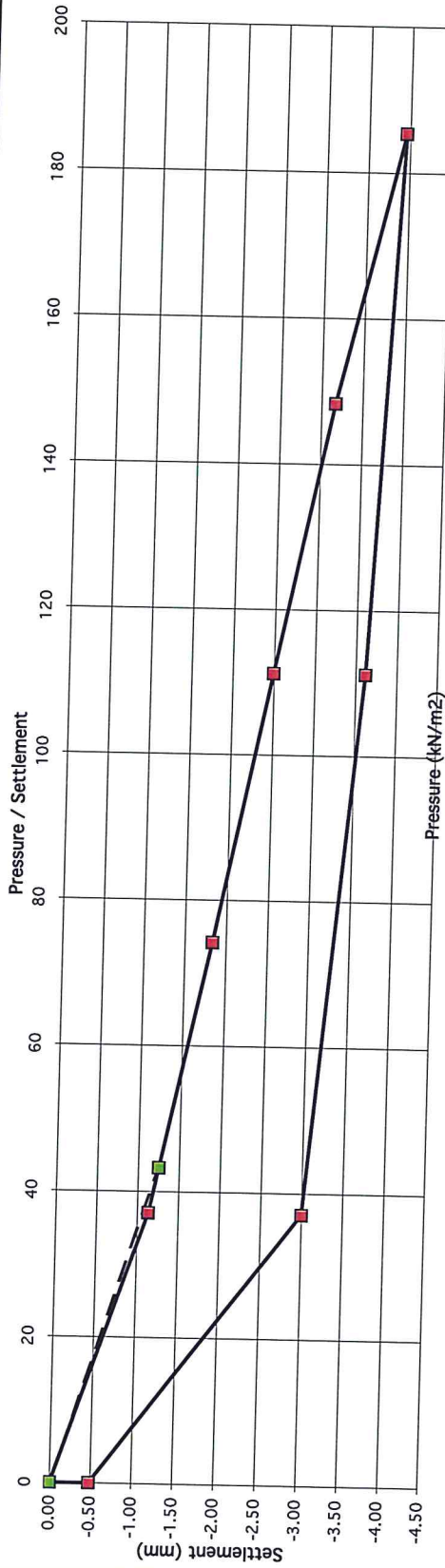
**Applied Pressure/Settlement Curve**

Reference No. R80220  
 Contract Capdoo Clane  
 Test No. CBR20  
 Location 687776.122, 728319.541, 69.608  
 Depth 0.5m  
 Client Ardstone/DBFL  
 Plate Diameter: 300 mm  
 Test Method BS 1377: Part 9: 1990 Test 4 - Incremental Loading Test  
 Technician L. Daniels  
 Authorised by [Signature]  
 Date 19-06-17

Description of soil under test  
 (natural soil, placed fill, sub-base)  
 Gravelly SILT



Sample Ref No. N/A  
 Depth 0.00 m bgl



Gradient at 1.25 mm settlement intersection = 35  
 Modulus of subgrade reaction = 16 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

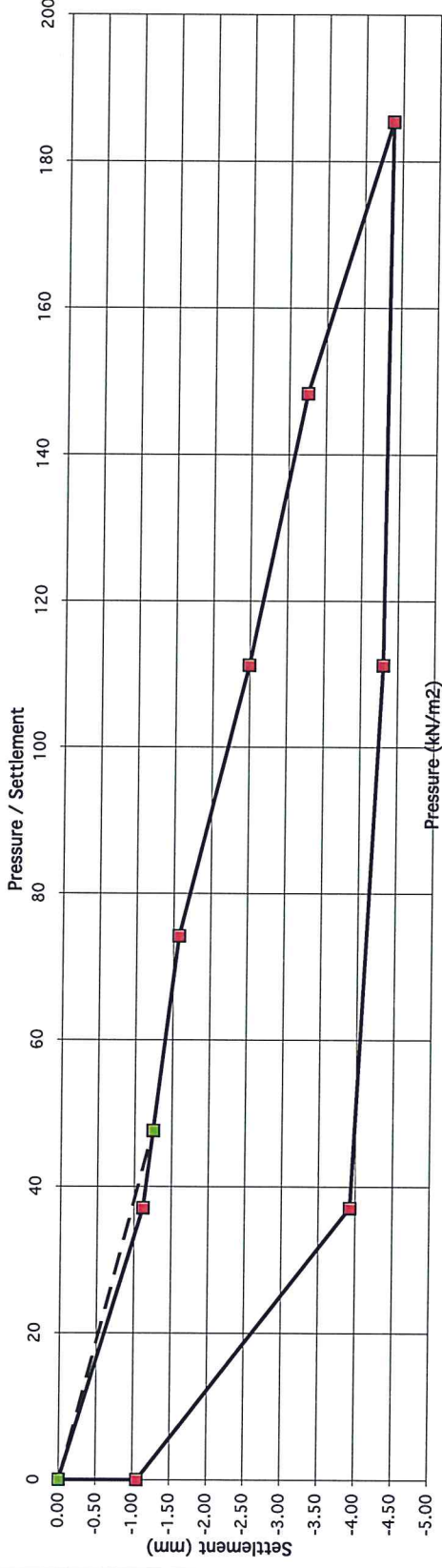
Equivalent CBR value in accordance with NRA HD25-26/10

1.2 %

PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve																							
Reference No. R80220	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A																						
Test No. CBR20 reload	Location 687776.122, 728319.541, 69.608			Depth 0.00 m bgl																					
Location 687776.122, 728319.541, 69.608	Depth 0.5m	IGSL Ltd.	NAB																						
Client Ardstone/DBFL	Plate Diameter: 300 mm																								
Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test	Technician L. Daniels	Applied Pressure / Settlement																							
Authorised by <i>[Signature]</i>	Date 19-06-17	<table border="1"> <caption>Applied Pressure / Settlement Curve Data Points</caption> <thead> <tr> <th>Pressure (kN/m<sup>2</sup>)</th> <th>Settlement (mm)</th> </tr> </thead> <tbody> <tr><td>0.00</td><td>0.00</td></tr> <tr><td>0.50</td><td>-0.50</td></tr> <tr><td>1.00</td><td>-1.00</td></tr> <tr><td>1.50</td><td>-1.50</td></tr> <tr><td>2.00</td><td>-2.00</td></tr> <tr><td>2.50</td><td>-2.50</td></tr> <tr><td>3.00</td><td>-3.00</td></tr> <tr><td>3.50</td><td>-3.50</td></tr> <tr><td>4.00</td><td>-4.00</td></tr> <tr><td>4.50</td><td>-4.50</td></tr> </tbody> </table>		Pressure (kN/m <sup>2</sup> )	Settlement (mm)	0.00	0.00	0.50	-0.50	1.00	-1.00	1.50	-1.50	2.00	-2.00	2.50	-2.50	3.00	-3.00	3.50	-3.50	4.00	-4.00	4.50	-4.50
Pressure (kN/m <sup>2</sup> )	Settlement (mm)																								
0.00	0.00																								
0.50	-0.50																								
1.00	-1.00																								
1.50	-1.50																								
2.00	-2.00																								
2.50	-2.50																								
3.00	-3.00																								
3.50	-3.50																								
4.00	-4.00																								
4.50	-4.50																								
Gradient at 1.25 mm settlement intersection = 50 Modulus of subgrade reaction = 23 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 2.2 %																							

**PLATE TEST REPORT SHEET (F3.1)**

Reference No. R80221 Contract Capdoo Crane Test No. CBR21 Location 687588.623, 728231.419, 73.716 Depth 0.5m Client Ardstone/DBFL Plate Diameter: 300 mm Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test Technician L. Daniels Authorised by Date 19-06-17	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A Depth 0.00 m bgl
---	--	--



Gradient at 1.25 mm settlement intersection = 38  
 Modulus of subgrade reaction = 17 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10  
 Equivalent CBR value in accordance with NRA HD25-26/10 1.4 %

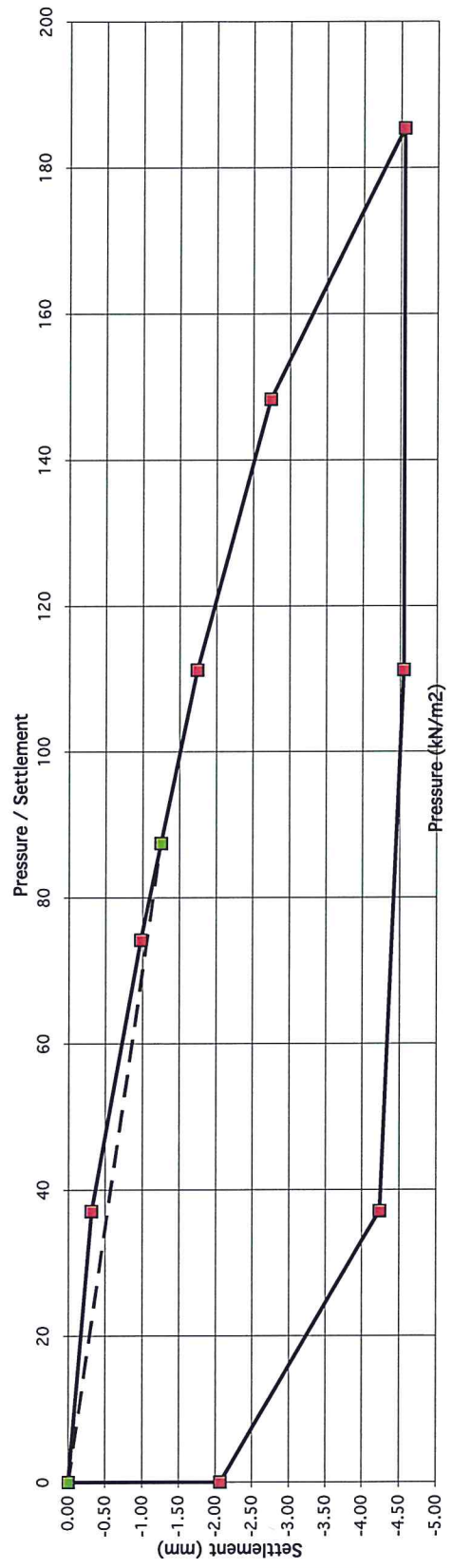
**PLATE TEST REPORT SHEET (F3.1)**

**Applied Pressure/Settlement Curve**

Reference No. R80221  
 Contract Capdoo Clane  
 Test No. CBR21 reload  
 Location 687588.623, 728231.419, 73.716  
 Depth 0.5m  
 Client Ardstone/DBFL  
 Plate Diameter: 300 mm  
 Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test  
 Technician L. Daniels  
 Authorised by  
 Date 19-06-17



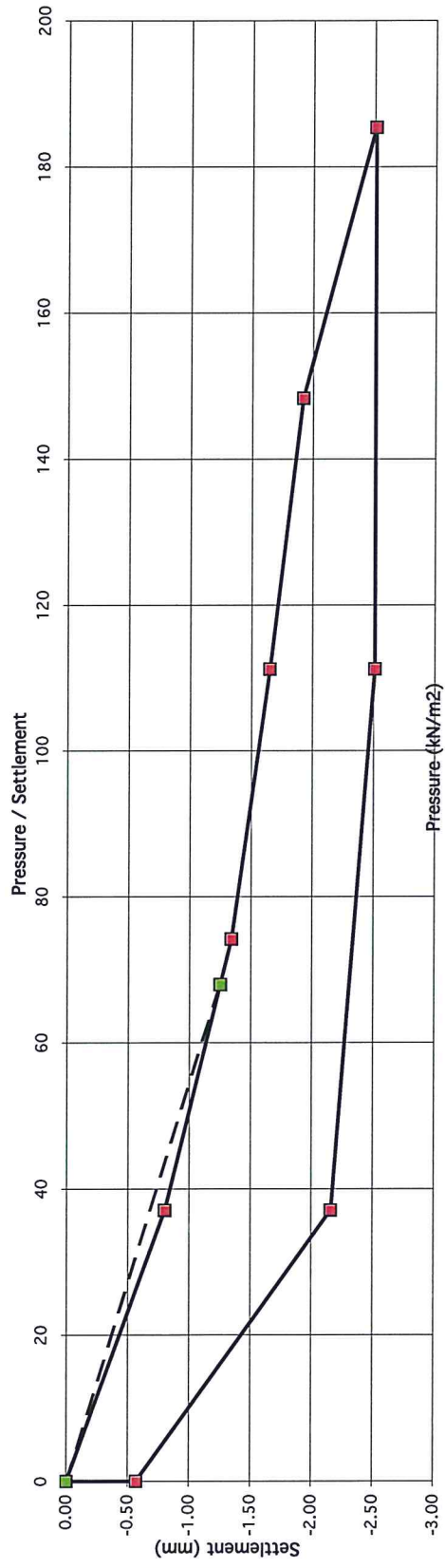
Description of soil under test  
 (natural soil, placed fill, sub-base)  
 Gravelly SILT

Sample Ref No. N/A  
 Depth 0.00 m bgl



Gradient at 1.25 mm settlement intersection = 70  
 Modulus of subgrade reaction = 32 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

Equivalent CBR value in accordance with NRA HD25-26/10  
 3.9 %

PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No. R80222	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A
Test No. CBR22	Location 687577.681, 728212.567, 74.216		
Depth 0.5m	Client Ardstone/DBFL	 	
Plate Diameter: 300 mm	Technician L. Daniels		
Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test	Authorised by <i>L. Daniels</i>		
Date 19-06-17			
 <p>The graph plots Settlement (mm) on the y-axis (0 to -3.00) against Pressure / Settlement (kN/m<sup>2</sup>) on the x-axis (0 to 200). A solid line with red square markers shows the test data points, and a dashed line shows the theoretical curve. The data points are approximately: (0, 0), (25, -0.5), (35, -1.0), (70, -1.5), (110, -2.0), (150, -2.5), (185, -3.0).</p>			
Gradient at 1.25 mm settlement intersection = 54 Modulus of subgrade reaction = 25 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 2.5 %	



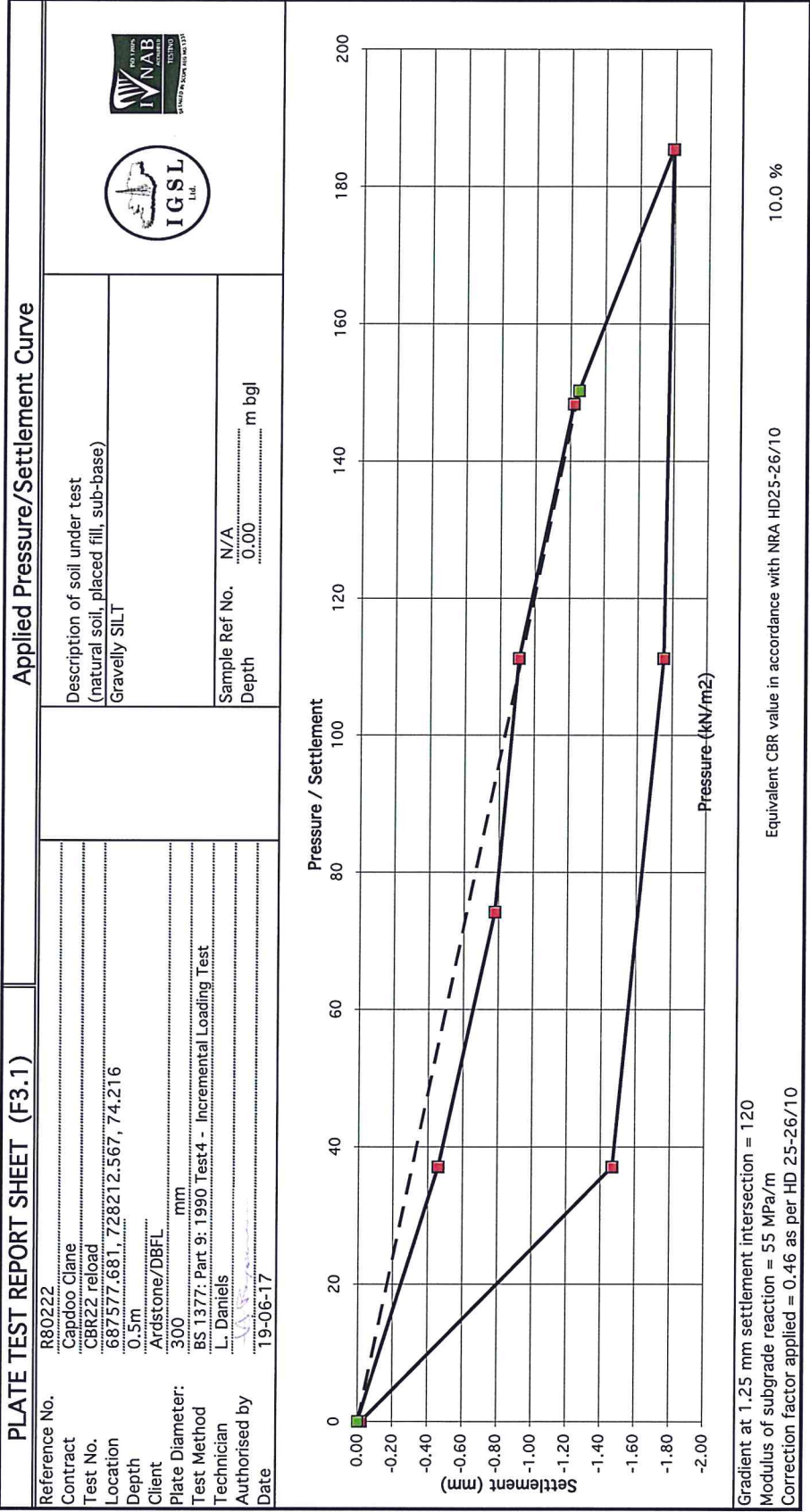






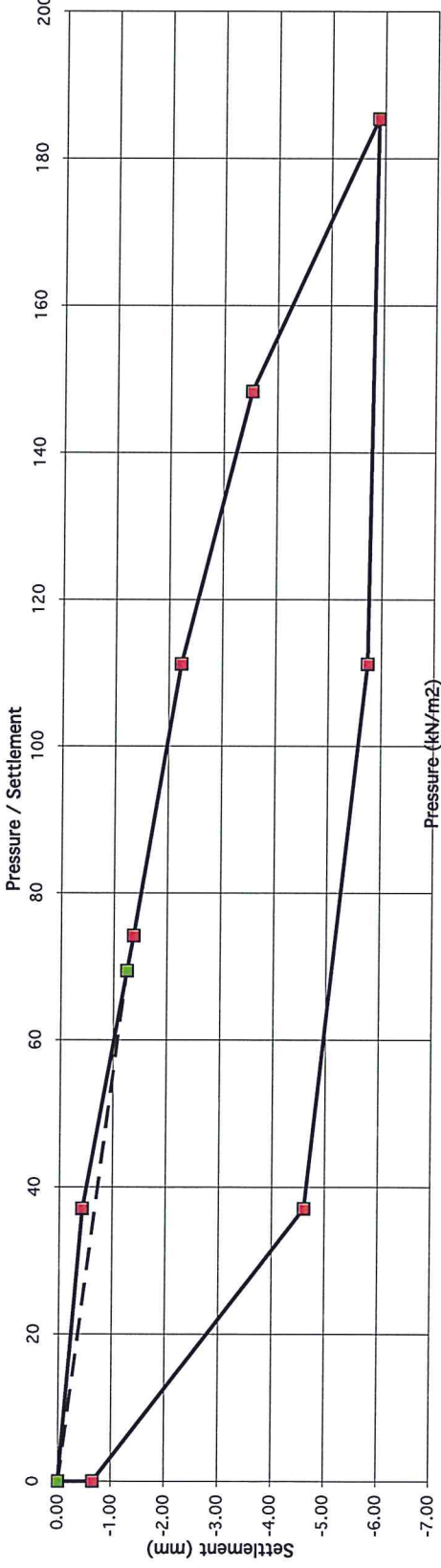
PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve																	
Reference No. R80223	Contract Capdoo Clane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A																
Test No. CBR23	Location 687718.138, 728235.801, 71.321																		
Depth 0.5m	Client Ardstone/DBFL	Depth 0.00	..... m bgl																
Plate Diameter: 300 mm	Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test																		
Technician L. Daniels	Authorised by <i>L. Daniels</i>																		
Date 19-06-17																			
		 																	
<table border="1"> <caption>Applied Pressure/Settlement Curve Data</caption> <thead> <tr> <th>Pressure (kN/m<sup>2</sup>)</th> <th>Settlement (mm)</th> </tr> </thead> <tbody> <tr><td>0</td><td>0.00</td></tr> <tr><td>10</td><td>-0.50</td></tr> <tr><td>35</td><td>-1.20</td></tr> <tr><td>75</td><td>-2.00</td></tr> <tr><td>110</td><td>-3.00</td></tr> <tr><td>148</td><td>-4.00</td></tr> <tr><td>185</td><td>-5.00</td></tr> </tbody> </table>				Pressure (kN/m <sup>2</sup> )	Settlement (mm)	0	0.00	10	-0.50	35	-1.20	75	-2.00	110	-3.00	148	-4.00	185	-5.00
Pressure (kN/m <sup>2</sup> )	Settlement (mm)																		
0	0.00																		
10	-0.50																		
35	-1.20																		
75	-2.00																		
110	-3.00																		
148	-4.00																		
185	-5.00																		
Gradient at 1.25 mm settlement intersection = 33 Modulus of subgrade reaction = 15 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 1.1 %																	

PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No. R80223	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	 	Sample Ref No. N/A Depth 0.00 m bgl
Contract Capdoo Glane Test No. CBR23 reload Location 687718.138, 728235.801, 71.321 Depth 0.5m Client Ardstone/DBFL Plate Diameter: 300 mm Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test Technician L. Daniels Authorised by L. Daniels Date 19-06-17			
 <p>The graph plots Settlement (mm) on the y-axis (0 to -7.00) against Pressure (kN/m<sup>2</sup>) on the x-axis (0 to 200). A solid line with red square markers shows the test data points, and a dashed line shows the theoretical curve. The data points are approximately: (0, 0), (35, -0.5), (70, -1.0), (110, -1.5), (145, -2.0), (185, -2.5).</p>			
Gradient at 1.25 mm settlement intersection = 56 Modulus of subgrade reaction = 25 MPa/m Correction factor applied = 0.46 as per HD 25-26/10			
Equivalent CBR value in accordance with NRA HD25-26/10 2.6 %			

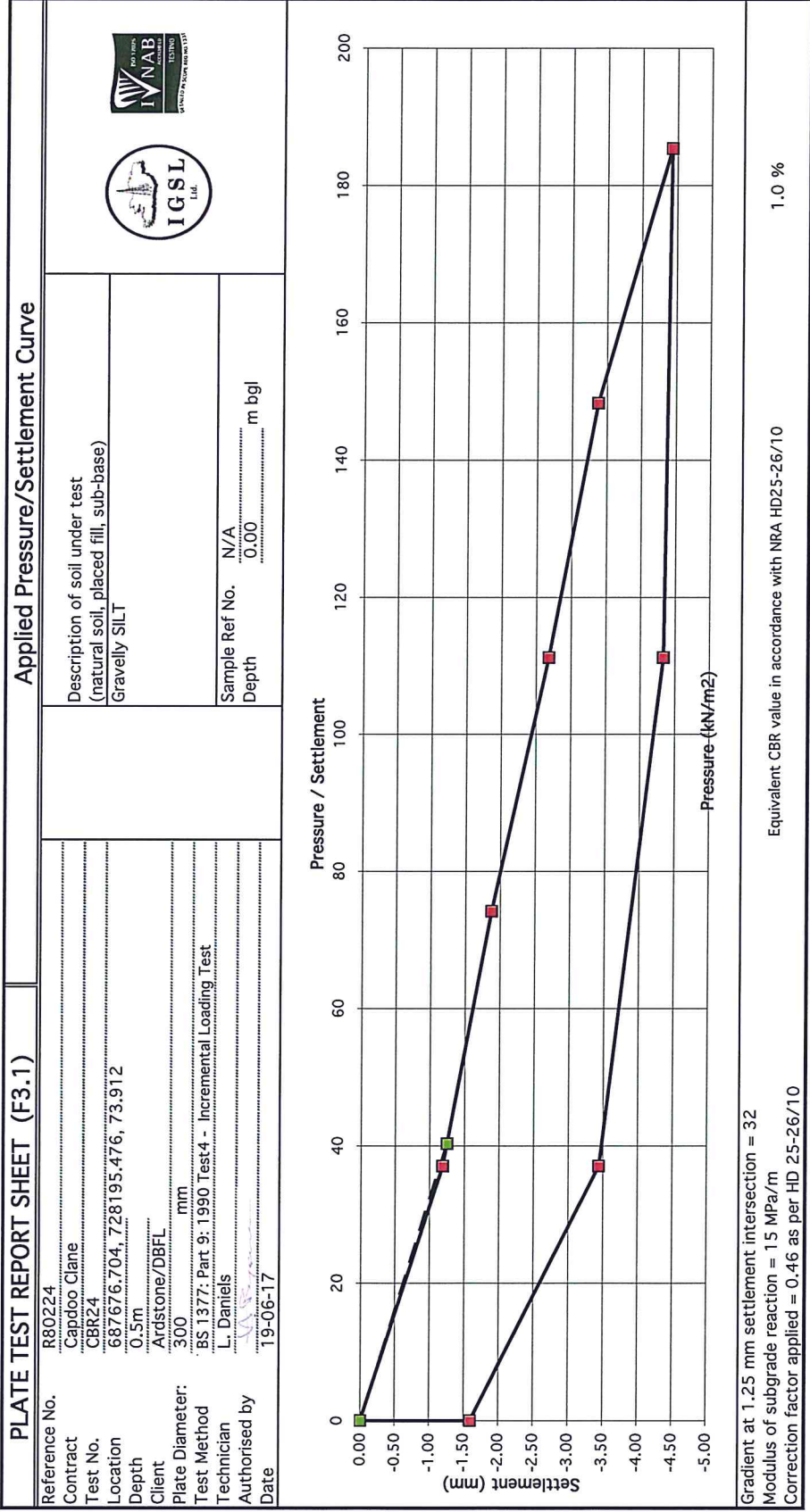


PLATE TEST REPORT SHEET (F3.1)		Applied Pressure/Settlement Curve	
Reference No. R80224	Contract Capdoo Glane	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT	Sample Ref No. N/A
Test No. CBR24 reload	Location 687676.704, 728195.476, 73.912		
Location 687676.704, 728195.476, 73.912	Depth 0.5m	IGSL LTD	INAB INCORPORATED
Client Ardstone/DBFL	Plate Diameter: 300 mm		
Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test	Technician L. Daniels	Applied Pressure / Settlement	
Authorised by	Date 19-06-17	<p>Pressure (kN/m<sup>2</sup>)</p> <p>Settlement (mm)</p>	
Gradient at 1.25 mm settlement intersection = 43 Modulus of subgrade reaction = 19 MPa/m Correction factor applied = 0.46 as per HD 25-26/10		Equivalent CBR value in accordance with NRA HD25-26/10 1.7 %	

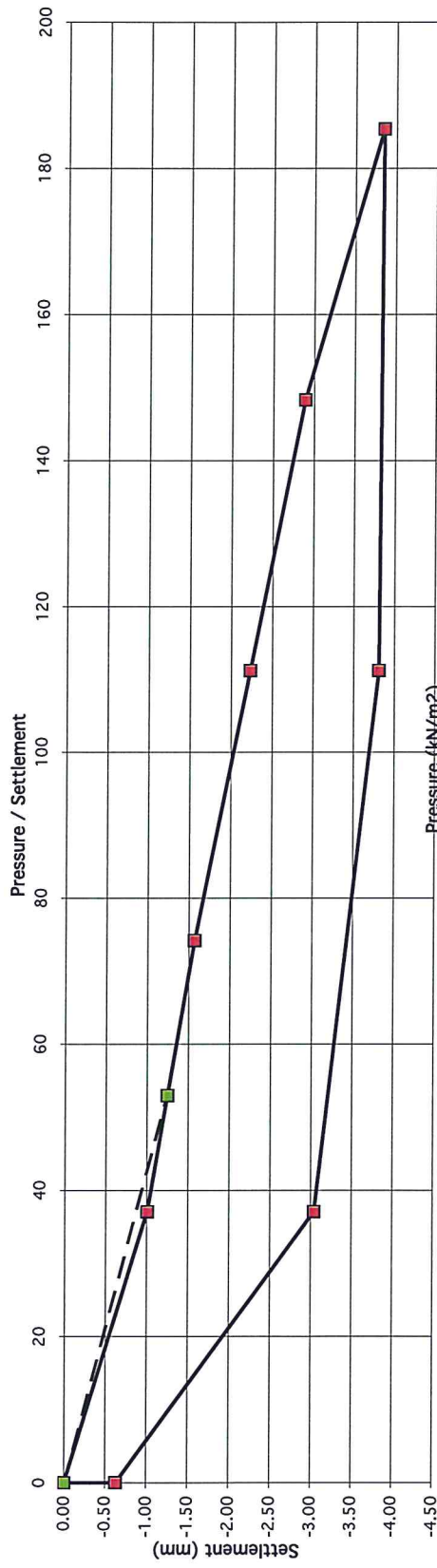
**PLATE TEST REPORT SHEET (F3.1)**

**Applied Pressure/Settlement Curve**

Reference No. R80225  
 Contract Capdoo Clane  
 Test No. CBR25  
 Location See map  
 Depth 0.5m  
 Client Ardstone/DBFL  
 Plate Diameter: 300 mm  
 Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test  
 Technician L. Daniels  
 Authorised by *L. Daniels*  
 Date 16-06-17

Description of soil under test  
 (natural soil, placed fill, sub-base)  
 Gravelly SILT

Sample Ref No. N/A  
 Depth 0.00 m bgl





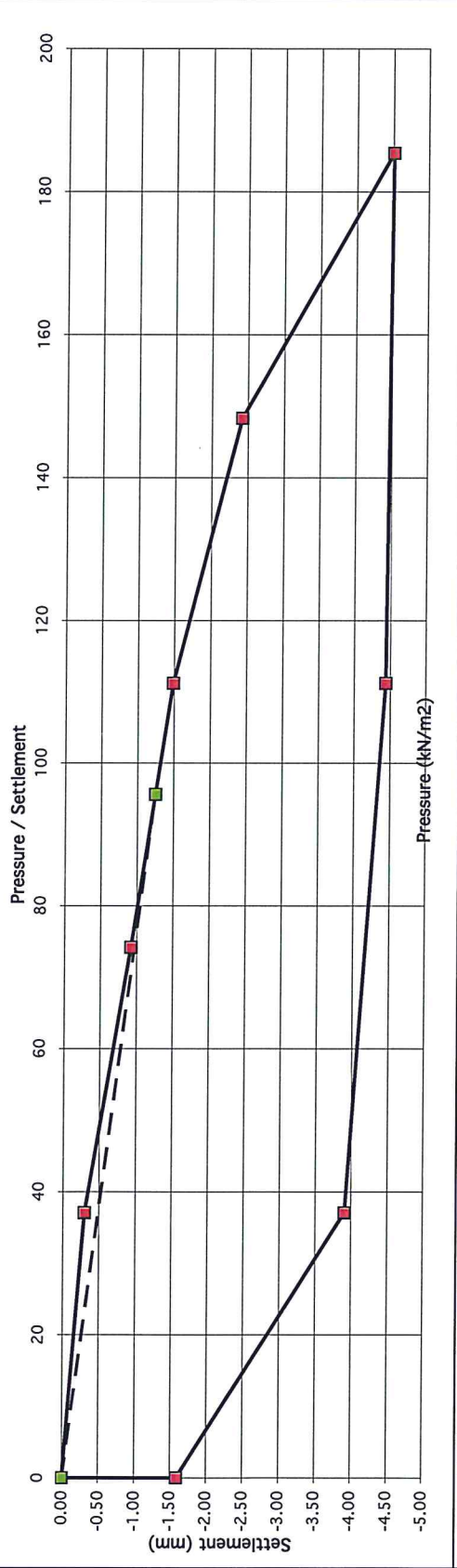
Gradient at 1.25 mm settlement intersection = 42  
 Modulus of subgrade reaction = 19 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10

Equivalent CBR value in accordance with NRA HD25-26/10

1.6 %

**PLATE TEST REPORT SHEET (F3.1)**

Reference No. R80225 Contract Capdoo Clane Test No. CBR25 reload Location 687631.745, 728185.586, 75.104 Depth 0.5m Client Ardstone/DBFL Plate Diameter: 300 mm Test Method BS 1377: Part 9: 1990 Test4 - Incremental Loading Test Technician L. Daniels Authorised by <i>LA</i> Date 16-06-17	Description of soil under test (natural soil, placed fill, sub-base) Gravelly SILT  Sample Ref No. N/A Depth 0.00 m bgl	 
--	--	--



Gradient at 1.25 mm settlement intersection = 77  
 Modulus of subgrade reaction = 35 MPa/m  
 Correction factor applied = 0.46 as per HD 25-26/10  
 Equivalent CBR value in accordance with NRA HD25-26/10 4.6 %

## **Appendix V BRE Digest 365 Tests**



# Soakaway

IGSL

Contract: Capdoo, Clane

Contract No.

20159

Test No. IT01

Client Ardstone/DBFL

Date: 22/06/2017

## Summary of ground conditions

from	to	Description	Ground water
0.00	0.50	TOPSOIL	
0.50	2.30	Brown gravelly SILT. Gravel fine to coarse subangular.	

Notes: Location: 687650.505, 728377.037, 75.419

## Field Data

## Field Test

Depth to Water (m)	Elapsed Time (min)
1.65	0.00
1.65	1.00
1.65	2.00
1.65	3.00
1.65	4.00
1.65	5.00
1.65	10.00
1.65	15.00
1.65	20.00
1.65	30.00
1.65	40.00
1.65	60.00

Depth of Pit (D)  m  
 Width of Pit (B)  m  
 Length of Pit (L)  m

Initial depth to Water =  m  
 Final depth to water =  m  
 Elapsed time (mins)=

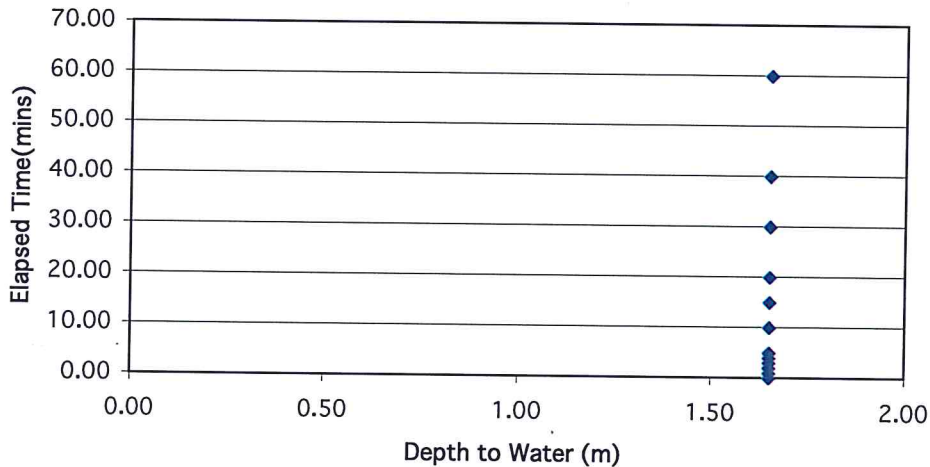
Top of permeable soil  m  
 Base of permeable soil  m

Base area=  m<sup>2</sup>  
 \*Av. side area of permeable stratum over test period  m<sup>2</sup>  
 Total Exposed area =  m<sup>2</sup>

Infiltration rate (f) = Volume of water used/unit exposed area / unit time

f= 0 m/min or 0 m/sec

Depth of water vs Elapsed Time (mins)



# Soakaway

**IGSL**

Contract: Capdoo, Clane

Test No. IT02

Contract No.

20159

Client Ardstone/DBFL

Date: 22/06/2017

## Summary of ground conditions

from	to	Description	Ground water
0.00	0.50	TOPSOIL	
0.50	2.50	Black gravelly medium to coarse gritty SAND	

Notes: Location: 687758.740, 728337.281, 69.924

## Field Data

Depth to Water (m)	Elapsed Time (min)
1.66	0.00
1.67	1.00
1.68	2.00
1.69	3.00
1.70	4.00
1.71	5.00
1.72	10.00
1.73	15.00
1.74	20.00
1.77	30.00
1.80	40.00
1.85	60.00
1.92	90.00

## Field Test

Depth of Pit (D) 

2.50
------

 m  
 Width of Pit (B) 

0.40
------

 m  
 Length of Pit (L) 

1.70
------

 m

Initial depth to Water = 

1.66
------

 m  
 Final depth to water = 

1.92
------

 m  
 Elapsed time (mins)= 

90.00
-------

Top of permeable soil 

--

 m  
 Base of permeable soil 

--

 m

Base area= 

0.68
------

 m<sup>2</sup>  
 \*Av. side area of permeable stratum over test period 

2.982
-------

 m<sup>2</sup>  
 Total Exposed area = 

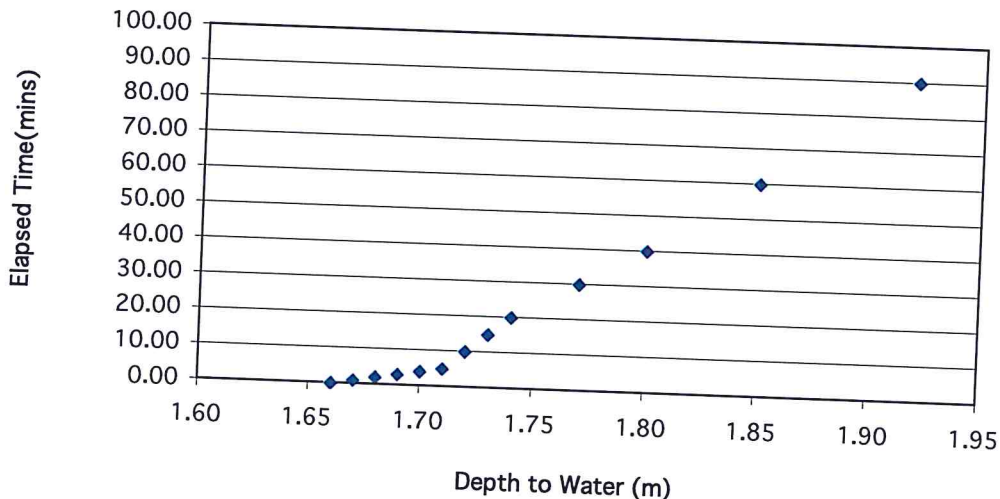
3.662
-------

 m<sup>2</sup>

Infiltration rate (f) = Volume of water used/unit exposed area / unit time

f= 0.00054 m/min or 8.941E-06 m/sec

Depth of water vs Elapsed Time (mins)



# Soakaway

IGSL

Contract: Capdoo, Clane

Test No. IT03

Contract No.

20159

Client Ardstone/DBFL

Date: 21/06/2017

## Summary of ground conditions

from	to	Description	Ground water
0.00	0.60	TOPSOIL	
0.60	1.60	Grey silty fine to coarse SAND	
1.60	2.50	Grey silty gravelly fine to coarse SAND	

Notes: Location: 687729.310, 728440.316, 72.962

## Field Data

Depth to Water (m)	Elapsed Time (min)
1.50	0.00
1.51	1.00
1.52	2.00
1.53	3.00
1.54	4.00
1.56	5.00
1.65	10.00
1.72	15.00
1.77	20.00
1.82	30.00
1.90	40.00
2.06	60.00
2.22	90.00

## Field Test

Depth of Pit (D)  m  
 Width of Pit (B)  m  
 Length of Pit (L)  m

Initial depth to Water =  m  
 Final depth to water =  m  
 Elapsed time (mins)=

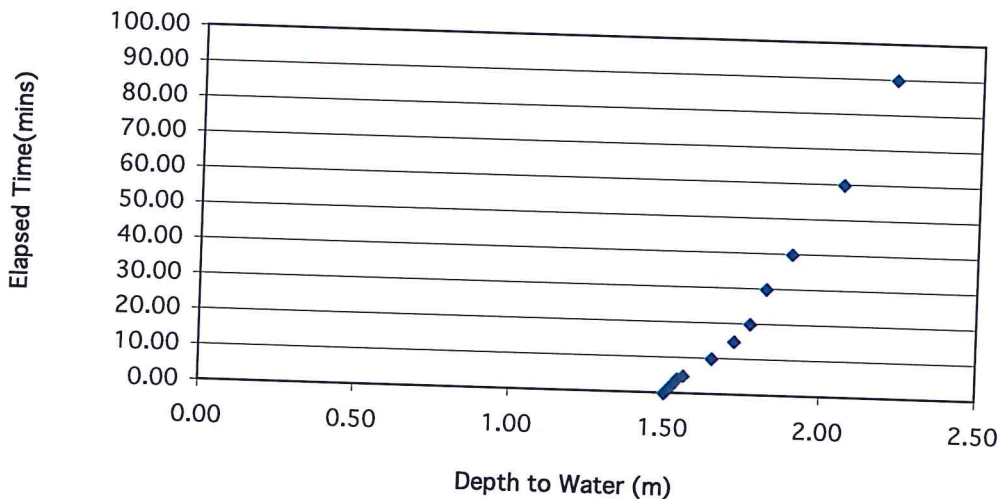
Top of permeable soil  m  
 Base of permeable soil

Base area=  m<sup>2</sup>  
 \*Av. side area of permeable stratum over test period  m<sup>2</sup>  
 Total Exposed area =  m<sup>2</sup>

Infiltration rate (f) = Volume of water used/unit exposed area / unit time

f= 0.00163 m/min or 2.715E-05 m/sec

Depth of water vs Elapsed Time (mins)



# Soakaway

IGSL

Contract: Capdoo, Clane  
 Test No. IT04  
 Client Ardstone/DBFL  
 Date: 21/06/2017

Contract No. 20159

## Summary of ground conditions

from	to	Description	Ground water
0.00	0.50	TOPSOIL	
0.50	1.90	Grey slightly silty fine to coarse SAND	
1.90	2.50	Grey gravelly moderately cobbly fine to coarse SAND	

Notes: Location: 687749.826, 728441.334, 71.325

## Field Data

Depth to Water (m)	Elapsed Time (min)
1.38	0.00
1.39	1.00
1.40	2.00
1.41	3.00
1.43	4.00
1.45	5.00
1.46	6.00
1.48	7.00
1.49	8.00
1.49	9.00
1.50	10.00
1.53	15.00
1.55	20.00
1.68	40.00
1.80	60.00
1.90	90.00

## Field Test

Depth of Pit (D) = 2.50 m  
 Width of Pit (B) = 0.40 m  
 Length of Pit (L) = 2.10 m

Initial depth to Water = 1.38 m  
 Final depth to water = 1.90 m  
 Elapsed time (mins) = 90.00

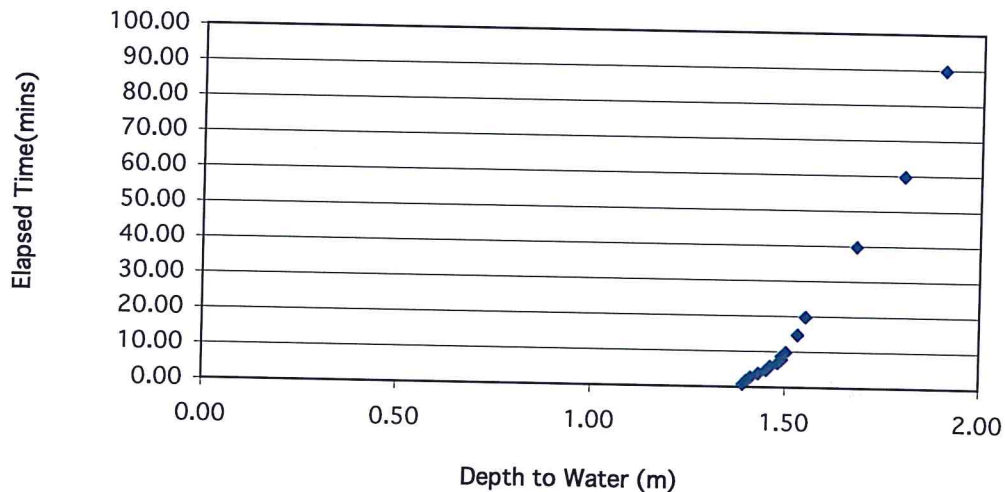
Top of permeable soil = m  
 Base of permeable soil = m

Base area = 0.84 m<sup>2</sup>  
 \*Av. side area of permeable stratum over test period = 4.3 m<sup>2</sup>  
 Total Exposed area = 5.14 m<sup>2</sup>

Infiltration rate (f) = Volume of water used/unit exposed area / unit time

f = 0.00094 m/min or 1.574E-05 m/sec

Depth of water vs Elapsed Time (mins)



# Soakaway

IGSL

Contract: Capdoo, Clane  
 Test No. IT05  
 Client Ardstone/DBFL  
 Date: 21/06/2017

Contract No. 20159

## Summary of ground conditions

from	to	Description	Ground water
0.00	0.50	TOPSOIL	1.30m
0.30	1.60	Grey silty fine to coarse subangular to subrounded GRAVEL	

Notes: Location: 687850.393, 728469.376 ,68.013  
 Moderate seepage at 1.50m. Groundwater settled at 1.30m after a period of 30 minutes.

## Field Data

## Field Test

Depth to Water (m)	Elapsed Time (min)
NA	NA

Depth of Pit (D)  m  
 Width of Pit (B)  m  
 Length of Pit (L)  m

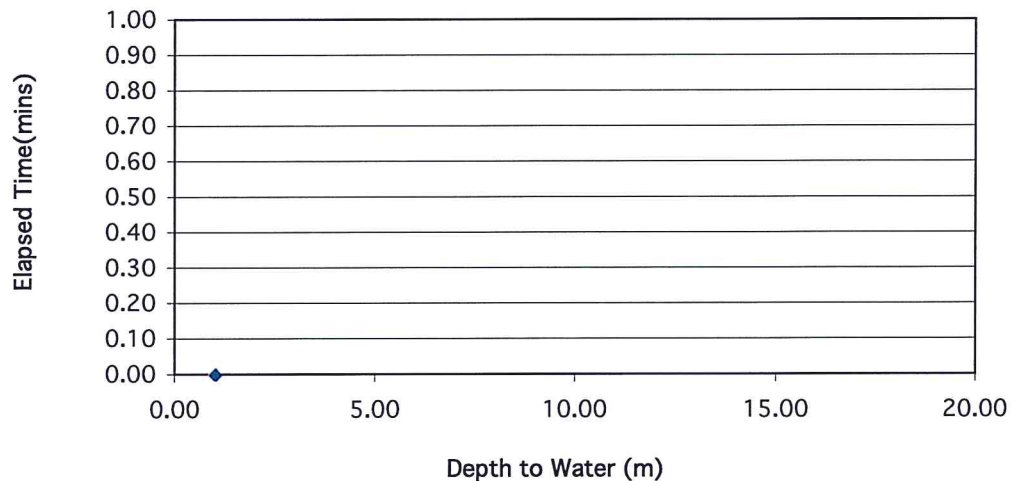
Initial depth to Water =   
 Final depth to water =  m  
 Elapsed time (mins) =

Top of permeable soil   
 Base of permeable soil  m

Base area =  m<sup>2</sup>  
 \*Av. side area of permeable stratum over test period  m<sup>2</sup>  
 Total Exposed area =  m<sup>2</sup>

Infiltration rate (f) =      Volume of water used/unit exposed area / unit time  
 f =  m/min      or       m/sec

Depth of water vs Elapsed Time (mins)



# Soakaway

IGSL

Contract: Capdoo, Clane  
 Test No. IT06  
 Client Ardstone/DBFL  
 Date: 21/06/2017

Contract No. 20159

### Summary of ground conditions

from	to	Description	Ground water
0.00	0.30	TOPSOIL	0.90m
0.30	1.20	Grey silty fine to coarse subangular to subrounded GRAVEL	

Notes: Location: 687855.724, 728492.341, 67.366  
 Moderate seepage at 1.20m. Groundwater settled at 0.90m after a period of 30 minutes.

#### Field Data

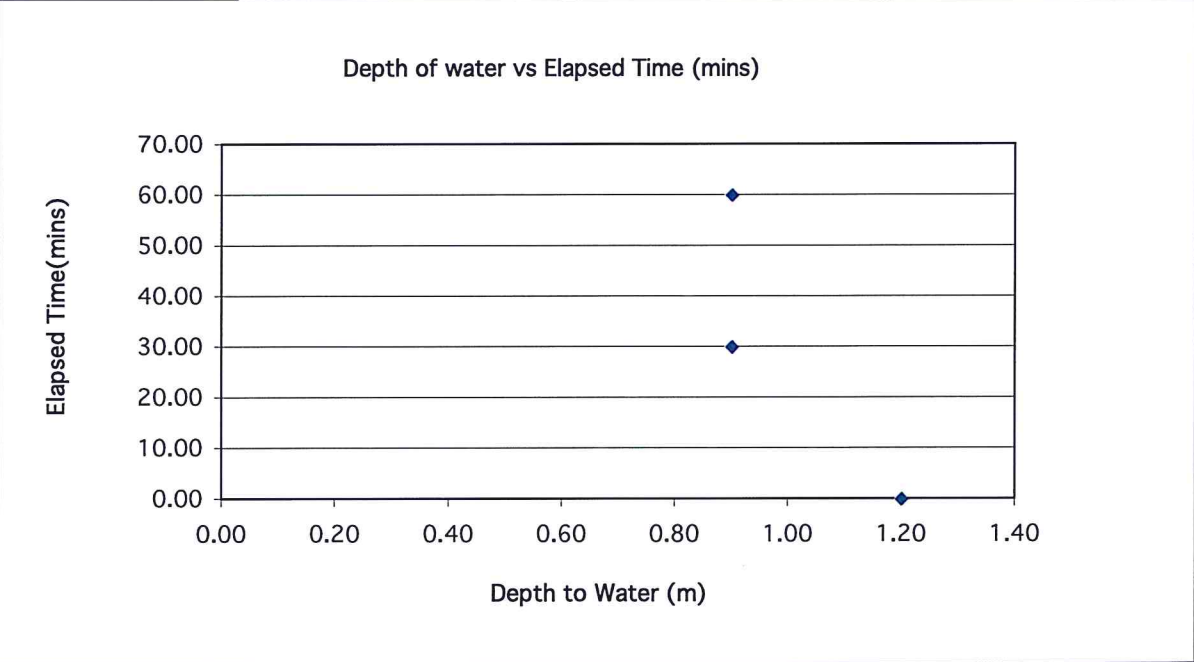
Depth to Water (m)	Elapsed Time (min)
1.20	0.00
0.90	30.00
0.90	60.00

#### Field Test

Depth of Pit (D)	<input type="text" value="1.20"/>	m
Width of Pit (B)	<input type="text" value="0.40"/>	m
Length of Pit (L)	<input type="text" value="1.50"/>	m
Initial depth to Water =	<input type="text" value="1.20"/>	m
Final depth to water =	<input type="text" value="0.90"/>	m
Elapsed time (mins)=	<input type="text" value="60.00"/>	
Top of permeable soil	<input type="text"/>	m
Base of permeable soil	<input type="text"/>	m

Base area=	<input type="text" value="0.6"/>	m2
*Av. side area of permeable stratum over test period	<input type="text" value="0.57"/>	m2
Total Exposed area =	<input type="text" value="1.17"/>	m2

Infiltration rate (f) =  $\frac{\text{Volume of water used/unit exposed area}}{\text{unit time}}$   
 $f = -0.0026 \text{ m/min} \quad \text{or} \quad -4.274\text{E-}05 \text{ m/sec}$



# Soakaway

IGSL

Contract: Capdoo, Clane  
 Test No. IT07  
 Client Ardstone/DBFL  
 Date: 22/06/2017

Contract No. 20159

## Summary of ground conditions

from	to	Description	Ground water
0.00	0.70	TOPSOIL	
0.70	1.30	Brown slightly sandy gravelly SILT	
1.30	1.80	Grey slightly silty sandy fine to coarse gritty GRAVEL	
1.80	2.30	Brown gravelly fine to medium SAND	

Notes:

### Field Data

Depth to Water (m)	Elapsed Time (min)
1.70	0.00
1.71	1.00
1.72	2.00
1.74	3.00
1.75	4.00
1.76	5.00
1.80	10.00
1.83	15.00
1.86	20.00
1.92	30.00
1.96	40.00
2.15	60.00
2.30	90.00

### Field Test

Depth of Pit (D)	2.30	m
Width of Pit (B)	0.40	m
Length of Pit (L)	2.00	m

Initial depth to Water =	1.70	m
Final depth to water =	2.30	m
Elapsed time (mins)=	90.00	

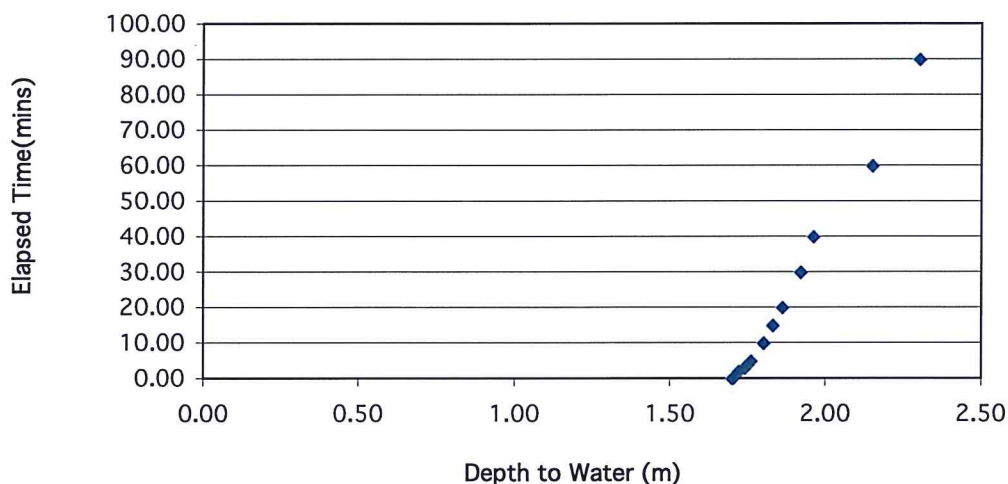
Top of permeable soil		m
Base of permeable soil		m

Base area=	0.8	m <sup>2</sup>
*Av. side area of permeable stratum over test period	1.44	m <sup>2</sup>
Total Exposed area =	2.24	m <sup>2</sup>

Infiltration rate (f) = Volume of water used/unit exposed area / unit time

f= 0.00238 m/min or 3.968E-05 m/sec

Depth of water vs Elapsed Time (mins)



# Soakaway

IGSL

Contract: Capdoo, Clane  
 Test No. IT08  
 Client Ardstone/DBFL  
 Date: 22/06/2017

Contract No. 20159

**Summary of ground conditions**

from	to	Description	Ground water
0.00	0.50	TOPSOIL	
0.50	1.90	Brown gravelly SILT. Gravel fine to coarse subangular.	
1.90	2.40	Black gravelly coarse SAND.	

Notes: Location: IT08,687748.117,728233.974,70.390,,

**Field Data**

Depth to Water (m)	Elapsed Time (min)
1.33	0.00
1.33	1.00
1.33	2.00
1.34	3.00
1.34	4.00
1.34	5.00
1.36	10.00
1.37	15.00
1.37	20.00
1.37	30.00
1.39	40.00
1.40	60.00
1.42	90.00

**Field Test**

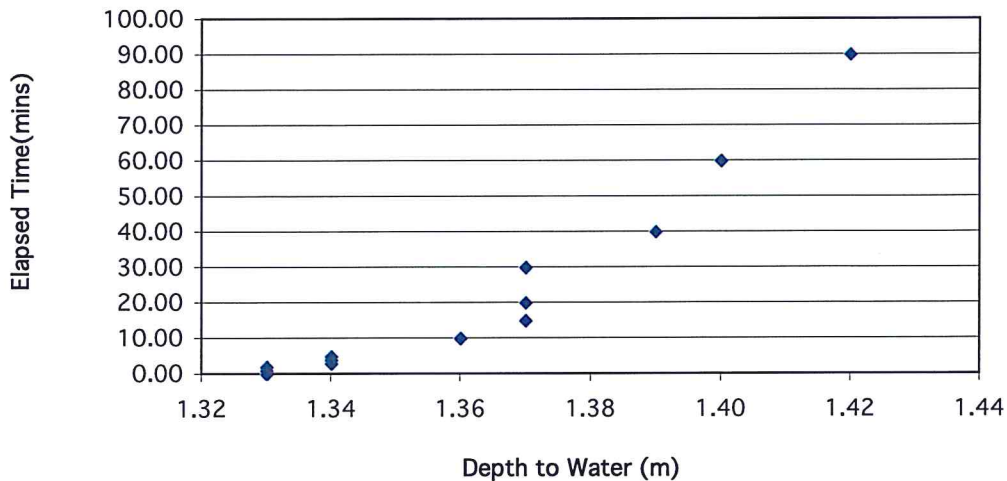
Depth of Pit (D)	2.40	m
Width of Pit (B)	0.40	m
Length of Pit (L)	2.00	m
Initial depth to Water =	1.33	m
Final depth to water =	1.42	m
Elapsed time (mins)=	90.00	
Top of permeable soil		m
Base of permeable soil		m

Base area=	0.8	m <sup>2</sup>
*Av. side area of permeable stratum over test period	4.92	m <sup>2</sup>
Total Exposed area =	5.72	m <sup>2</sup>

Infiltration rate (f) = Volume of water used/unit exposed area / unit time

f = 0.00014 m/min or 2.331E-06 m/sec

Depth of water vs Elapsed Time (mins)





## **Appendix VI Laboratory Data**

IGSL Ltd  
 Materials Laboratory  
 Unit J5, M7 Business Park  
 Newhall, Naas  
 Co. Kildare  
 045 846176

**Test Report**

**Determination of Moisture Content, Liquid & Plastic Limits**

Tested in accordance with BS1377:Part 2:1990, clauses 3.2\*, 4.3, 4.4 & 5.3



Report No. **R80600** Contract No. 20159 Contract Name: Capdoo, Clane  
 Customer DBFL Consulting Engineers, Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
 Samples Received: 04-07-17 Date Tested: 05-07-17

BH/TP	Sample No.	Depth (m)	Lab. Ref	Sample Type	Moisture Content %	Liquid Limit %	Plastic Limit %	Plasticity Index	% <425µm	Preparation	Liquid Limit Clause	Classification (BS5930)	Description
BH01	AA56212	7.0	A17/3239	B	2.6		NP	NP					Grey/brown slightly silty, slightly sandy, GRAVEL with many cobbles
BH02	AA56214	1.0	A17/3240	B	12	30	17	13	57	WS	4.4	CL	Dark brown slightly sandy, gravelly, CLAY
BH03	AA56217	1.0	A17/3241	B	12	28	18	10	58	WS	4.4	CL	Brown sandy gravelly CLAY with root hairs
TP09	AA78622	0.5	A17/3245	B	14	24	NP	NP	40	WS	4.4		Dark brown very sandy very gravelly SILT
TP11	AA78660	0.8	A17/3246	B	8.9	20	NP	NP	51	WS	4.4		Dark brown sandy, gravelly, SILT
TP22	AA67763	1.2	A17/3250	B	18	28	18	10	72	WS	4.4	CL	Brown sandy gravelly CLAY

Notes: Preparation: WS - Wet sieved  
 AR - As received  
 NP - Non plastic  
 Liquid Limit 4.3 Cone Penetrometer definitive method  
 Clause: 4.4 Cone Penetrometer one point method

Sample Type: B - Bulk Disturbed  
 U - Undisturbed

Remarks:  
 NOTE: \*Clause 3.2 of BS1377 is a "withdrawn" standard due to publication of ISO17892-1:2014  
 Opinions and interpretations are outside the scope of accreditation.  
 The results relate to the specimens tested. Any remaining material will be retained for one month.

Persons authorized to approve reports  
 H Byrne (Laboratory Manager)

Approved by: *H Byrne* Date: 24-07-17 Page: 1 of 1

# TEST REPORT

## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)

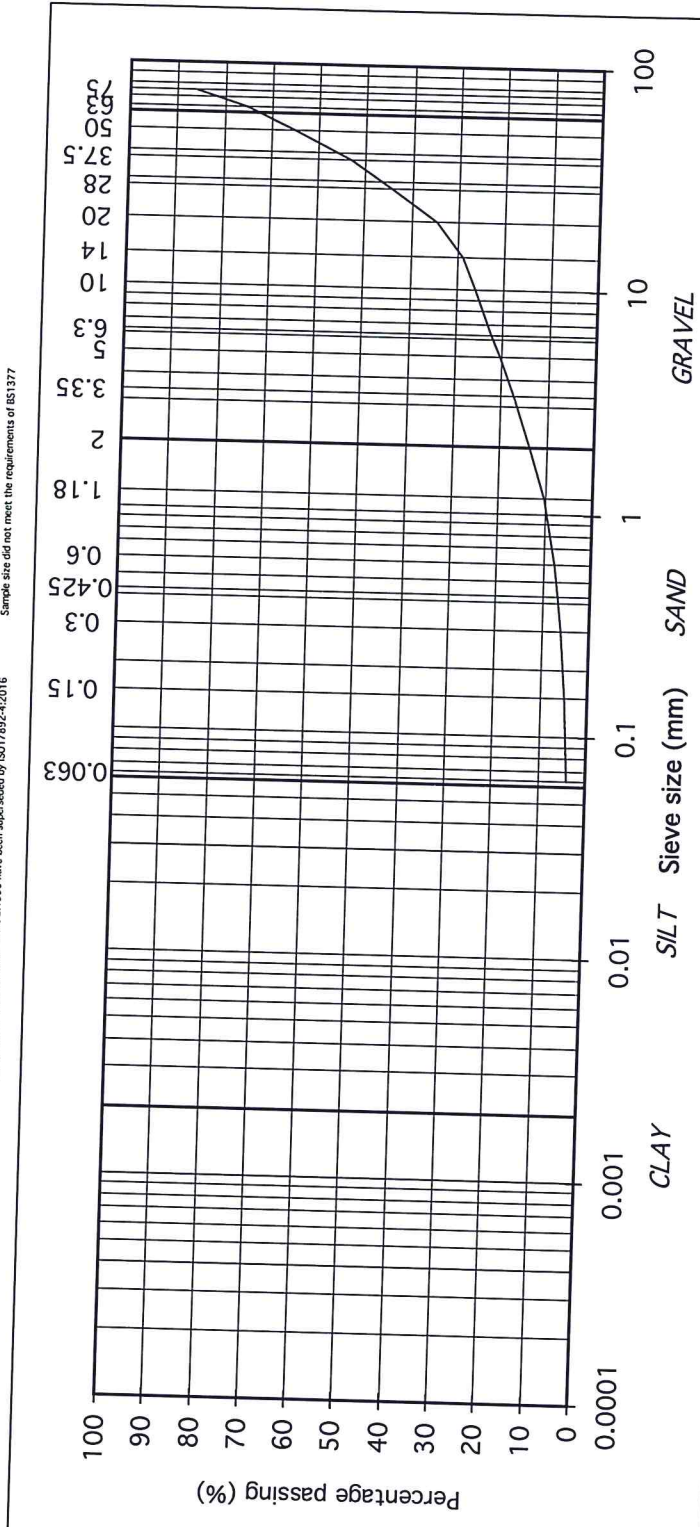


Contract No: 20159 Report No. R80628  
 Contract: Capdoo, Clane  
 BH/TP: BH01  
 Sample No. AA56207 Lab. Sample No. A17/3237  
 Sample Type: B  
 Depth (m) 2.00 Customer: DBFL Consulting Engineers, Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
 Date Received 04-07-17 Date Testing started 05-07-17  
 Description: Grey/brown slightly clayey/silty, sandy, GRAVEL with many cobbles

### Remarks

Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by ISO17892-4:2016  
 Sample size did not meet the requirements of BS1377

particle size	% passing
75	86
63	75
50	65
37.5	53
28	44
20	35
14	29
10	26
6.3	22
5	20
3.35	17
2	13
1.18	10
0.6	8
0.425	7
0.3	6
0.15	5
0.063	4



IGSL Ltd Materials Laboratory

Approved by: *H Byrne* Date: 11-07-17 Page no: 1 of 1

# TEST REPORT

## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990 , clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)

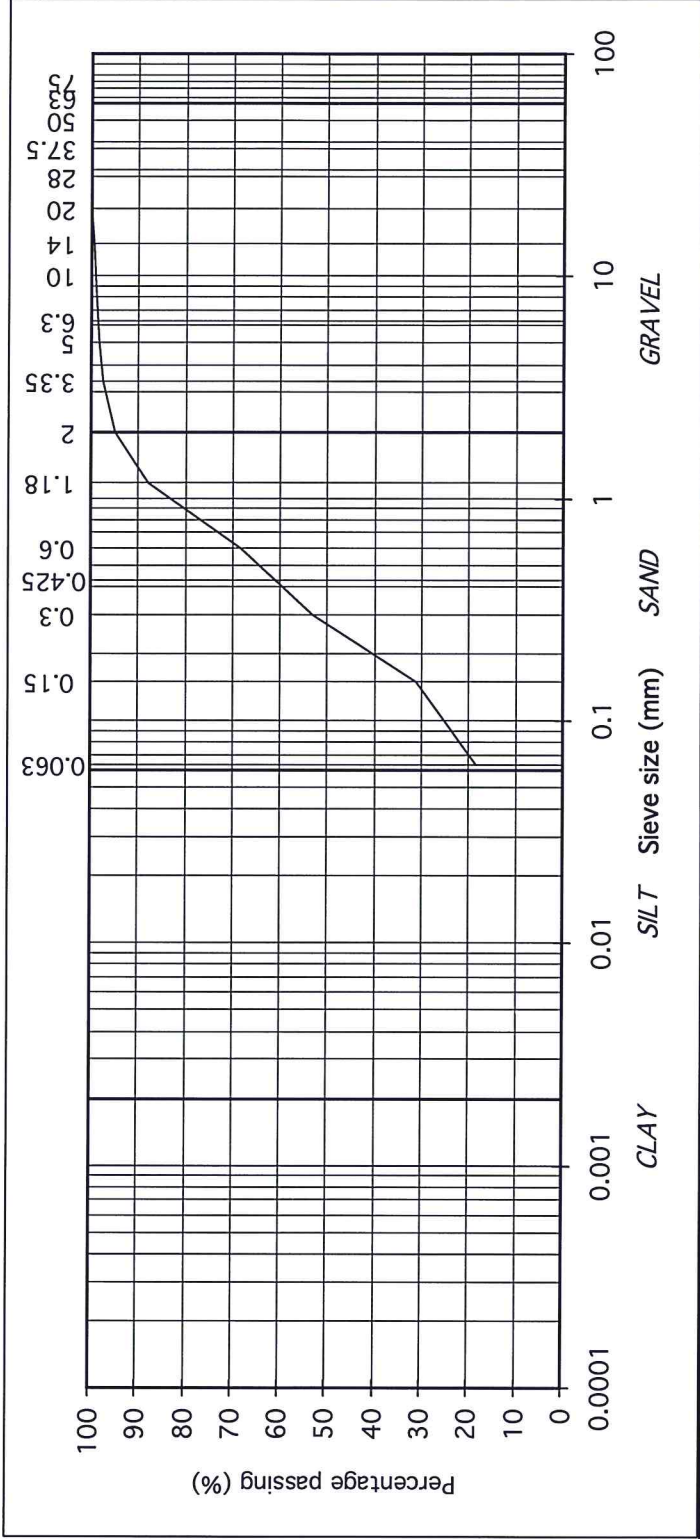


Contract No: 20159 Report No. R80664  
 Contract: Capdoo , Clane  
 BH/TP: BH01  
 Sample No. AA56210 Lab. Sample No. A17/3238  
 Sample Type: B  
 Depth (m) 5.00 Customer: DBFL Consulting Engineers,Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
 Date Received 04-07-17 Date Testing started 05-07-17  
 Description: Dark brown clayey/silty, gravelly, SAND

**Remarks**

Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by ISO7692-4:2016

particle size	% passing	
75	100	COBBLES
63	100	
50	100	
37.5	100	
28	100	
20	100	
14	99	GRAVEL
10	99	
6.3	99	
5	98	
3.35	97	
2	95	
1.18	88	
0.6	68	
0.425	61	SAND
0.3	53	
0.15	31	
0.063	18	SILT/CLAY



**IGSL Ltd Materials Laboratory**

Approved by: *H Byrne* Date: 24-07-17 Page no: 1 of 1

Persons authorised to approve report: J Barrett (Quality Manager) H Byrne (Laboratory Manager)

# TEST REPORT

## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)

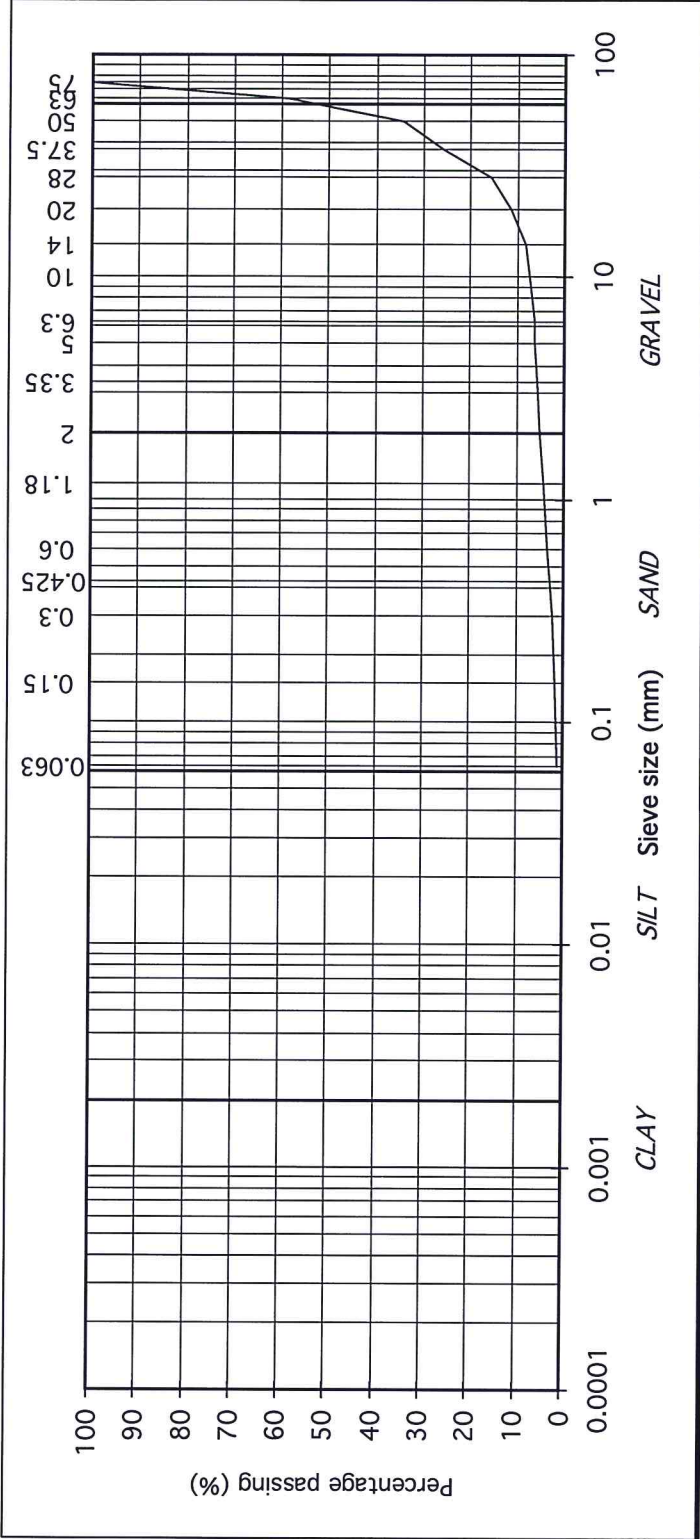


Contract No: 20159 Report No. R80838  
 Contract: Capdoo, Clane  
 BH/TP: BH01  
 Sample No. AA56212 Lab. Sample No. A17/3239  
 Sample Type: B  
 Depth (m) 7.00 Customer: DBFL Consulting Engineers, Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
 Date Received 04-07-17 Date Testing started 05-07-17  
 Description: Grey/brown slightly silty, slightly sandy, GRAVEL with many cobbles

### Remarks

Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by BS017692-4:2016  
 Sample size did not meet the requirements of BS1377

particle size	% passing	
75	100	COBBLES
63	58	
50	34	
37.5	26	
28	16	
20	11	
14	8	
10	7	GRAVEL
6.3	6	
5	6	
3.35	6	
2	5	
1.18	4	
0.6	3	
0.425	3	SAND
0.3	2	
0.15	2	
0.063	1	SILT/CLAY



<b>IGSL Ltd Materials Laboratory</b>	
Approved by: <i>H Byrne</i>	Date: 24-07-17
Page no: 1 of 1	

Persons authorised to approve report: J Barrett (Quality Manager) H Byrne (Laboratory Manager)

# TEST REPORT

## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)

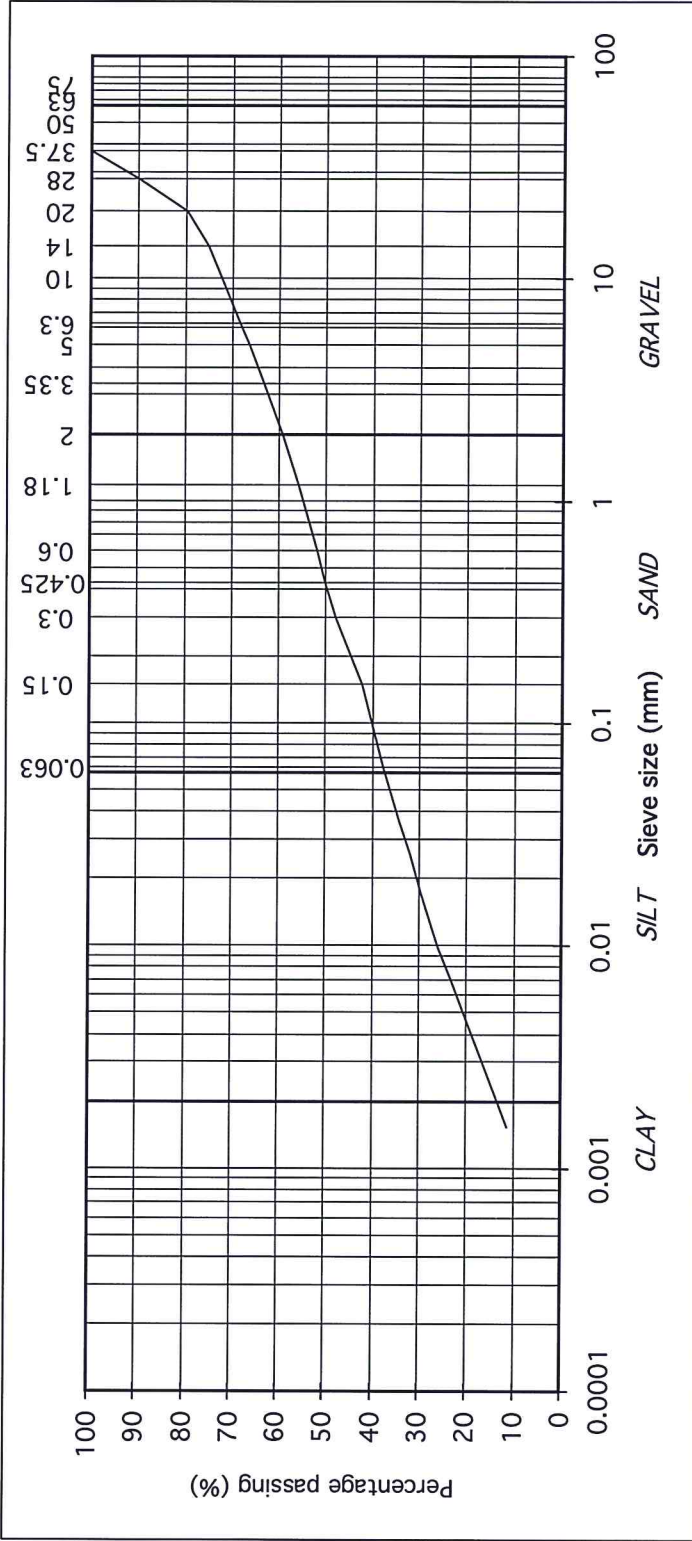


Contract No: 20159 Report No. R80727  
 Contract: Capdoo, Clane  
 BH/TP: BH2  
 Sample No. AA56214 Lab. Sample No. A17/3240  
 Sample Type: B  
 Depth (m) 1.00 Customer: DBFL Consulting Engineers, Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
 Date Received 04-07-17 Date Testing started 07-07-17  
 Description: Dark brown slightly sandy, gravelly, CLAY

### Remarks

Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by BS017892-4:2016

particle size	% passing
75	100
63	100
50	100
37.5	100
28	90
20	80
14	75
10	72
6.3	68
5	66
3.35	63
2	59
1.18	56
0.6	52
0.425	50
0.3	48
0.15	42
0.063	38
0.037	34
0.026	32
0.017	30
0.010	26
0.007	23
0.005	21
0.002	11



IGSL Ltd Materials Laboratory

Approved by: *H Byrne*

Date: 24-07-17

Page no: 1 of 1

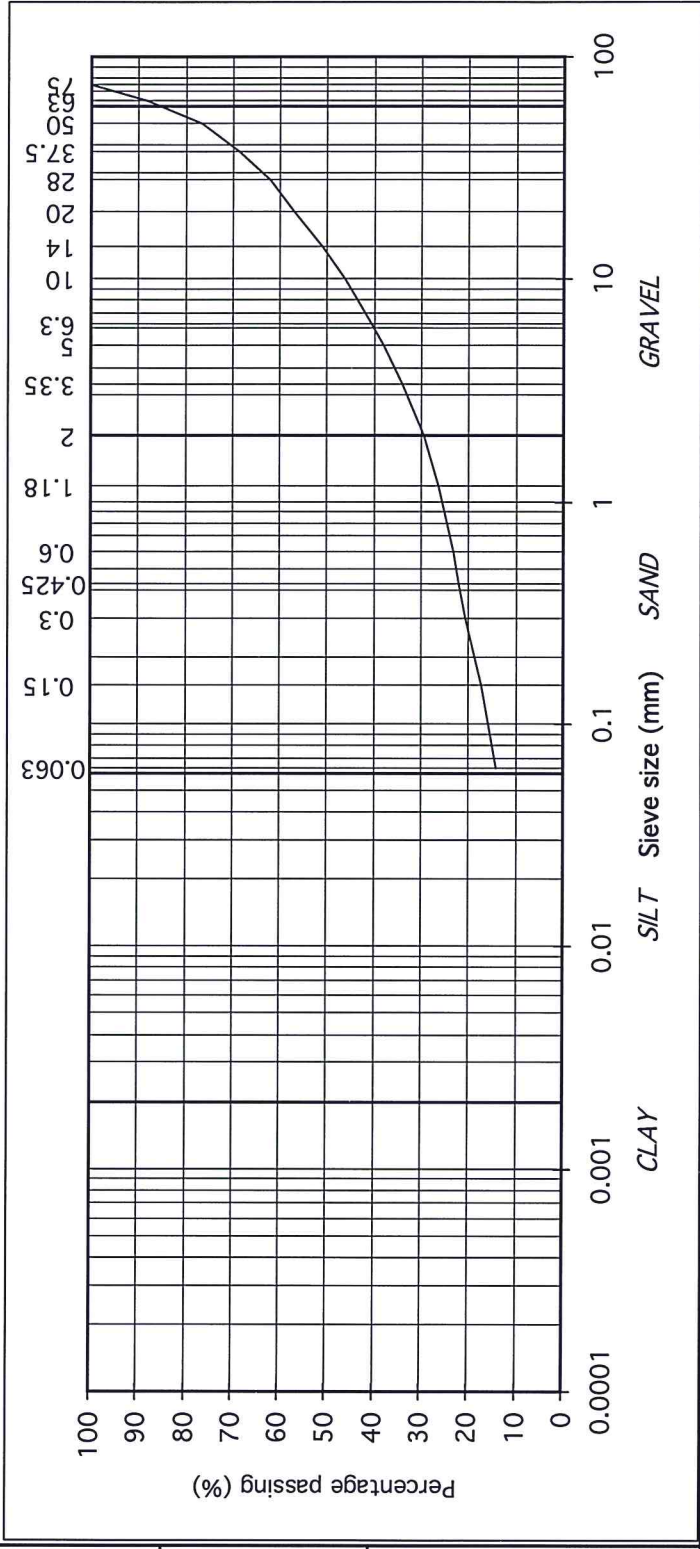
# TEST REPORT

## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990 , clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)



Contract No:	20159	Report No.	R80630
Contract:	Capdoo , Clane		
BH/TP :	TP07		
Sample No.	AA78667	Lab. Sample No.	A17/3244
Sample Type:	B		
Depth (m)	0.50	Customer:	DBFL Consulting Engineers,Ormond House, Upper Ormond Quay, Dublin 7, Ireland
Date Received	04-07-17	Date Testing started	05-07-17
Description:	Brown clayey/silty, sandy, GRAVEL with some cobbles		
Remarks	<p>Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by ISO17892-4:2016</p> <p>Sample size did not meet the requirements of BS1377</p>		
particle size	% passing		
75	100	COBBLES	
63	88		
50	77		
37.5	69		
28	62		
20	57		
14	51	GRAVEL	
10	46		
6.3	40		
5	38		
3.35	34		
2	29		
1.18	26		
0.6	23	SAND	
0.425	22		
0.3	21		
0.15	17		
0.063	14	SILT/CLAY	



# TEST REPORT

## Determination of Particle Size Distribution

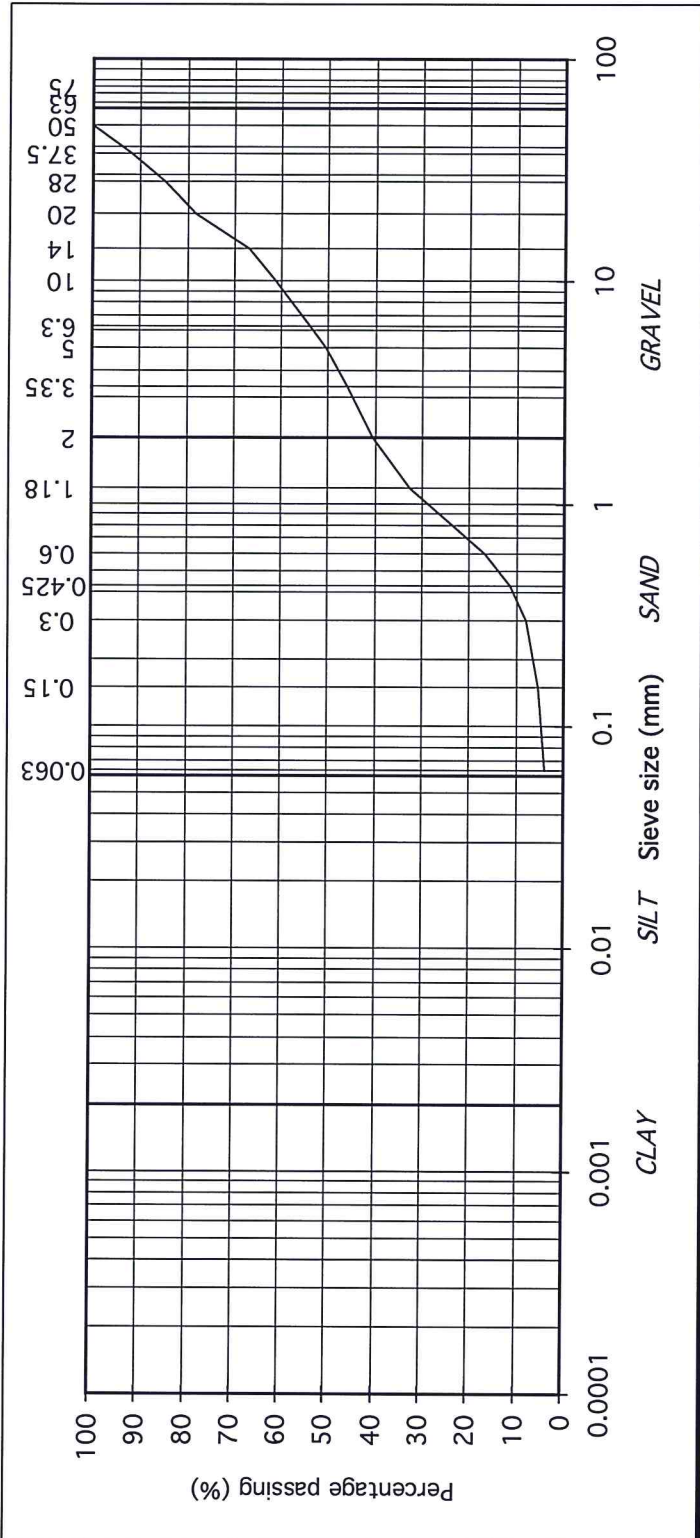
Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)



Contract No: 20159 Report No. R80839  
 Contract: Capdoo, Clane  
 BH/TP: TP05  
 Sample No. AA67770 Lab. Sample No. A17/3243  
 Sample Type: B  
 Depth (m) 1.60 Customer: DBFL Consulting Engineers, Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
 Date Received 04-07-17 Date Testing started 07-07-17  
 Description: Dark brown slightly clayey/silty, very sandy, GRAVEL

Remarks: Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by BS07892-4:2016

particle size	% passing
75	100
63	100
50	100
37.5	92
28	85
20	78
14	67
10	61
6.3	54
5	51
3.35	46
2	41
1.18	33
0.6	17
0.425	11
0.3	8
0.15	5
0.063	4





# TEST REPORT

## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)

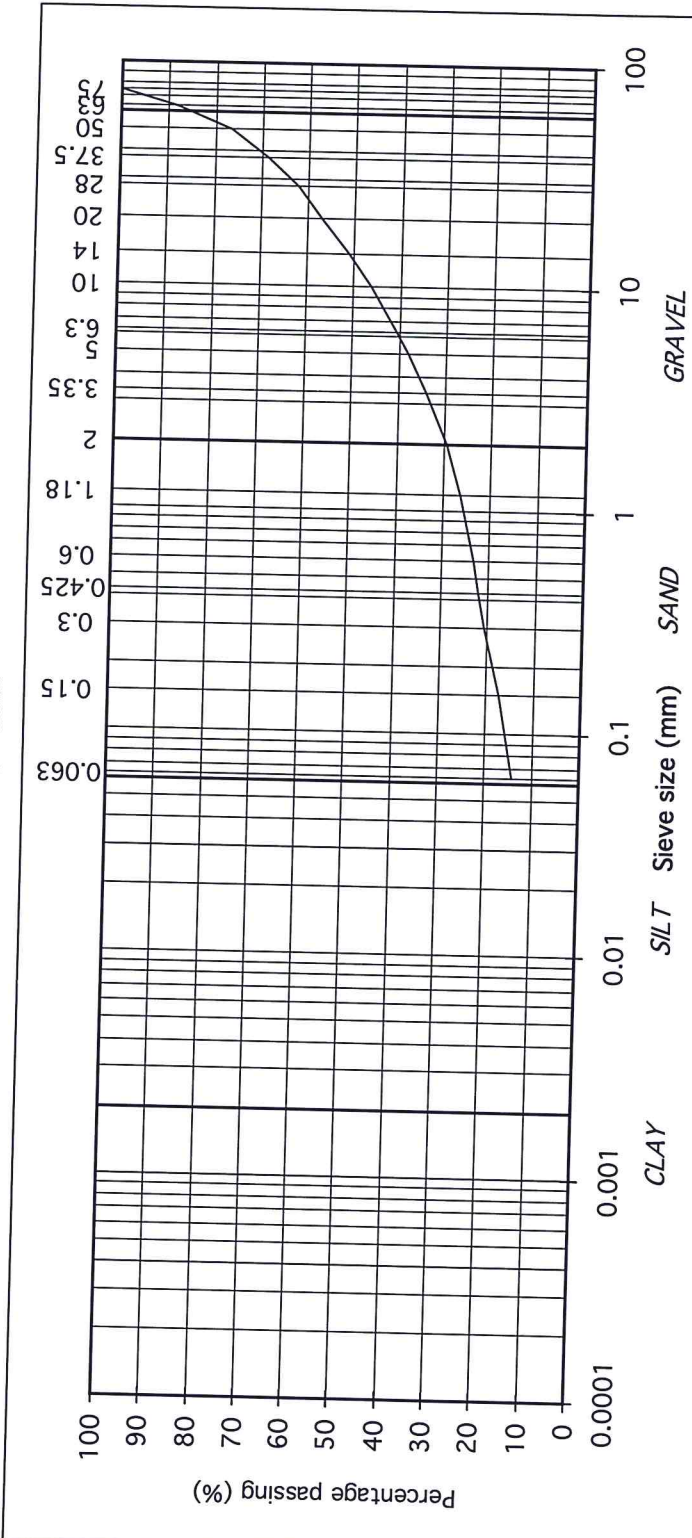


Contract No: 20159 Report No. R80630  
 Contract: Capdoo, Clane  
 BH/TP: TP07  
 Sample No. AA78667 Lab. Sample No. A17/3244  
 Sample Type: B  
 Depth (m) 0.50 Customer: DBFL Consulting Engineers, Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
 Date Received 04-07-17 Date Testing started 05-07-17  
 Description: Brown clayey/silty, sandy, GRAVEL with some cobbles

### Remarks

Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by ISO17892-4:2016

particle size	% passing
75	100
63	88
50	77
37.5	69
28	62
20	57
14	51
10	46
6.3	40
5	38
3.35	34
2	29
1.18	26
0.6	23
0.425	22
0.3	21
0.15	17
0.063	14



IGSL Ltd Materials Laboratory

Approved by: *H Byrne* Date: 24-07-17 Page no: 1 of 1  
 Persons authorised to approve report: J Barrett (Quality Manager) H Byrne (Laboratory Manager)

# TEST REPORT

## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)



	Contract No: 20159	Report No. R80631	
	Contract: Capdoo, Clane		
	BH/TP: TP11		
	Sample No. AA78666	Lab. Sample No. A17/3246	
	Sample Type: B		
	Depth (m) 0.80	Customer: DBFL Consulting Engineers, Ormond House, Upper Ormond Quay, Dublin 7, Ireland	
	Date Received 04-07-17	Date Testing started 05-07-17	
	Description: Dark brown sandy, gravelly, SILT/CLAY		
Remarks			
<small>Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by ISO17892-4:2016 Sample size did not meet the requirements of BS1377</small>			

particle size	% passing	
75	100	COBBLES
63	100	
50	100	
37.5	84	
28	81	
20	77	
14	75	GRAVEL
10	72	
6.3	71	
5	70	
3.35	67	
2	63	
1.18	57	
0.6	52	
0.425	49	SAND
0.3	44	
0.15	35	
0.063	27	
0.037	24	
0.026	22	
0.017	20	
0.010	17	SILT/CLAY
0.007	15	
0.005	13	
0.002	7	

IGSL Ltd Materials Laboratory

Approved by: *H Byrne*

Date: 24-07-17

Page no: 1 of 1

Persons authorised to approve report: J Barrett (Quality Manager) H Byrne (Laboratory Manager)

# TEST REPORT

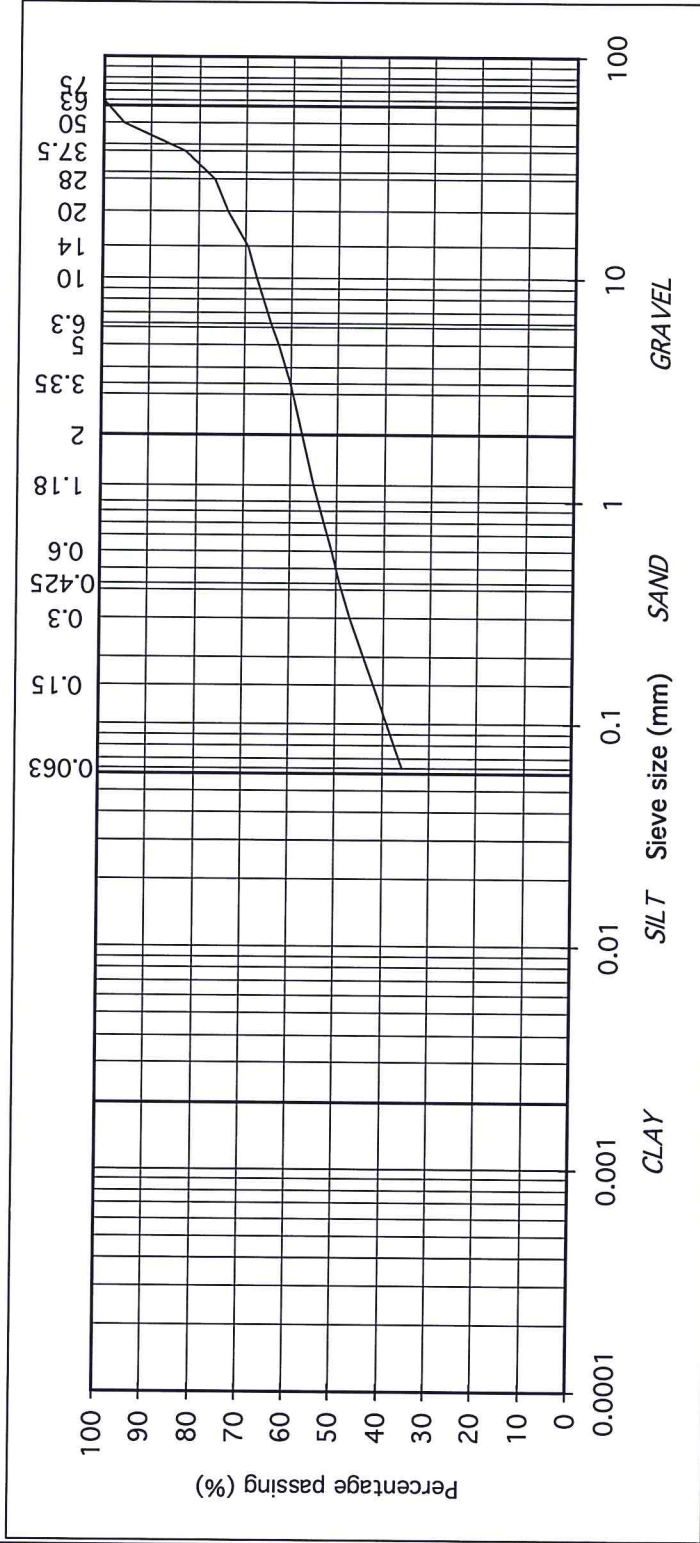
## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)



particle size	% passing	Contract No: 20159	Report No. R80665
75	100	Contract: Capdoo, Clane	
63	100	BH/TP: TP14	
50	96	Sample No. AA78687	Lab. Sample No. A17/3247
37.5	83	Sample Type: B	
28	77	Depth (m) 1.20	Customer: DBFL Consulting Engineers, Ormond House, Upper Ormond Quay, Dublin 7, Ireland
20	74	Date Received 04-07-17	Date Testing started 05-07-17
14	69	Description: Brown slightly sandy, gravelly, SILT/CLAY	
10	67	Remarks	
6.3	64		
5	63		
3.35	60		
2	58		
1.18	55		
0.6	51		
0.425	49		
0.3	47		
0.15	42		
0.063	36		

Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by ISO17892-4:2016



<b>IGSL Ltd Materials Laboratory</b>	
Approved by: <i>H. Byrne</i>	Date: 24-07-17
Page no: 1 of 1	

# TEST REPORT

## Determination of Particle Size Distribution

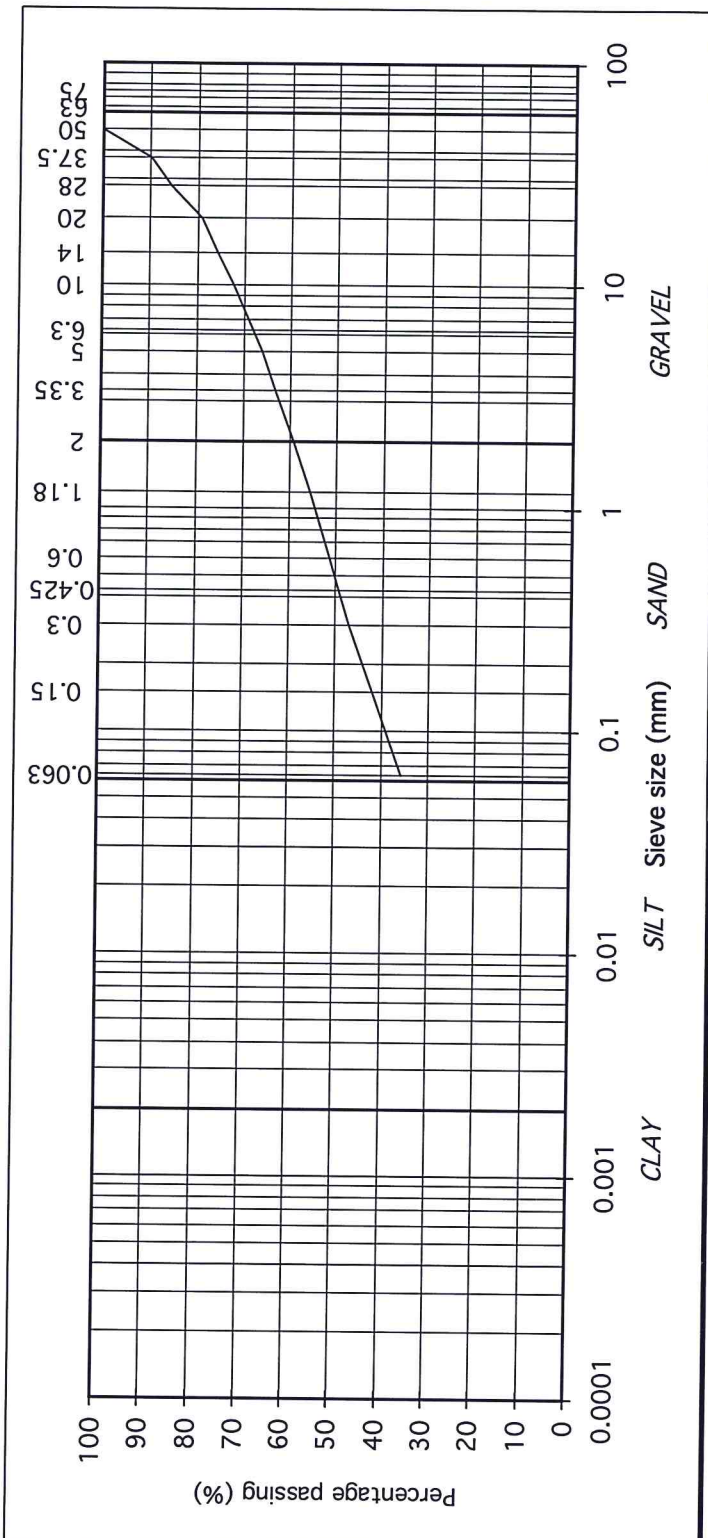
Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)



**Contract No:** 20159    **Report No.:** R80666  
**Contract:** Capdoo, Clane  
**BH/TP:** TP18  
**Sample No.:** AA78671    **Lab. Sample No.:** A17/3248  
**Sample Type:** B  
**Depth (m):** 1.10    **Customer:** DBFL Consulting Engineers, Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
**Date Received:** 04-07-17    **Date Testing started:** 05-07-17  
**Description:** Mottled brown slightly sandy, gravelly, SILT/CLAY

Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by ISO17892-4:2016

particle size	% passing	
75	100	COBBLES
63	100	
50	100	
37.5	90	GRAVEL
28	85	
20	79	
14	76	
10	72	
6.3	68	
5	66	
3.35	63	SAND
2	59	
1.18	56	
0.6	51	
0.425	49	SILT/CLAY
0.3	47	
0.15	42	
0.063	36	



**Approved by:** *H Byrne*    **Date:** 24-07-17    **Page no:** 1 of 1  
**IGSL Ltd Materials Laboratory**  
 Persons authorised to approve report: J Bairrett (Quality Manager) H Byrne (Laboratory Manager)

# TEST REPORT

## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)

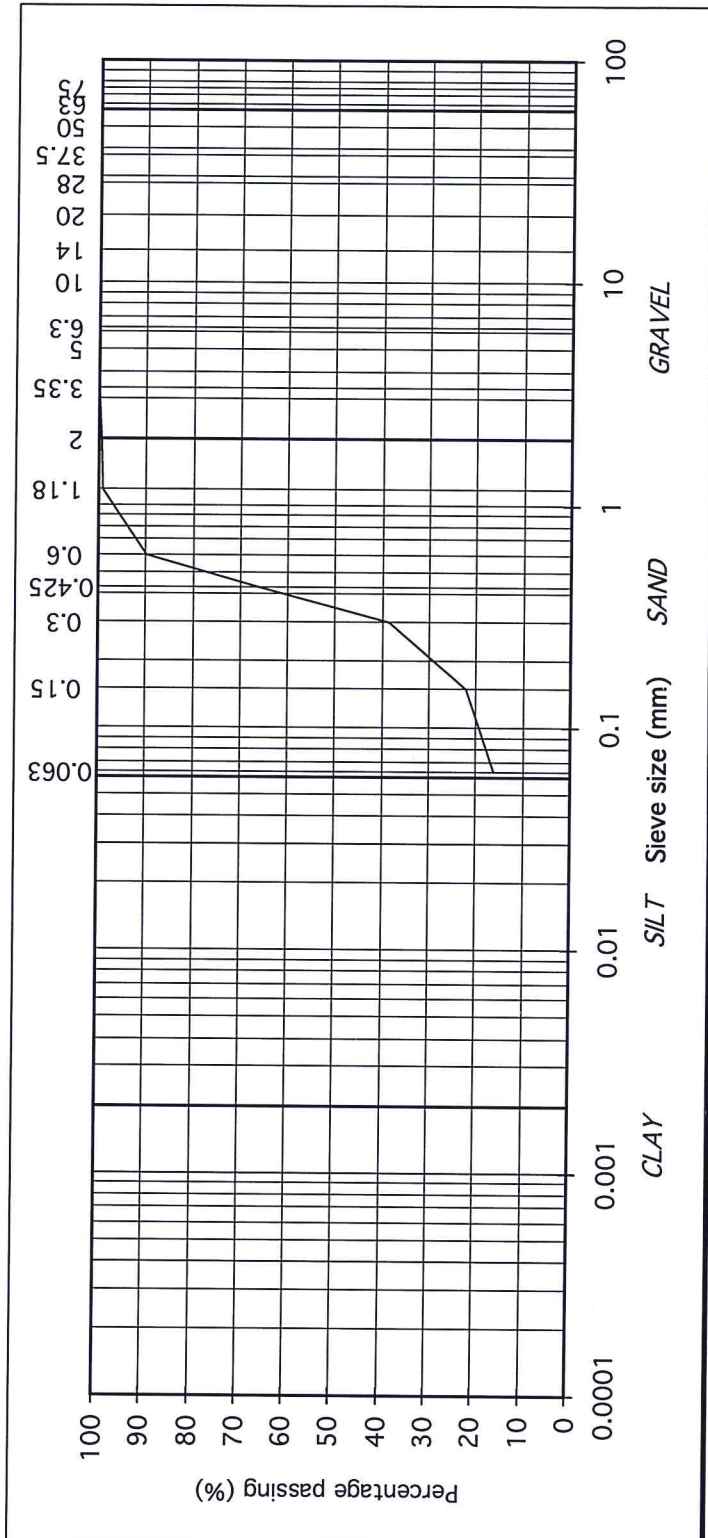


Contract No: 20159 Report No. R80667  
 Contract: Capdoo, Clane  
 BH/TP: TP19  
 Sample No. AA78765 Lab. Sample No. A17/3249  
 Sample Type: B  
 Depth (m) 0.80 Customer: DBFL Consulting Engineers, Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
 Date Received 04-07-17 Date Testing started 05-07-17  
 Description: Dark brown clayey/silty, SAND

Remarks

Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by BS07892-4:2016

particle size	% passing
75	100
63	100
50	100
37.5	100
28	100
20	100
14	100
10	100
6.3	100
5	100
3.35	100
2	100
1.18	99
0.6	90
0.425	66
0.3	39
0.15	22
0.063	16



# TEST REPORT

## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990 , clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)

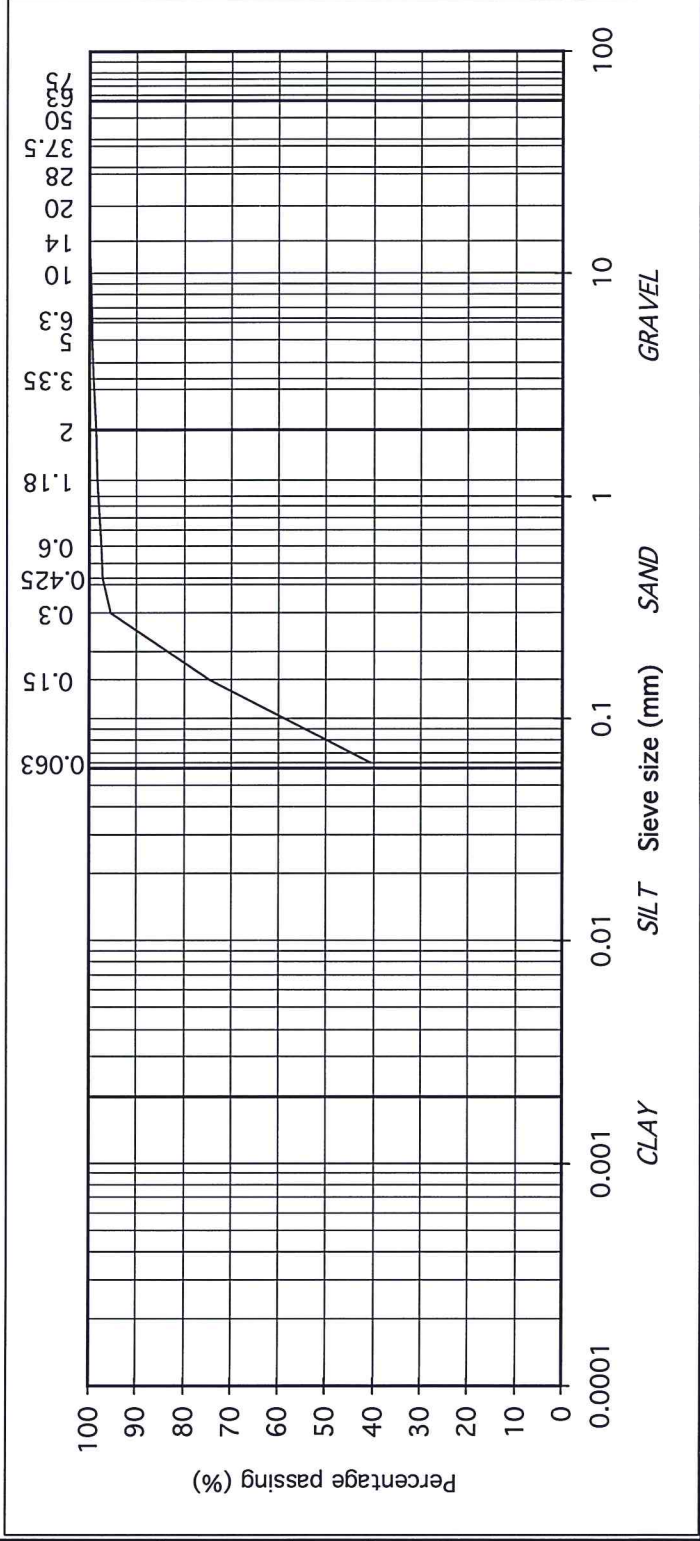


Contract No: 20159 Report No. R80632  
 Contract: Capdoo , Clane  
 BH/TP : TP23  
 Sample No. AA67755 Lab. Sample No. A17/3251  
 Sample Type: B  
 Depth (m) 0.50 Customer: DBFL Consulting Engineers,Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
 Date Received 04-07-17 Date Testing started 05-07-17  
 Description: Brown sandy, slightly gravelly, SILT/CLAY

**Remarks**

Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by ISO 7892-4:2016

particle size	% passing
75	100
63	100
50	100
37.5	100
28	100
20	100
14	100
10	100
6.3	99
5	99
3.35	99
2	99
1.18	98
0.6	97
0.425	97
0.3	95
0.15	74
0.063	41



Approved by: *H Byrne*

Date: 24-07-17

Page no: 1 of 1

**IGSL Ltd Materials Laboratory**

Persons authorised to approve report: J Barrett (Quality Manager) H Byrne (Laboratory Manager)

# TEST REPORT

## Determination of Particle Size Distribution

Tested in accordance with: BS1377:Part2:1990 , clause 9.2 & 9.5  
(note: Sedimentation stage not accredited)

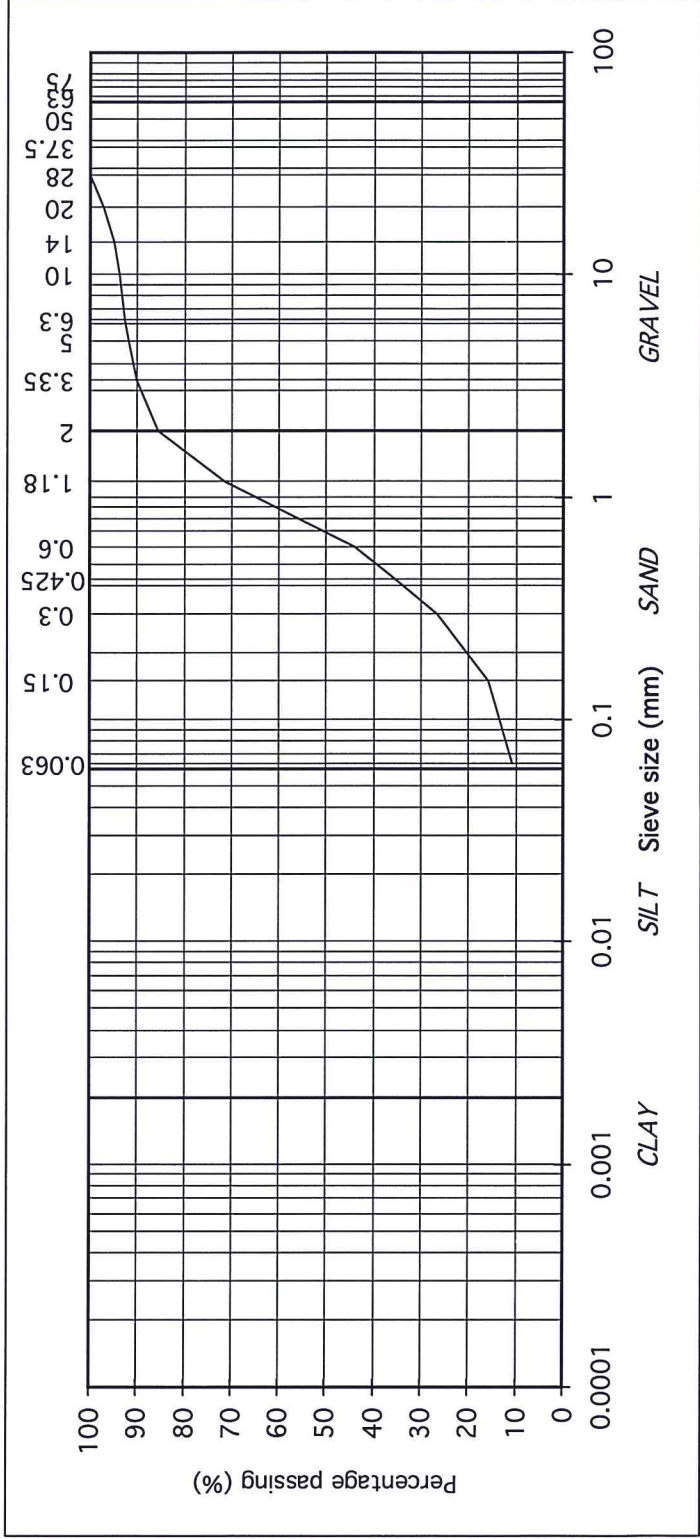


Contract No: 20159 Report No. R80633  
 Contract: Capdoo , Clane  
 BH/TP : TP25  
 Sample No. AA67751 Lab. Sample No. A17/3252  
 Sample Type: B  
 Depth (m) 1.80 Customer: DBFL Consulting Engineers,Ormond House, Upper Ormond Quay, Dublin 7, Ireland  
 Date Received 04-07-17 Date Testing started 05-07-17  
 Description: Dark brown clayey/silty, gravelly, SAND

**Remarks**

Note: Clause 9.2 and Clause 9.5 of BS1377:Part 2:1990 have been superseded by ISO7692-4:2016

particle size	% passing	
75	100	COBBLES
63	100	
50	100	
37.5	100	
28	100	
20	97	
14	95	
10	94	GRAVEL
6.3	93	
5	92	
3.35	90	
2	86	
1.18	71	
0.6	44	
0.425	35	SAND
0.3	27	
0.15	16	
0.063	11	SILT/CLAY



Approved by: *H Byrne*

Date: 24-07-17  
Page no: 1 of 1

**IGSL Ltd Materials Laboratory**

Persons authorised to approve report: J Barrett (Quality Manager) H Byrne (Laboratory Manager)



# Final Report

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**Report No.:** 17-17340-1

**Initial Date of Issue:** 13-Jul-2017

**Client:** IGSL

**Client Address:** M7 Business Park  
Naas  
County Kildare  
Ireland

**Contact(s):** Darren Keogh

**Project:** 20159 - Capdoo Clane (DBFL)

**Quotation No.:** Q17-08989

**Date Received:** 05-Jul-2017

**Order No.:**

**Date Instructed:** 06-Jul-2017

**No. of Samples:** 5

**Turnaround (Wkdays):** 5

**Results Due:** 12-Jul-2017

**Date Approved:** 13-Jul-2017

**Approved By:**

**Details:** Martin Dyer, Laboratory Manager

---



<b>Client:</b> IGSL	<b>Chemtest Job No.:</b> 17-17340	17-17340		
<b>Quotation No.:</b> Q17-08989	<b>Chemtest Sample ID.:</b> 480025	480363		
<b>Order No.:</b>	<b>Client Sample Ref.:</b> 78693	78679		
	<b>Client Sample ID.:</b> TP4	TP15		
	<b>Sample Type:</b> SOIL	SOIL		
	<b>Top Depth (m):</b> 0.50	0.60		
	<b>Bottom Depth (m):</b> 0.50	0.60		
<b>Determinand</b>	<b>Accred.</b>	<b>SOP</b>	<b>Units</b>	<b>LOD</b>
Ammonium	U	1220	mg/l	0.010
Ammonium	N	1220	mg/kg	0.10
Boron (Dissolved)	U	1450	µg/l	20
Boron (Dissolved)	N	1450	mg/kg	0.20
				< 20
				< 0.20

Client: IGSL		Chemtest Job No.:		17-17340		17-17340		17-17340		17-17340	
Quotation No.: Q17-08989		Chemtest Sample ID.:		480022		480023		480024		480025	
Order No.:		Client Sample Ref.:		56214		67763		78662		78693	
		Client Sample ID.:		BH2		TP9		TP22		TP4	
		Sample Type:		SOIL		SOIL		SOIL		SOIL	
		Top Depth (m):		1.00		0.50		1.20		0.50	
		Bottom Depth (m):		1.00		0.50		1.20		0.50	
		Asbestos Lab:						COVENTRY		COVENTRY	
Determinand	Accred.	SOP	Units	LOD							
ACM Type	U	2192		N/A							
Asbestos Identification	U	2192	%	0.001					No Asbestos Detected		No Asbestos Detected
Moisture	N	2030	%	0.020	7.8	11	19	18			14
pH	M	2010		N/A	[A] 8.1	[A] 8.5	[A] 8.5				
Boron (Hot Water Soluble)	M	2120	mg/kg	0.40				< 0.40			0.90
Sulphate (2:1 Water Soluble) as SO4	M	2120	g/l	0.010	< 0.010	0.017	< 0.010				
Sulphur (Elemental)	M	2180	mg/kg	1.0							[A] < 1.0
Cyanide (Total)	M	2300	mg/kg	0.50							[A] < 0.50
Sulphide (Easily Liberatable)	U	2325	mg/kg	0.50							[A] 3.8
Sulphate (Acid Soluble)	M	2430	%	0.010							[A] 0.036
Arsenic	M	2450	mg/kg	1.0				22			[A] 0.026
Barium	M	2450	mg/kg	10				79			63
Cadmium	M	2450	mg/kg	0.10				3.9			1.7
Chromium	M	2450	mg/kg	1.0				32			19
Copper	M	2450	mg/kg	0.50				69			22
Mercury	M	2450	mg/kg	0.10				0.28			0.16
Molybdenum	M	2450	mg/kg	2.0				3.8			3.3
Nickel	M	2450	mg/kg	0.50				91			32
Lead	M	2450	mg/kg	0.50				51			27
Antimony	N	2450	mg/kg	2.0				3.3			< 2.0
Selenium	M	2450	mg/kg	0.20				1.5			0.91
Zinc	M	2450	mg/kg	0.50				300			110
Chromium (Trivalent)	N	2490	mg/kg	5.0				32			19
Chromium (Hexavalent)	N	2490	mg/kg	0.50				< 0.50			< 0.50
Total Organic Carbon	M	2625	%	0.20				[A] 0.50			[A] 0.49
Mineral Oil	N	2670	mg/kg	10				< 10			< 10
Aliphatic TPH >C5-C6	N	2680	mg/kg	1.0				[A] < 1.0			[A] < 1.0
Aliphatic TPH >C6-C8	N	2680	mg/kg	1.0				[A] < 1.0			[A] < 1.0
Aliphatic TPH >C8-C10	M	2680	mg/kg	1.0				[A] < 1.0			[A] < 1.0
Aliphatic TPH >C10-C12	M	2680	mg/kg	1.0				[A] < 1.0			[A] < 1.0
Aliphatic TPH >C12-C16	M	2680	mg/kg	1.0				[A] < 1.0			[A] < 1.0
Aliphatic TPH >C16-C21	M	2680	mg/kg	1.0				[A] < 1.0			[A] < 1.0
Aliphatic TPH >C21-C35	M	2680	mg/kg	1.0				[A] < 1.0			[A] < 1.0
Aliphatic TPH >C35-C44	N	2680	mg/kg	1.0				[A] < 1.0			[A] < 1.0
Total Aliphatic Hydrocarbons	N	2680	mg/kg	5.0				[A] < 5.0			[A] < 5.0
Aromatic TPH >C5-C7	N	2680	mg/kg	1.0				[A] < 1.0			[A] < 1.0
Aromatic TPH >C7-C8	N	2680	mg/kg	1.0				[A] < 1.0			[A] < 1.0

Client: IGSL	Chemtest Job No.:		17-17340	17-17340	17-17340	17-17340	17-17340	17-17340
	Quotation No.:	Chemtest Sample ID.:						
	Q17-08989	480022	480022	480022	480022	480022	480022	480022
Order No.:		Client Sample Ref.:	56214	78662	78662	78662	78662	78662
		Client Sample ID.:	BH2	TP9	TP22	TP4	TP15	TP15
		Sample Type:	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL
		Top Depth (m):	1.00	0.50	1.20	0.50	0.50	0.60
		Bottom Depth (m):	1.00	0.50	1.20	0.50	0.50	0.60
		Asbestos Lab:				COVENTRY	COVENTRY	COVENTRY
Determinand	Accred.	SOP	Units	LOD				
Aromatic TPH >C8-C10	M	2680	mg/kg	1.0			[A] < 1.0	[A] < 1.0
Aromatic TPH >C10-C12	M	2680	mg/kg	1.0			[A] < 1.0	[A] < 1.0
Aromatic TPH >C12-C16	M	2680	mg/kg	1.0			[A] < 1.0	[A] < 1.0
Aromatic TPH >C16-C21	U	2680	mg/kg	1.0			[A] < 1.0	[A] < 1.0
Aromatic TPH >C21-C35	M	2680	mg/kg	1.0			[A] < 1.0	[A] < 1.0
Aromatic TPH >C35-C44	N	2680	mg/kg	1.0			[A] < 1.0	[A] < 1.0
Total Aromatic Hydrocarbons	N	2680	mg/kg	5.0			[A] < 5.0	[A] < 5.0
Total Petroleum Hydrocarbons	N	2680	mg/kg	10.0			[A] < 10	[A] < 10
Benzene	M	2760	µg/kg	1.0			[A] < 1.0	[A] < 1.0
Toluene	M	2760	µg/kg	1.0			[A] < 1.0	[A] < 1.0
Ethylbenzene	M	2760	µg/kg	1.0			[A] < 1.0	[A] < 1.0
m & p-Xylene	M	2760	µg/kg	1.0			[A] < 1.0	[A] < 1.0
o-Xylene	M	2760	µg/kg	1.0			[A] < 1.0	[A] < 1.0
Methyl Tert-Butyl Ether	M	2760	µg/kg	1.0			[A] < 1.0	[A] < 1.0
Naphthalene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Acenaphthylene	N	2800	mg/kg	0.10			< 0.10	< 0.10
Acenaphthene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Fluorene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Phenanthrene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Anthracene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Fluoranthene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Pyrene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Benzo[a]anthracene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Chrysene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Benzo[b]fluoranthene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Benzo[k]fluoranthene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Benzo[a]pyrene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Indeno(1,2,3-c,d)Pyrene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Dibenz(a,h)Anthracene	N	2800	mg/kg	0.10			< 0.10	< 0.10
Benzo[g,h,i]perylene	M	2800	mg/kg	0.10			< 0.10	< 0.10
Coronene	N	2800	mg/kg	0.10			< 0.10	< 0.10
Total Of 17 PAH's	N	2800	mg/kg	2.0			< 2.0	< 2.0
PCB 28	M	2815	mg/kg	0.010			[A] < 0.010	[A] < 0.010
PCB 52	M	2815	mg/kg	0.010			[A] < 0.010	[A] < 0.010
PCB 90+101	M	2815	mg/kg	0.010			[A] < 0.010	[A] < 0.010
PCB 118	M	2815	mg/kg	0.010			[A] < 0.010	[A] < 0.010
PCB 153	M	2815	mg/kg	0.010			[A] < 0.010	[A] < 0.010
PCB 138	M	2815	mg/kg	0.010			[A] < 0.010	[A] < 0.010



The right chemistry to deliver results

Project: 20159 - Capdoo Clane (DBFL)

## Results - Soil

	Chemtest Job No.:	17-17340	17-17340	17-17340	17-17340	17-17340	17-17340
Client: IGSL	Chemtest Sample ID.:	480022	480023	480024	480025	480363	480363
Quotation No.: Q17-08989	Client Sample Ref.:	56214	78662	67763	78693	78679	78679
Order No.:	Client Sample ID.:	BH2	TP9	TP22	TP4	TP15	TP15
	Sample Type:	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL
	Top Depth (m):	1.00	0.50	1.20	0.50	0.60	0.60
	Bottom Depth (m):	1.00	0.50	1.20	0.50	0.60	0.60
	Asbestos Lab:				COVENTRY	COVENTRY	COVENTRY
<b>Determinand</b>	<b>Accred.</b>	<b>SOP</b>	<b>Units</b>	<b>LOD</b>			
PCB 180	M	2815	mg/kg	0.010	[A] < 0.010	[A] < 0.010	[A] < 0.010
Total PCBs (7 Congeners)	N	2815	mg/kg	0.10	[A] < 0.10	[A] < 0.10	[A] < 0.10
Total Phenols	M	2920	mg/kg	0.30	< 0.30	< 0.30	< 0.30

## Results - Single Stage WAC

**Project:** 20159 - Capdoo Clane (DBFL)

**Chemtest Job No:** 17-17340

**Chemtest Sample ID:** 480025

**Sample Ref:** 78693

**Sample ID:** TP4

**Top Depth(m):** 0.50

**Bottom Depth(m):** 0.50

**Sampling Date:**

Determind	SOP	Accred.	Units	Landfill Waste Acceptance Criteria Limits		
				Inert Waste Landfill	Stable, Non-reactive hazardous waste in non-hazardous Landfill	Hazardous Waste Landfill
Total Organic Carbon	2625	M	%	[A] 0.50	3	6
Loss On Ignition	2610	M	%	2.3	---	10
Total BTEX	2760	M	mg/kg	[A] < 0.010	---	---
Total PCBs (7 Congeners)	2815	M	mg/kg	< 0.10	---	---
TPH Total WAC (Mineral Oil)	2670	M	mg/kg	[A] < 10	---	---
Total (OF 17) PAH's	2800	N	mg/kg	< 2.0	---	---
pH	2010	M		8.1	---	---
Acid Neutralisation Capacity	2015	N	mol/kg	0.031	---	---
<b>Eluate Analysis</b>			<b>10:1 Eluate mg/l</b>	<b>10:1 Eluate mg/kg</b>	<b>Limit values for compliance leaching test using BS EN 12457-3 at L/S 10 l/kg</b>	<b>To evaluate</b>
Arsenic	1450	U	< 0.0010	< 0.050	0.5	25
Barium	1450	U	0.0038	< 0.50	20	300
Cadmium	1450	U	< 0.00010	< 0.010	0.04	1
Chromium	1450	U	< 0.0010	< 0.050	0.5	10
Copper	1450	U	0.0023	< 0.050	2	50
Mercury	1450	U	< 0.00050	< 0.0050	0.01	2
Molybdenum	1450	U	0.0031	< 0.050	0.5	10
Nickel	1450	U	< 0.0010	< 0.050	0.4	10
Lead	1450	U	< 0.0010	< 0.010	0.5	10
Antimony	1450	U	< 0.0010	< 0.010	0.06	0.7
Selenium	1450	U	< 0.0010	< 0.010	0.1	0.5
Zinc	1450	U	0.0022	< 0.50	4	50
Chloride	1220	U	< 1.0	< 10	800	15000
Fluoride	1220	U	0.38	3.8	10	150
Sulphate	1220	U	15	150	1000	20000
Total Dissolved Solids	1020	N	66	660	4000	60000
Phenol Index	1920	U	< 0.030	< 0.30	1	---
Dissolved Organic Carbon	1610	U	9.2	92	500	800

Solid Information	
Dry mass of test portion/kg	0.090
Moisture (%)	18

### Waste Acceptance Criteria

Landfill WAC analysis (specifically leaching test results) must not be used for hazardous waste classification purposes. This analysis is only applicable for hazardous waste landfill acceptance and does not give any indication as to whether a waste may be hazardous or non-hazardous.

## Results - Single Stage WAC

**Project:** 20159 - Capdoo Clane (DBFL)

**Chemtest Job No:** 17-17340  
**Chemtest Sample ID:** 480363  
**Sample Ref:** 78679  
**Sample ID:** TP15  
**Top Depth(m):** 0.60  
**Bottom Depth(m):** 0.60  
**Sampling Date:**

Determinand	SOP	Accred.	Units	Landfill Waste Acceptance Criteria Limits		
				Inert Waste Landfill	Stable, Non-reactive hazardous waste in non-hazardous Landfill	Hazardous Waste Landfill
Total Organic Carbon	2625	M	%		[A] 0.49	6
Loss On Ignition	2610	M	%		1.5	10
Total BTEX	2760	M	mg/kg		[A] < 0.10	--
Total PCBs (7 Congeners)	2815	M	mg/kg	1		--
TPH Total WAC (Mineral Oil)	2670	M	mg/kg	500	[A] < 10	--
Total (Of 17) PAH's	2800	N	mg/kg	100	< 2.0	--
pH	2010	M		--	8.1	--
Acid Neutralisation Capacity	2015	N	mol/kg	--	0.049	--
<b>Eluate Analysis</b>			<b>10:1 Eluate mg/l</b>	<b>Limit values for compliance leaching test using BS EN 12457-3 at L/S 10 l/kg</b>	<b>10:1 Eluate mg/kg</b>	<b>To evaluate</b>
Arsenic	1450	U	< 0.0010	0.5	< 0.050	2
Barium	1450	U	0.0031	20	< 0.50	100
Cadmium	1450	U	< 0.00010	0.04	< 0.010	1
Chromium	1450	U	0.0011	0.5	< 0.050	10
Copper	1450	U	0.0012	2	< 0.050	50
Mercury	1450	U	< 0.00050	0.01	< 0.0050	0.2
Molybdenum	1450	U	0.0068	0.5	0.068	10
Nickel	1450	U	< 0.0010	0.4	< 0.050	10
Lead	1450	U	< 0.0010	0.5	< 0.010	10
Antimony	1450	U	< 0.0010	0.06	< 0.010	0.7
Selenium	1450	U	< 0.0010	0.1	< 0.010	0.5
Zinc	1450	U	0.0020	4	< 0.50	50
Chloride	1220	U	1.7	800	17	15000
Fluoride	1220	U	0.20	10	2.0	150
Sulphate	1220	U	6.4	1000	64	20000
Total Dissolved Solids	1020	N	71	4000	710	60000
Phenol Index	1920	U	< 0.030	1	< 0.30	--
Dissolved Organic Carbon	1610	U	9.2	500	92	800

Solid Information	
Dry mass of test portion/kg	0.090
Moisture (%)	14

### Waste Acceptance Criteria

Landfill WAC analysis (specifically leaching test results) must not be used for hazardous waste classification purposes. This analysis is only applicable for hazardous waste landfill acceptance and does not give any indication as to whether a waste may be hazardous or non-hazardous.

## Deviations

In accordance with UKAS Policy on Deviating Samples TPS 63. Chemtest have a procedure to ensure 'upon receipt of each sample a competent laboratory shall assess whether the sample is suitable with regard to the requested test(s)'. This policy and the respective holding times applied, can be supplied upon request. The reason a sample is declared as deviating is detailed below. Where applicable the analysis remains UKAS/MCERTs accredited but the results may be compromised.

Sample ID:	Sample Ref:	Sample ID:	Sampled Date:	Deviation Code(s):	Containers Received:
480022	56214	BH2		A	Amber Glass 250ml
480023	78662	TP9		A	Amber Glass 250ml
480024	67763	TP22		A	Amber Glass 250ml
480025	78693	TP4		A	Amber Glass 250ml
480025	78693	TP4		A	Amber Glass 60ml
480025	78693	TP4		A	Plastic Tub 500g
480363	78679	TP15		A	Amber Glass 250ml
480363	78679	TP15		A	Amber Glass 60ml
480363	78679	TP15		A	Plastic Tub 500g

SOP	Title	Parameters included	Method summary
1020	Electrical Conductivity and Total Dissolved Solids (TDS) in Waters	Electrical Conductivity and Total Dissolved Solids (TDS) in Waters	Conductivity Meter
1220	Anions, Alkalinity & Ammonium in Waters	Fluoride; Chloride; Nitrite; Nitrate; Total; Oxidisable Nitrogen (TON); Sulfate; Phosphate; Alkalinity; Ammonium	Automated colorimetric analysis using 'Aquakem 600' Discrete Analyser.
1450	Metals in Waters by ICP-MS	Metals, including: Antimony; Arsenic; Barium; Beryllium; Boron; Cadmium; Chromium; Cobalt; Copper; Lead; Manganese; Mercury; Molybdenum; Nickel; Selenium; Tin; Vanadium; Zinc	Filtration of samples followed by direct determination by inductively coupled plasma mass spectrometry (ICP-MS).
1610	Total/Dissolved Organic Carbon in Waters	Organic Carbon	TOC Analyser using Catalytic Oxidation
1920	Phenols in Waters by HPLC	Phenolic compounds including: Phenol, Cresols, Xylenols, Trimethylphenols Note: Chlorophenols are excluded.	Determination by High Performance Liquid Chromatography (HPLC) using electrochemical detection.
2010	pH Value of Soils	pH	pH Meter
2015	Acid Neutralisation Capacity	Acid Reserve	Titration
2030	Moisture and Stone Content of Soils (Requirement of MCERTS)	Moisture content	Determination of moisture content of soil as a percentage of its as received mass obtained at <37°C.
2120	Water Soluble Boron, Sulphate, Magnesium & Chromium	Boron; Sulphate; Magnesium; Chromium	Aqueous extraction / ICP-OES
2180	Sulphur (Elemental) in Soils by HPLC	Sulphur	Dichloromethane extraction / HPLC with UV detection
2192	Asbestos	Asbestos	Polarised light microscopy / Gravimetry
2300	Cyanides & Thiocyanate in Soils	Free (or easy liberatable) Cyanide; total Cyanide; complex Cyanide; Thiocyanate	Alkaline extraction followed by colorimetric determination using Automated Flow Injection Analyser.
2325	Sulphide in Soils	Sulphide	Steam distillation with sulphuric acid / analysis by 'Aquakem 600' Discrete Analyser, using N,N-dimethyl-p-phenylenediamine.
2430	Total Sulphate in soils	Total Sulphate	Acid digestion followed by determination of sulphate in extract by ICP-OES.
2450	Acid Soluble Metals in Soils	Metals, including: Arsenic; Barium; Beryllium; Cadmium; Chromium; Cobalt; Copper; Lead; Manganese; Mercury; Molybdenum; Nickel; Selenium; Vanadium; Zinc	Acid digestion followed by determination of metals in extract by ICP-MS.
2490	Hexavalent Chromium in Soils	Chromium [VI]	Soil extracts are prepared by extracting dried and ground soil samples into boiling water. Chromium [VI] is determined by 'Aquakem 600' Discrete Analyser using 1,5-diphenylcarbazide.
2610	Loss on Ignition	loss on ignition (LOI)	Determination of the proportion by mass that is lost from a soil by ignition at 550°C.
2625	Total Organic Carbon in Soils	Total organic Carbon (TOC)	Determined by high temperature combustion under oxygen, using an Eltra elemental analyser.
2670	Total Petroleum Hydrocarbons (TPH) in Soils by GC-FID	TPH (C6–C40); optional carbon banding, e.g. 3-band – GRO, DRO & LRO*TPH C8–C40	Dichloromethane extraction / GC-FID
2680	TPH A/A Split	Aliphatics: >C5–C6, >C6–C8, >C8–C10, >C10–C12, >C12–C16, >C16–C21, >C21–C35, >C35–C44 Aromatics: >C5–C7, >C7–C8, >C8–C10, >C10–C12, >C12–C16, >C16–C21, >C21–C35, >C35–C44	Dichloromethane extraction / GCxGC FID detection



SOP	Title	Parameters included	Method summary
2760	Volatile Organic Compounds (VOCs) in Soils by Headspace GC-MS	Volatile organic compounds, including BTEX and halogenated Aliphatic/Aromatics.(cf. USEPA Method 8260)*please refer to UKAS schedule	Automated headspace gas chromatographic (GC) analysis of a soil sample, as received, with mass spectrometric (MS) detection of volatile organic compounds.
2800	Speciated Polynuclear Aromatic Hydrocarbons (PAH) in Soil by GC-MS	Acenaphthene*; Acenaphthylene; Anthracene*; Benzo[a]Anthracene*; Benzo[a]Pyrene*; Benzo[b]Fluoranthene*; Benzo[ghi]Perylene*; Benzo[k]Fluoranthene; Chrysene*; Dibenz[ah]Anthracene; Fluoranthene*; Fluorene*; Indeno[123cd]Pyrene*; Naphthalene*; Phenanthrene*; Pyrene*	Dichloromethane extraction / GC-MS
2815	Polychlorinated Biphenyls (PCB) ICES7Congeners in Soils by GC-MS	ICES7 PCB congeners	Acetone/Hexane extraction / GC-MS
2920	Phenols in Soils by HPLC	Phenolic compounds including Resorcinol, Phenol, Methylphenols, Dimethylphenols, 1-Naphthol and TrimethylphenolsNote: chlorophenols are excluded.	60:40 methanol/water mixture extraction, followed by HPLC determination using electrochemical detection.

## Report Information

### Key

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- U UKAS accredited
- M MCERTS and UKAS accredited
- N Unaccredited
- S This analysis has been subcontracted to a UKAS accredited laboratory that is accredited for this analysis
- SN This analysis has been subcontracted to a UKAS accredited laboratory that is not accredited for this analysis
- T This analysis has been subcontracted to an unaccredited laboratory
- I/S Insufficient Sample
- U/S Unsuitable Sample
- N/E not evaluated
- < "less than"
- > "greater than"

Comments or interpretations are beyond the scope of UKAS accreditation

The results relate only to the items tested

Uncertainty of measurement for the determinands tested are available upon request

None of the results in this report have been recovery corrected

All results are expressed on a dry weight basis

The following tests were analysed on samples as received and the results subsequently corrected to a dry weight basis TPH, BTEX, VOCs, SVOCs, PCBs, Phenols

For all other tests the samples were dried at < 37°C prior to analysis

All Asbestos testing is performed at the indicated laboratory

Issue numbers are sequential starting with 1 all subsequent reports are incremented by 1

### Sample Deviation Codes

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- A - Date of sampling not supplied
- B - Sample age exceeds stability time (sampling to extraction)
- C - Sample not received in appropriate containers
- D - Broken Container
- E - Insufficient Sample

### Sample Retention and Disposal

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All soil samples will be retained for a period of 45 days from the date of receipt

All water samples will be retained for 14 days from the date of receipt

Charges may apply to extended sample storage

If you require extended retention of samples, please email your requirements to:

[customerservices@chemtest.co.uk](mailto:customerservices@chemtest.co.uk)

## **Appendix VII Site Plan**

IGSL LTD. 100, 102, 104, 106, 108, 110, 112, 114, 116, 118, 120, 122, 124, 126, 128, 130, 132, 134, 136, 138, 140, 142, 144, 146, 148, 150, 152, 154, 156, 158, 160, 162, 164, 166, 168, 170, 172, 174, 176, 178, 180, 182, 184, 186, 188, 190, 192, 194, 196, 198, 200, 202, 204, 206, 208, 210, 212, 214, 216, 218, 220, 222, 224, 226, 228, 230, 232, 234, 236, 238, 240, 242, 244, 246, 248, 250, 252, 254, 256, 258, 260, 262, 264, 266, 268, 270, 272, 274, 276, 278, 280, 282, 284, 286, 288, 290, 292, 294, 296, 298, 300, 302, 304, 306, 308, 310, 312, 314, 316, 318, 320, 322, 324, 326, 328, 330, 332, 334, 336, 338, 340, 342, 344, 346, 348, 350, 352, 354, 356, 358, 360, 362, 364, 366, 368, 370, 372, 374, 376, 378, 380, 382, 384, 386, 388, 390, 392, 394, 396, 398, 400, 402, 404, 406, 408, 410, 412, 414, 416, 418, 420, 422, 424, 426, 428, 430, 432, 434, 436, 438, 440, 442, 444, 446, 448, 450, 452, 454, 456, 458, 460, 462, 464, 466, 468, 470, 472, 474, 476, 478, 480, 482, 484, 486, 488, 490, 492, 494, 496, 498, 500, 502, 504, 506, 508, 510, 512, 514, 516, 518, 520, 522, 524, 526, 528, 530, 532, 534, 536, 538, 540, 542, 544, 546, 548, 550, 552, 554, 556, 558, 560, 562, 564, 566, 568, 570, 572, 574, 576, 578, 580, 582, 584, 586, 588, 590, 592, 594, 596, 598, 600, 602, 604, 606, 608, 610, 612, 614, 616, 618, 620, 622, 624, 626, 628, 630, 632, 634, 636, 638, 640, 642, 644, 646, 648, 650, 652, 654, 656, 658, 660, 662, 664, 666, 668, 670, 672, 674, 676, 678, 680, 682, 684, 686, 688, 690, 692, 694, 696, 698, 700, 702, 704, 706, 708, 710, 712, 714, 716, 718, 720, 722, 724, 726, 728, 730, 732, 734, 736, 738, 740, 742, 744, 746, 748, 750, 752, 754, 756, 758, 760, 762, 764, 766, 768, 770, 772, 774, 776, 778, 780, 782, 784, 786, 788, 790, 792, 794, 796, 798, 800, 802, 804, 806, 808, 810, 812, 814, 816, 818, 820, 822, 824, 826, 828, 830, 832, 834, 836, 838, 840, 842, 844, 846, 848, 850, 852, 854, 856, 858, 860, 862, 864, 866, 868, 870, 872, 874, 876, 878, 880, 882, 884, 886, 888, 890, 892, 894, 896, 898, 900, 902, 904, 906, 908, 910, 912, 914, 916, 918, 920, 922, 924, 926, 928, 930, 932, 934, 936, 938, 940, 942, 944, 946, 948, 950, 952, 954, 956, 958, 960, 962, 964, 966, 968, 970, 972, 974, 976, 978, 980, 982, 984, 986, 988, 990, 992, 994, 996, 998, 1000

1:1000

DATE: 15/07/2017

SCALE: 1:1000

PROJECT: SITE INVESTIGATION

CLIENT: IGSL LTD.

LOCATION: LANDS AT CARDOO, CLANE, CO. KILDARE

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CLIENT: IGSL LTD.

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Ref: No. 20159 July 2017



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